



40 CFR PART 257 GROUNDWATER MONITORING PLAN

Meramec Energy Center

St. Louis County, Missouri, USA



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1.0 INTRODUCTION

This Groundwater Monitoring Plan (GMP) presents information on the design of the groundwater monitoring system, groundwater sampling and analysis procedures, and groundwater statistical analysis methods for Ameren Missouri's (Ameren) Meramec Energy Center (Facility) in St. Louis County, Missouri (see location on **Figure 1**). The Meramec Energy Center currently manages and has historically managed Coal Combustion Residuals (CCR) generated from the facility at a number of surface impoundments. The surface impoundments onsite consist of:

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- Active Surface Impoundments
 - Surface Impoundment 492 (MCPA), approximately 6 acres
 - Surface Impoundment 493 (MCPB), approximately 6 acres
 - Surface Impoundment 496 (MCPC), approximately 10 acres
 - Surface Impoundment 498 (MCPD), approximately 17 acres
 - Surface Impoundment 489 (MCPE), approximately 24 acres
- Excluded Surface Impoundments
 - Surface Impoundment 490 (MOPF), approximately 23 acres
 - Surface Impoundment 491 (MOPG), approximately 12 acres
 - Surface Impoundment 494 (MOPH), approximately 31 acres
 - Surface Impoundment 495 (MOPI), approximately 16 acres

According to the CCR Rule, all of the Meramec Surface Impoundments are unlined. However, Surface Impoundments 489 and 498 do have a liner in place. Since all the surface impoundments lie very close to one another and dividing berms were constructed with locally derived alluvial material and Coal Combustion Residuals (CCR), the monitoring network design monitors the Meramec Surface Impoundments as one multi-unit system.

This GMP was developed to meet the requirements of United States Environmental Protection Agency (USEPA) 40 CFR Part 257 "Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities; Final Rule" (the CCR Rule). The CCR Rule requires owners or operators of an existing CCR Surface Impoundment to install a groundwater monitoring system and develop a sampling and analysis program (§§ 257.90 - 257.94). Ameren Missouri has determined that the CCR Surface Impoundments at the Meramec Energy Center are subject to the requirements of the CCR Rule. For this GMP, the Meramec Energy Center generating plant is referred to as the MEC and the MEC and its surrounding facilities, including the Meramec Surface Impoundment, are referred to as the Facility or Site.





Ameren owns and operates the Facility in St. Louis County, Missouri located approximately 18 miles southwest of downtown St. Louis. Figure 1 depicts the location of the Facility and property boundaries referenced to local topographic features, the Mississippi River, and the Meramec River. Figure 2 depicts Facility structures relative to site property boundaries and the two adjoining rivers. The Facility property encompasses approximately 480 acres and is primarily located in the topographically low area north of the confluence of the Mississippi and Meramec Rivers. The property is bounded to the northeast by wooded and partially developed land, to the southeast by the Mississippi River, to the southwest and west by the Meramec River and to the northwest by wooded and partially developed land.

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The Facility is located in a topographically low area in a valley at the confluence of the Meramec and Mississippi Rivers, with a surface elevation of approximately 420 feet above mean sea level (MSL) at the plant area. Topographically higher terrain is located west of the Meramec River Valley. The terrain to the east of the Facility consists of topographically higher terrain, at elevations generally ranging from 450 MSL feet to as high as 550 feet MSL, as shown on Figure 2 and Appendix A.

2.1 **Coal Combustion Residuals (CCR) Surface Impoundments**

The Facility includes a coal fired power plant as well as five (5) currently active CCR surface impoundments that are used for CCR management. Historically, CCR has also been stored in four (4) additional surface impoundments, which are no longer ponded and are excluded from the CCR Rule groundwater monitoring requirements. A list of the Meramec Surface Impoundments is provided above in Section 1.0.

The present Site grade is as much as 20 feet above the original ground surface. As part of the MEC plant construction project, the original grade of the plant was increased by using fill material. The ash ponds were reportedly made by excavating on-Site material silts and clays and using the materials as construction fill beneath the plant as well as for surface impoundment berms (CH2MHILL, 1997). Reportedly, the Meramec Surface Impoundments were excavated approximately 10-20 feet below the original grade and then were used to contain the CCR. Therefore, present day ash thickness is reported to be typically 20 to 30 feet below the present Site grade, which is considered to be nominally at approximately 420 feet MSL (CH2MHILL, 1997). Based on this information, the generalized elevation of the base of the coal ash is estimated to be approximately 390 feet MSL. A cross section drawn through Ash Ponds 489 and 491 indicate the elevation of the base of ash is 390 feet MSL and 395 feet, respectively (CH2MHILL 1997, Appendix B).

CCR thickness was directly measured at three locations in Surface Impoundment 494 to be at least 26.5 feet thick (Golder, 2008) and at an elevation as low as approximately 387 feet MSL. CCR thickness was measured at two locations in Surface Impoundment 489 (Woodward-Clyde Consultants, 1988). The bottom of ash elevations were estimated to be 387.3 and 389.1 feet MSL.



While according to the CCR Rule all of the Meramec Surface Impoundments are treated as unlined units, Surface Impoundment 498 has a geomembrane liner with a base elevation of approximately 395 feet MSL (Ameren drawing SK-005-R2, 2011) and Surface Impoundment 489 is lined with a geomembrane with a base at an elevation of approximately 408 feet MSL (Ameren drawing 8020-X-135358, 1994). See **Appendix B** for referenced drawings.

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2.2 Geology

2.2.1 Physiographic Setting and Regional Geology

The Facility is located in the extreme southeastern corner of the Central Lowland Physiographic Province and the Dissected Till Plains (Miller et al., 1974). However, the Facility lies between two major river systems near their confluence and within the floodplain of the Mississippi and Meramec Rivers in an area that contains alluvial river deposits. Therefore, the local site landforms are characterized by alluvial flood plain landforms.

2.2.2 Local Geology

The geology immediately surrounding the Facility is comprised of two distinctly different geological terrains; (1) floodplain deposits of the Mississippi and Meramec River Valleys and (2) older sedimentary bedrock formations. Most of the Facility, including all of the plant infrastructure and the Meramec Surface Impoundments lie within these floodplain deposits. The river valley area is comprised of floodplain and alluvial deposits that are the result of the water flow and deposition of the Mississippi and Meramec Rivers.

Based on previous investigations, the alluvial materials on the east side of the Facility tend to have more clayey silts, silty clays, and fine sands (CH2MHILL, 1997). Alluvial materials to the west, closer to the Meramec River, include coarser materials, including fine- to medium-grained sand with clay, silt, and some gravels (CH2MHILL, 1997). The depth of the alluvial deposits near the MEC range from approximately 105 to 120 feet below ground surface (bgs) and become shallower towards the bluffs to the northeast.

Shannon and Wilson (1979) completed a geotechnical investigation in the area directly around the MEC. 16 geotechnical borings were completed as a part of this investigation. Based on borings and cross sections from this report, the local geology directly adjacent to the MEC is as follows:

- Approximately 420-410 feet MSL Fill Materials
- Approximately 410-375 feet MSL Clays, Clayey Silts, and Silty Clays
- Approximately 375-340 feet MSL Silts, Sandy Silts, Silty Sands, and Sands that thicken to the southeast towards the Mississippi River
- Approximately 340-320 feet MSL Clays and Silty Clays
- Approximately 320-310 feet MSL Intermittent Sands, Gravels, and Clayey Gravels
- Approximately 310 feet MSL and below Limestone and Shale Bedrock



Drilling completed as a part of installation of the monitoring well network used for this GMP show similar results to previous studies. Borings located to the southwest of the MEC (MW-5, MW-6 and MW-7) encounter poorly and well graded sands that are likely associated with past meanders of the adjacent Mississippi and Meramec Rivers. The sand in these wells becomes more prevalent at locations closer to the Mississippi River to the south/southeast. Drilling completed further from the Mississippi River to the northwest consisted of more fine-grained materials such as silts, clays and silty clays with occasional sandy/gravelly lens deposits. These deposits are typical for low energy floodplain deposits with occasional sandy/gravel units from historical Meramec River channel meanders.

Bedrock beneath the Facility consists of the Warsaw Formation, of the Mississippian aged Meramecian Series and consists of shales and fine-grained shaley limestone (CH2MHILL, 1997). The bluff area on the east side of the Facility consists of the Salem Formation at lower elevations and St. Louis Limestone at higher elevations (Middendorf and Brill, 2002).

2.3 Site Hydrogeology

Site hydrogelogy has been characterized based on data collected during several different investigations. In 1988, five (5) monitoring wells were installed around the MEC by Woodward-Clyde Consultants (Woodward-Clyde). A map of the monitoring wells is provided in **Appendix C**. Observations from these five groundwater monitoring wells is summarized below. CH2MHill (1997) also completed a hydrogeological assessment using the monitoring wells installed by Woodward Clyde.

Golder (2008) installed five (5) piezometers both in and directly adjacent to Surface Impoundment 494. This effort provides information on the depth of ash in the Meramec Surface Impoundments, geotechnical data of the soil in and around the Meramec Surface Impoundments, and water level information in and around the Meramec Surface Impoundments.

Golder also installed ten (10) monitoring wells and borings as a part of the installation of the CCR monitoring well network used for CCR monitoring. **Appendix A** provides cross section depictions of the subsurface geology. Boring logs and monitoring well construction diagrams are provided in **Appendix D** and **Appendix E**.

2.3.1 Uppermost Aquifer

The CCR Rule requires that a groundwater monitoring system be completed in the uppermost aquifer around each Active CCR Surface Impoundment (§257.91(a)). As shown on **Appendix A**, the uppermost aquifer is the alluvial silt, sand and gravel deposits associated with the Meramec and Mississippi River Valley alluvium (CH2MHILL, 1997; Shannon & Wilson, 1979; **Appendix C**). These channel deposits are intermixed with a wide variety of clay/silty clay floodplain deposits and, therefore, can appear at varying





depths. However, sandy/gravelly units were encountered at many locations at approximately 360-370 feet MSL, likely deposited from a historic meander of the Meramec River. These alluvial deposits overlie Mississippian-age limestone and shale of the Meramecian Series. The depth of the alluvial aquifer typically ranges from approximately 105 to 120 feet bgs (approximately 255 to 331 feet MSL), but thins to the east toward the bluff (CH2MHILL, 1997), where it is not present at higher elevations above the floodplain.

2.3.2 Surface Water and Groundwater Elevations

2.3.2.1 CCR Surface Impoundment Water

Meramec pond gauge measurements were provided by Ameren for Surface Impoundments 498, 492, 493, and 496. These measurements were obtained during a similar timeframe as the groundwater measurements from each of the 8 initial background sampling events (baseline events). During this time, Surface Impoundment 498 had a pond level ranging from approximately 417 to 418 feet MSL. This pond has a liner system in place and does not connect with the underlying aquifer or surrounding surface impoundments. The pond level in Surface Impoundments 492, 493, and 496 ranged between approximately 408 and 412 feet MSL. These Surface Impoundments ranged between 9 to 30 feet above the natural groundwater elevations in the surrounding aquifer. The difference between the pond level and the natural groundwater elevation is greatest when the Mississippi River level is low. Data show water mounding within the Meramec Surface Impoundments without a liner regardless of the river level; however, the mounding is less pronounced at times of high river level.

2.3.2.2 Alluvial Aguifer

Groundwater elevations within the alluvial aquifer in the Facility area have been obtained in several different studies. Historical groundwater measurements come from five (5) monitoring wells installed in 1988 by Woodward-Clyde and then re-analyzed in 1997 by CH2MHILL. Three of the monitoring wells (B-4, B-5, and B-6) were installed with total depths ranging from 90 and 101 feet bgs. These three (3) monitoring wells were located near Surface Impoundment 489 at the southwest corner of the Facility, near the Meramec River. Groundwater elevations in the downgradient monitoring wells near Surface Impoundment 489 ranged between approximately 377 and 385 feet MSL and were similar to the concurrent Mississippi River level. Monitoring wells B-1 and B-2 were installed on the east (upgradient) side of the Facility with total depths ranging from 41 to 56 feet bgs. Groundwater elevations in these monitoring wells ranged from approximately 403 to 415 feet MSL and were typically 20 to 30 feet higher in elevation than the Mississippi River. Additionally, one monitoring well (B-7) was installed into the coal ash to a total depth of 389 feet MSL and was dry in all readings (Woodward-Clyde Consultants, 1988). Results from these groundwater elevation measurements are provided in **Appendix C**.

Golder obtained groundwater elevation measurements from March 2016 through June 2017 within the alluvial aquifer for the CCR monitoring wells. For each of the 8 baseline sampling events, groundwater





elevations were measured at monitoring wells within a 24-hour timeframe and a potentiometric map was generated from these data (**Appendix F and Table 1**). Groundwater elevations ranged from approximately 380 to 400 feet MSL throughout the baseline sampling events except at MW-1, which ranged from approximately 400 to 404 feet MSL.

2.3.3 Groundwater Flow Directions

Groundwater flow within the alluvial aquifer is dynamic and is influenced by seasonal changes in the water level in the adjacent Mississippi and Meramec Rivers. River water levels measured at the Facility display large seasonal changes in the elevation of the Mississippi River water surface. For example, from January 2010 to April 2017, river water levels fluctuated between approximately 365 to 413 feet MSL. Water flows into and out of the alluvial aquifer as a result of fluctuating river water levels that produce "bank recharge" and "bank discharge" conditions. Under normal aquifer conditions, groundwater flow in the alluvial aquifer would be expected to have a flow direction component toward the Mississippi and Meramec Rivers, with a net flow direction generally to the southwest.

Although the movement of groundwater within the alluvial aquifer at the Facility is complex, the movement has been characterized by groundwater elevation measurements and the generation of potentiometric surface maps generated by Woodward-Clyde and Golder (**Appendix C, Appendix F, and Table 1**). The potentiometric surface maps display minor variability in the groundwater flow direction. These changes in flow direction are related to the level within the adjacent Mississippi and Meramec Rivers.

Groundwater flow direction and hydraulic gradient were estimated for the CCR wells using the EPA's Online Tool for Site Assessment (USEPA, 2016). Estimated results from this analysis using groundwater elevations within the CCR monitoring wells are provided in **Table 2**. These results indicate that while groundwater flow direction is somewhat variable, overall net groundwater flow during the baseline sampling period was generally toward the west/southwest, flowing from the bluffs toward the rivers.

Based on the potentiometric surface maps and groundwater calculations, a general flow direction from the northeast (bluffs) to the southwest (Mississippi and Meramec Rivers) under normal river conditions is expected. However, during periods of high river levels, groundwater flow can temporarily reverse in localized areas. During these times of high river stage and temporary flow direction changes, horizontal groundwater gradients generally decrease and little net movement of groundwater to the north and east occurs.

Horizontal and vertical groundwater flow within the uppermost aquifer has been locally influenced by operation of the Meramec Surface Impoundments. Ponding of water in the Meramec Surface Impoundments that do not have a liner in place at elevations greater than the static water levels in the





underlying alluvial aquifer groundwater creates a localized mounding effect, resulting in localized downward gradients and localized radial groundwater flow downward and outward from these impoundments.

2.3.3.1 Horizontal Gradients

Horizontal groundwater gradients in the alluvial aquifer are very dependent on river water levels (bank recharge and bank discharge conditions described earlier). Site wide horizontal gradients were calculated for each of the CCR groundwater baseline sampling events and the results of these are displayed on **Table**2. The horizontal groundwater gradients range from 0.001 to 0.003 feet/foot.

2.3.3.2 Vertical Gradients

A review of downward gradients that exist on site was completed by comparing groundwater elevations in the CCR monitoring wells to the Meramec Surface Impoundment pond gauges. On average, the groundwater elevation of the active ponds that do not have a liner (492, 493, and 496) is approximately 9 to 30 feet higher than the alluvial groundwater zone. However, this downward gradient also changes seasonally based on river levels. During high river level conditions, the difference in groundwater elevation between the surface impoundments and the alluvial groundwater zone is the smallest.

2.3.4 Hydraulic Conductivities

Golder performed in-situ rising head hydraulic conductivity tests on the 10 newly installed CCR monitoring wells used to monitor the Meramec Surface Impoundments in order to estimate the hydraulic conductivities. The tests were conducted using a pneumatic slug (Hi-K slug) and a downhole pressure transducer. The results of Golder's hydraulic conductivity testing estimated an average hydraulic conductivity of approximately 2.3 x 10⁻² centimeters per second (cm/sec) and a geometric mean of 1.4 x 10 of ⁻² cm/sec. Golder's findings for hydraulic conductivity values are summarized below in **Table 3** provided below in the text.

Estimated groundwater flow velocities were calculated using the CCR monitoring well hydraulic conductivity, hydraulic gradients and an estimated value for effective porosity (**Table 2**). Using these values, flow velocities are estimated to range between 0.13 and 0.34 feet per day, and approximately 87 feet per year.



Well ID	Total Depth (feet BTOC)	Well Screen Interval (feet BTOC)	Well Screen interval (feet MSL)	Estimated Hydraulic Conductivity (feet/day)	Estimated Hydraulic Conductivity (cm/sec)
MW-1	41.4	36.2 - 41.0	365.4 - 370.2	85	3.00E-02
MW-2	36.8	31.6 - 36.4	362.2 - 367.0	92	3.26E-02
MW-3	33.1	27.9 - 32.7	364.4 - 369.2	185	6.52E-02
MW-4	45.2	40.0 - 44.8	359.3 - 364.1	46	1.63E-02
MW-5	62.7	52.5 - 62.3	340.6 - 350.4	56	1.98E-02
MW-6	54.9	44.7 - 54.5	363.6 - 373.4	37	1.32E-02
MW-7	54.9	44.7 - 54.5	363.4 - 373.2	49	1.74E-02
MW-8	77.8	67.6 - 77.4	346.0 - 355.8	5	1.89E-03
BMW-1	62.89	52.7 - 62.5	356.6 - 366.4	3	9.91E-04
BMW-2	44.9	39.7 - 44.5	364.5 - 369.3	106	3.75E-02

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Notes:

- 1. feet BTOC feet below top of casing ft BGS feet below ground surface.
- 2. feet MSL feet above mean sea level.
- 3. cm/sec centimeters per second.
- 4. Slug tests were completed by Golder Associates using a Pneumatic Hi-K Slug[®].

2.3.5 Porosity and Effective Porosity

Porosities were estimated based on the grain size distributions of aquifer soil samples collected during monitoring well drilling. Representative grain size distributions were collected from the screened intervals at MW-6 and MW-8 using the ASTM D6912 Method B and the results are provided in **Appendix G**. MW-6 represents monitoring wells that were located closer to the Mississippi River and had more sandy environments, whereas MW-8 represents wells that contained gravel/silty sand environments that were further from the Mississippi and are historical Meramec River channels. The results indicate that the screened intervals of the alluvial aquifer near the Mississippi River are mostly comprised of sand (at least 90%) with lesser amounts of gravel, silt and clay. Also, the typical grain size of the sand ranges from fine to medium sand. Textbook values of porosities for sands and sand/gravel mixes range from 25-50% (Fetter, 2000 and Freeze and Cherry, 1979) and fine sands typically range from 29-46%, whereas coarse sands typically range from 26-43% (Das, 2008). An average porosity of 35% is estimated for the alluvial aquifer based on the Site data.

Effective porosity is the porosity that is available for fluid flow. Studies completed in unconsolidated sediments have determined that water molecules pass through all pores and the effective porosity is approximately equal to the total porosity (Fetter, 2000). Therefore, the effective porosity of the alluvial aquifer is also estimated to be 35%.





3.0 **GROUNDWATER MONITORING NETWORK**

3.1 **Monitoring Network Design Criteria**

§257.91 of the CCR Rule sets out the requirements for development of a groundwater monitoring system for both new and existing CCR landfills and surface impoundments. The performance standard in the CCR Rule (§257.91(a)) states that the groundwater monitoring system must consist of a sufficient number of wells at appropriate locations to yield groundwater samples in the uppermost aquifer that accurately represent:

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- The quality of background groundwater
- The quality of groundwater passing the waste boundary of the CCR unit

3.2 **Design of the Groundwater Monitoring System**

The detection monitoring well network for the Facility is depicted on Figure 2. The network consists of 10 monitoring wells screened in the uppermost aguifer for the purpose of monitoring the Meramec Surface Impoundments. The monitoring well network includes two (2) background groundwater monitoring wells (BMW-1 and BMW-2) that are located on the bluff side of the facility in areas upgradient and unaffected by CCR disposal. BMW-1 is located near the bluffs on the southeastern portion of the site and BMW-2 is located near the bluffs on the northeastern portion of the site. Eight (8) of the groundwater monitoring wells are placed ringing the Meramec Surface Impoundments and are downgradient wells. groundwater monitoring well locations were selected based on site-specific technical information presented in Section 2.0 of this document, as well as the preferential migration pathway analysis below.

3.2.1 Preferential Migration Pathway Analysis

As discussed in Section 2.3, the movement of constituents in water from the ash within the Meramec Surface Impoundments will be downward and predominately in the downgradient direction toward the Meramec and Mississippi Rivers. Groundwater elevations are higher to the east and lower to the west/south, and fluctuate with river stages. CCR is known to be at least 28 feet thick, placing it at an approximate base elevation of 385 to 390 feet MSL. Groundwater levels onsite in downgradient wells typically range from 380 to 385 feet MSL under normal river conditions and can be as high as 395 feet MSL or higher during high river conditions. Upgradient wells range from 390 to 400 feet MSL. The potential exists for constituents to migrate from the Meramec Surface Impoundments into the alluvial aquifer from depths ranging from the water table surface down to the lowest depth of CCR, followed by lateral movement in the direction of groundwater flow. Geologically, the preferential pathway for groundwater is through zones with the highest conductivity and flow. The highest conductivity layers on-site are those comprised of coarse-grained particles such as sand, gravel and silty sands. Groundwater in these units will have higher dispersivity.





In order to place monitoring well screens within the migration pathway from the unit and to consistently have water for sampling, monitoring wells were installed with screen intervals below the seasonal groundwater lows and placed with screening levels that intercept water from the units with the greatest hydraulic conductivity and flow. The system of monitoring wells ringing the Meramec Surface Impoundments are screened in the uppermost unit and monitor groundwater quality passing the waste boundary.

3.3 Groundwater Monitoring Well Placement

3.3.1 Background/Upgradient Monitoring Well Locations

As described above, the flow of groundwater in the alluvial aquifer is generally from the bluff area located northeast of the site toward the Mississippi and Meramec Rivers to the south and west, however, alluvial aquifer flow is locally influenced by water levels in the active surface impoundments without a liner (492, 493, and 496) and the Mississippi and Meramec River levels. The CCR Rule (§257.91(a)(1)) requires that background groundwater samples from the uppermost aquifer "Accurately represent the quality of background groundwater that has not been affected by leakage from a CCR unit."

As shown in **Figure 2**, the background monitoring wells BMW-1 and BMW-2 are located close to the bluff on the eastern side of the Facility. BMW-1 is located to the southeast of the Meramec Surface Impoundments and BMW-2 is located to the northeast of the Meramec Surface Impoundments. These wells provide background groundwater quality representative of upgradient groundwater that will pass through the Meramec Surface Impoundments.

3.3.2 Downgradient Monitoring Well Locations

As discussed above, downgradient monitoring wells are located ringing the Meramec Surface Impoundments to monitor potential migration pathways. **Figure 2** shows that the downgradient well network consists of eight (8) groundwater monitoring wells (MW-1, MW-2, MW-3, MW-4, MW-5, MW-6, MW-7, and MW-8) around the Meramec Surface Impoundments at locations that are located as close to the waste boundary as practical.

3.3.3 Groundwater Monitoring Well Screen Intervals

The system of monitoring wells ringing the Meramec Surface Impoundments are screened in the alluvial aquifer zone near the base elevation of the CCR. Details on the construction of the groundwater monitoring wells are provided in **Table 4** and **Appendix E**.

Screen intervals were installed within the uppermost high conductivity unit within the alluvial aquifer at each location that was below the seasonal low for groundwater. Each well has an approximately 5- or 10-footlong screen interval. Screen intervals for the CCR Wells range from approximately 341 to 374 feet MSL





(approximately 25 to 75 feet bgs). Monitoring well construction information is shown in **Table 4** and **Appendix E**.



4.0 INSTALLATION OF THE GROUNDWATER MONITORING SYSTEM

The CCR Rule Groundwater Monitoring System for the Meramec Surface Impoundments was installed in January 2016 and April 2016 as described in the following subsections.

4.1 Drilling Methods and Monitoring Well Constructions

Cascade Drilling LP installed the monitoring wells using a rotosonic drill rig (Mini Sonic CDD 1415) under direct supervision of a Golder Geologist or Engineer. Continuous soil core samples were obtained at each well borehole location and were logged in the field by Golder. Soils were classified according to the Unified Soil Classification System. Boring logs and well construction diagrams are provided in **Appendix D** and **Appendix E** respectively.

Groundwater monitoring wells were installed in accordance with Missouri Department of Natural Resources (MDNR) Well Construction Rules (10 CSR 23-4.060 Construction Standards for Monitoring Wells). All groundwater monitoring wells were installed using 2-inch diameter PVC well riser pipe and 5 or 10-foot long, 0.010-inch machine slotted well screens. Wells were installed with a sand filter pack, bentonite seal, and annular space in accordance with MDNR Well Construction Rules. Details on the construction of the groundwater monitoring wells are provided in **Table 4** and **Appendix E**.

Monitoring wells were completed with an aluminum protective cover with a locking lid that extends approximately 2 to 3 feet above ground surface and a small concrete pad. Three yellow protective posts (concrete filled steel bollards) were installed around each monitoring well surface completion.

4.2 Groundwater Monitoring Well Development

After well construction, a Golder Geologist or Engineer developed groundwater monitoring wells using surging and purging techniques. During development, field parameters (pH, conductivity, temperature, and turbidity) were recorded and development was complete once a minimum of three well-bore volumes of water were purged, turbidity was typically less than 20 nephelometric turbidity units (NTU) or ± 10% and consecutive measurements of field parameter values were within 10 percent difference. Groundwater monitoring wells were developed using an inertial pump with a surge block ring attached to a foot valve to surge and purge the well. Well development forms are attached in **Appendix H**.

4.3 Dedicated Pump Installation

A dedicated pump was installed in each groundwater monitoring well after development and hydraulic conductivity testing. The dedicated pumps provide a consistent, repeatable sampling method to reduce likelihood of cross contamination, reduce water sample turbidity, and expedite sampling. For the purposes of this groundwater monitoring network, low-flow QED brand PVC MicroPurge bladder pumps with Dura-Flex Teflon bladders were installed in each well.





4.4 Surveying and Well Registration

Zahner and Associates, Inc., a Professional Land Surveyor licensed in Missouri, surveyed the location and top of casing elevation of the monitoring wells. A drawing showing the location of the groundwater monitoring wells is shown in **Figure 2** and a summary of survey information is provided in **Table 4**. Upon completion of monitoring well installation and surveying, MDNR Well Construction Registration Forms were prepared for each well and submitted to MDNR. Copies of these forms are provided in **Appendix I**.



5.0 GROUNDWATER MONITORING PROGRAM

The groundwater monitoring program for the Meramec Surface Impoundments is described in the following sections.

5.1 Baseline Sampling Events

In accordance with section 257.94(b) of the CCR Rule, before starting detection monitoring, eight baseline (or background) samples were collected for all Appendix III and Appendix IV parameters at all downgradient and upgradient/background monitoring wells prior to October 17, 2017. These samples establish initial baseline datasets that are used for the statistical evaluation of groundwater results.

5.2 Detection Monitoring

The Detection Monitoring Program is defined in the CCR Rule in section 257.94 and the following sections outline the procedures for the detection monitoring program.

5.2.1 Sampling Constituents and Monitoring Frequency

Detection monitoring should be completed at a minimum of semi-annually (approximately every 6 months) for all Appendix III constituents (**Table 5**) unless a demonstration that the need for an alternative monitoring schedule is required. **Table 6** lists the analytical methods and practical quantitation limits used for the monitoring program.

5.2.2 Data Evaluation and Response

As required in the CCR Rule, a statistical evaluation of the groundwater data must be completed within 90 days of receiving data from the laboratory. The data will be analyzed using the methods and procedures outlined in the statistical analysis plan (**Appendix J**).

5.3 Assessment Monitoring

Assessment monitoring is outlined in section 257.95 of the CCR Rule and is initiated after a confirmed SSI has been identified and no alternate source demonstration has been completed. In accordance with the CCR Rule, a notification must be prepared and placed within the Facility operating record and on the publically available website stating that an Assessment Monitoring program has been initiated. The purpose of Assessment Monitoring is to determine whether or not groundwater concentrations are at a Statistically Significant Level (SSL) compared to Groundwater Protection Standards (GWPS). Detection Monitoring sampling continues during Assessment Monitoring.

5.3.1 Sampling Constituents and Monitoring Frequency

As outlined in section 257.95 of the CCR rule, Assessment Monitoring groundwater sampling must begin within 90 days of a confirmed SSI determination. Sampling must be completed at all monitoring wells used in the detection monitoring program, for all Appendix IV analytes (**Table 5**). Within 90 days of receiving





data from this initial Assessment Monitoring sampling event, a second sampling event must be completed analyzing the Appendix IV constituents detected in groundwater during the initial sampling event.

Following this initial phase of the Assessment Monitoring Program, the CCR Rule requires sampling of the full list of Appendix IV constituents on an annual basis (Annual Assessment Event). During the other semi-annual Assessment Sampling Event, only those Appendix IV constituents that are detected during the annual sampling event are to be analyzed and reported. Additionally, verification resampling will be performed within 90 days of receiving data from the laboratory for all detected Appendix IV constituents for each event.

5.3.2 Data Evaluation and Response

As required in the CCR Rule, a statistical evaluation of the groundwater data must be completed within 90 days of receiving data from the laboratory. The data will be analyzed using the methods and procedures outlined in the Statistical Analysis Plan (**Appendix J**).

A GWPS is required for each Appendix IV constituent and must be included in the annual report. The GWPS will be either the MCL or a value based on background data, whichever is higher. The generation of the GWPS is discussed in more detail in the Statistical Analysis Plan (**Appendix J**). Statistical analysis must be completed within 90 days of receiving data from the laboratory. The statistical analysis will determine if any constituents are SSLs greater than the GWPS.

In order to discontinue Assessment Monitoring and return to Detection Monitoring, the concentration of all Appendix III and Appendix IV constituents for all compliance wells must be at levels statistically lower than background levels for two consecutive sampling events (257.95(e)). If any constituent is present at a statistical level above background levels, but below the GWPS, then Assessment Monitoring continues.

5.3.2.1 Responding to a SSL

If the Assessment Monitoring statistical evaluations demonstrate that a SSL has been triggered, then the owner/operator of the CCR unit must complete the following four actions as described in 257.95(g):

- 1. Prepare a notification identifying the constituents in Appendix IV that have exceeded a CCR Unit specific GWPS. This notification must be placed in the facility operating record within 30 days of identifying the SSL (257.95(g)) and 257.105(h)). Additionally, within 30 days of placing the notification in the operating record, the notification must be posted to the internet site (257.107(h)).
- 2. Define the character and extent of the release and any relevant site conditions that may affect the corrective action remedy that is ultimately selected. The characterization must be sufficient to support a complete and accurate assessment of the corrective measures necessary to effectively clean up releases from the CCR Unit and must include at least the following: (No timeframe is specified in the CCR Rule for this action)





- A. Installation of additional monitoring wells that are necessary to define the contaminant plume
- B. Collect data on the nature and estimated quantity of the material released
- C. Install and sample at least one additional monitoring well at the facility boundary in the direction of the contaminant plume migration
- 3. Notify off-site property owners if the contamination plume has migrated offsite on to their property within 30 days of this determination.
- 4. If possible, provide an alternate source demonstration that determines that the SSL is not caused by a release at the facility within 90 days of completing the statistical evaluation. If no alternate source demonstration can be made and the plume is determined to have originated from the CCR Unit, then proceed to corrective action steps in the CCR Rule.
 - D. If no alternate source demonstration is made, and the CCR Unit is an unlined surface impoundment, the closure or retrofit must be initiated.

Actions 1-3 must be completed regardless of whether or not an alternate source demonstration can be made.

5.3.3 Annual Reporting Requirements

In addition to the periodical reporting listed above, an annual groundwater monitoring report will be prepared according to the requirements of 40 CFR §257.90(e). At a minimum, the annual groundwater monitoring report will contain the following information:

- The current status of the groundwater monitoring program
- A projection of key activities planned for the upcoming year
- A map showing the CCR unit and all background (or upgradient) and downgradient monitoring wells included in this monitoring plan
- A discussion of any monitoring wells that were installed or decommissioned during the preceding year or any other changes made to the groundwater monitoring system
- Analytical results from groundwater sampling
- The monitoring data obtained under §§ 257.90 through 257.98, including a summary of the number of groundwater samples that were collected for analysis for each background and downgradient well, the dates the samples were collected, and whether the sample was required by the detection monitoring or assessment monitoring programs
- A narrative discussion of any transition between monitoring programs (e.g., the date and circumstances for transitioning from detection monitoring to assessment monitoring in addition to identifying the constituent(s) detected at a statistically significant increase over background levels)
- If required, an alternate source demonstration that is certified by a professional engineer
- If required, a demonstration that an alternate sampling frequency is needed
- If assessment monitoring is required, a listing of GWPS for each Appendix IV constituent



6.0 GROUNDWATER SAMPLING METHODOLOGY

Sampling will be performed in accordance with generally accepted practices within the industry and with the provisions of Missouri regulations. The following sections provide details regarding procedures that will be used to collect groundwater samples. Although this section provides reference to specific forms, the use of other equivalent forms to record the necessary data is permissible.

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6.1 Equipment Calibration

Equipment used to record field water quality parameters will be calibrated each day prior to use following manufacturers' recommendations. Calibration solutions for standardization materials will be freshly prepared or from non-expired stock. In the absence of manufacturer or regulatory guidance, field equipment should be calibrated to within +/- 10 percent of the standard (or 0.1 standard units for pH meters). Equipment that fails calibration may not be used. Calibration records will be maintained. A sample field Instrument Calibration Form is included in **Appendix K**.

6.2 Monitoring Well Inspection

Prior to performing any water purging or sampling, each monitoring well will be inspected to assess its integrity. The condition of each monitoring well will be evaluated for any physical damage or other breach of integrity. The security of each monitoring well will be assessed in order to confirm that no outside source constituents have been introduced to the monitoring well.

6.3 Water Level Measurement

To meet the requirements of §257.93(c), water level measurements will be taken at all monitoring wells and prior to the start of any groundwater purging. These measurements will be taken within a 24 hour period and will be recorded on the Record of Water Level Readings form or Groundwater Sample Collection Form (included in **Appendix I**). Static water levels will be measured in each monitoring well prior to purging using an electric meter accurate to 0.01 foot. The measuring probe will be rinsed with distilled or deionized water before and after use at each well.

6.4 Monitoring Well Purging

Prior to collecting samples, each monitoring well will be purged. Purging will be accomplished using either:

- Low-flow (a.k.a., minimal drawdown, or Micropurge) techniques
- Traditional purging techniques where at least three well volumes are evacuated before samples are collected

6.4.1 Low-Flow Sampling Technique

Low-flow groundwater sampling procedures will be used for purging and sampling monitoring wells that are equipped with dedicated pumps and will sustain a pumping rate of at least 100 milliliters per minute (ml/min).





Water will be purged from these wells at low rates in order to minimize drawdown in the well during purging and sampling. Depth to water measurements and field water quality parameters (temperature, pH, turbidity, and conductivity) recorded during purging will be used as criteria to determine when purging has been completed. Sample collection will be initiated immediately after purging at each well.

During water purging, wells will be pumped at rates that minimize drawdown in the well. Purging rates in the range of 100-500 ml/min typically will be used; however, higher rates may be used if sustained by the well. Stabilization of the water column will be considered achieved when three consecutive water level measurements vary by 0.3 foot or less at a pumping rate of no less than 100 ml/min.

At a minimum, field water quality parameter measurements of temperature, pH, turbidity, and conductivity, will be measured during purging at each well. Prior to collecting the initial set of field water quality parameters, the water in the sampling pump and discharge tubing (i.e., pump system volume) remaining from the previous sampling event will be removed.

After evacuating the water in the pump system, collecting field measurements will begin. Depth to water measurements and field water quality parameter measurements will be made during purging. If a field meter equipped with a flow cell is used, an amount of water equal to the volume of the flow cell should be allowed to pass through the flow cell between individual field stabilization measurements. Stabilization will be attained and purging considered complete when three consecutive measurements of each field parameter vary within the following limits:

- ± 0.2 for pH
- ± 3% for Conductivity
- ± 10% for Temperature
- Less than 10 nephelometric turbidity units (NTU) or ± 10% for Turbidity

All data gathered during monitoring well purging will be recorded on a form, an example of which is included in **Appendix K**.

6.4.2 Traditional Purge Techniques

If low-flow sampling is not performed, wells will be purged a minimum of 3 well volumes before collecting a sample. Purging procedures will generally follow those for low-flow sampling including measurement of the field parameters listed above with two exceptions:

- Higher flow rate may be used during purging
- Purging is completed after a minimum of 3 well volumes have been removed (see below)

Even where low-flow sampling is not performed, the sampling goals are to:





- Stabilize field parameters (listed in previous section) prior to collecting samples
- Minimize drawdown in the well

When traditional purge techniques are used, field stabilization measurements will be collected at the beginning of purging and between each well volume purged. The stability criteria will be those described above for low-flow sampling.

6.4.3 Low Yielding Wells

If a monitoring well purges dry, it will be allowed to recover up to 24 hours before samples are collected. No additional purging will be performed after initially purging the monitoring well dry. If recharge is insufficient to fill all necessary sample bottles, samplers will note this on the field form, and fill as many sample bottles as possible.

6.5 Sample Collection

Sampling should take place immediately after purging is complete. Samples will be transferred directly from field sampling equipment into containers supplied by the analytical laboratory appropriate for the constituents being monitored as listed in **Table 6**. Sample containers will be kept closed until the time each set of sample containers is filled.

6.6 Equipment Decontamination

All non-dedicated field equipment that is used for purging or sample collection shall be cleaned with a phosphate-free detergent and triple-rinsed, inside and out, with deionized or distilled water prior to use and between each monitoring well. Decontamination water shall be disposed of at an Ameren approved location. Any disposable tubing used with non-dedicated pumps should be discarded after use at each monitoring well. Clean latex gloves will be worn by sampling personnel during monitoring well purging and sample collection.

6.7 Sample Preservation and Handling

In accordance with §257.93 of the CCR Rule, groundwater samples collected as part of the monitoring program will not be filtered prior to analysis. Once groundwater samples have been collected and preserved in laboratory supplied containers, they will be packed into insulated, ice-filled coolers to be maintained at a temperature as close as possible to 4 degrees Celsius. Groundwater samples will be collected in the designated size and type of containers required for specific parameters. Sample containers will be filled in such a manner as not to lose preservatives by spilling or overfilling. Samples will be delivered to the laboratory or sent via overnight courier following chain-of-custody procedures.

6.8 Chain-of-Custody Program

The chain-of-custody (COC) program will allow for tracing sample possession and handling from the time of field collection through laboratory analysis. The COC program includes sample labels, sample seals,



field Groundwater Sample Collection Forms, and COC record. A sample Chain-of-Custody (COC) form is provided in **Appendix K**.

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Each sample will be assigned a unique sample identification number to be recorded on the sample label. The sample identification number for all samples will be designated differently based on the nature of the samples. Each sample identification number and description will be recorded on the field Groundwater Sample Collection Form and on the COC document.

6.8.1 Sample Labels

Sample labels sufficiently durable to remain legible when wet will contain the following information, written with indelible ink:

- Site and sample identification number
- Monitoring well number or other location
- Date and time of collection
- Name of collector
- Parameters to be analyzed
- Preservative, if applicable

6.8.2 Sample Seal

The shipping container will be sealed to prevent the samples from being disturbed during transport to the laboratory.

6.8.3 Field Forms

All field information must be completely and accurately documented to become part of the final report for the groundwater monitoring event. Example field forms are included in **Appendix J**. The field forms will document the following information:

- Identification of the monitoring well
- Sample identification number
- Field meter calibration information
- Static water level depth
- Purge volume
- Time monitoring well was purged
- Date and time of collection
- Parameters requested for analysis
- Preservative used
- Field water quality parameter measurements



- Field observations on sampling event
- Name of collector(s)
- Weather conditions including air temperature and precipitation

6.8.4 Chain-of-Custody Record

The COC record is required for tracing sample possession from time of collection to time of receipt at the laboratory. The National Enforcement Investigations Center (NEIC) of USEPA considers a sample to be in custody under any of the following conditions:

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- It is in the individual's possession
- It is in the individual's view after being in his possession
- It was in the individual's possession and he locked it up
- It is in a designated secure area

All environmental samples will be handled under strict COC procedures beginning in the field. The field team leader will be the field sample custodian and will be responsible for ensuring that COC procedures are followed. A COC record will accompany each individual shipment. The record will contain the following information:

- Sample destination and transporter
- Sample identification numbers
- Signature of collector
- Date and time of collection
- Sample type
- Identification of monitoring well
- Number of sample containers in shipping container
- Parameters requested for analysis
- Signature of person(s) involved in the chain of possession
- Inclusive dates of possession

A copy of the completed COC form will be placed in a water resistant bag and accompany the shipment and will be returned to the shipper after the shipping container reaches its destination. The COC record will also be used as the analysis request sheet. When shipping by courier, the courier does not sign the COC record: copies of shipping forms are retained to document custody.

6.9 Temperature Control and Sample Transportation

After collection, sample preservation, and labeling, sample containers will be placed in coolers containing water-ice with the goal of reducing the groundwater samples to a temperature of approximately 4°C or less.



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All samples included in the shipping container will be packed in such a manner to minimize the potential for container breakage. Samples will be either hand-delivered or shipped via commercial carrier to the certified analytical laboratory. Custody seals will be placed on the shipping containers if a third party courier is used.

7.0 ANALYTICAL AND QUALITY CONTROL PROCEDURES

7.1 Data Quality Objectives

As part of the evaluation component of the Quality Assurance (QA) program, analytical results will be evaluated for precision, accuracy, representativeness, completeness, and comparability (PARCC). These are defined as follows:

■ Precision is the agreement or reproducibility among individual measurements of the same property, usually made under the same conditions

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- Accuracy is the degree of agreement of a measurement with the true or accepted value
- Representativeness is the degree to which a measurement accurately and precisely represents a characteristic of a population, parameter, or variations at a sampling point, a process condition, or an environmental condition
- Completeness is a measure of the amount of valid data obtained from a measurement system compared with the amount that was expected to be obtained under correct normal conditions
- Comparability is an expression of the confidence with which one data set can be compared with another data set in regard to the same property

The accuracy, precision and representativeness of data will be functions of the sample origin, analytical procedures and the specific sample matrices. Quality Control (QC) practices for the evaluation of these data quality indicators include the use of accepted analytical procedures, adherence to hold time, and analysis of QC samples (e.g., blanks, replicates, spikes, calibration standards and reference standards).

Quantitative QA objectives for precision and accuracy, along with sensitivity (detection limits) are established in accordance with the specific analytical methodologies, historical data, laboratory method validation studies, and laboratory experience with similar samples. The Representativeness of the analytical data is a function of the procedures used to process the samples.

Completeness is a qualitative characteristic which is defined as the fraction of valid data obtained from a measurement system (e.g., sampling and analysis) compared to that which was planned. Completeness can be less than 100 percent due to poor sample recovery, sample damage, or disqualification of results which are outside of control limits due to laboratory error or matrix-specific interferences. Completeness is documented by including sufficient information in the laboratory reports to allow the data user to assess the quality of the results. The overall completeness goal for each task is difficult to determine prior to data acquisition. For this project, all reasonable attempts will be made to attain 90% completeness or better (laboratory).

Comparability is a qualitative characteristic which allows for comparison of analytical results with those obtained by other laboratories. This may be accomplished through the use of standard accepted methodologies, traceability of standards to the National Bureau of Standards (NBS) or USEPA sources,





use of appropriate levels of quality control, reporting results in consistent, standard units of measure, and participation in inter-laboratory studies designed to evaluate laboratory performance.

Data quality and the standard commercial report package will be evaluated with respect to PARCC criteria using the laboratory's QA practices, use of standard analytical methods, certifications, participation in interlaboratory studies, temperature control, adherence to hold times, and COC documentation (also called Data Validation).

7.2 Quality Assurance/Quality Control Samples

This section describes the various Quality Assurance/Quality Control (QA/QC) samples that will be collected in the field and analyzed in the laboratory and the frequency at which they will be performed.

7.2.1 Field Equipment Rinsate Blanks

In cases where sampling equipment is not dedicated or disposable, an equipment rinsate blank will be collected. The equipment rinsate blanks are prepared in the field using laboratory-supplied analyte-free water. The water is poured over and through each type of sampling equipment following decontamination and submitted to the laboratory for analysis of target constituents. **One rinsate blank will be collected for every 10 samples.**

7.2.2 Field Duplicates

Field duplicates are collected by sampling the same location twice, but the field duplicate is assigned a unique sample identification number. Samplers will document which location is used for the duplicate sample. One field duplicate will be collected for every 10 samples.

7.2.3 Field Blank

Field blanks are collected in the field using laboratory-supplied analyte-free water. The water is poured directly into the supplied sample containers in the field and submitted to the laboratory for analysis of target constituents. One field blank will be collected for every 10 samples.

7.2.4 Laboratory Quality Control Samples

The laboratory will have an established QC check program using procedural (method) blanks, laboratory control spikes, matrix spikes, and duplicates. Details of the internal QC checks used by the laboratory will be found in the laboratory QAP and the published analytical methods. These QC samples will be used to determine if results may have been affected by field activities or procedures used in sample transportation or if matrix interferences are an issue. One (1) Matrix Spike (MS)/ Matrix Spike Duplicate (MSD) set (i.e. one sample plus one MS, and one MSD sample at one location) will be collected per 20 samples. MS/MSD samples will have a naming convention as follows:



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Sample: M-MW-1MS: M-MW-1-MSMSD: M-MW-1-MSD



8.0 DATA EVALUATION AND STATISTICAL ANALYSIS

The following sections describe the evaluation and analysis procedures that are followed upon receipt of the analytical report.

8.1 Evaluation of Rate and Direction of Groundwater Flow

Groundwater elevations will be determined for each sampling event and will be used to develop a groundwater elevation contour map that will be submitted with reports. The direction of groundwater flow will be determined from up-and downgradient relationships as depicted on the potentiometric surface map. Based on these maps, groundwater flow velocities will be estimated for each event.

8.2 Data Validation

Before the data are used for statistical analysis, they will be evaluated by examining the quality control data accompanying the data report from the laboratory. Relevant quality control data could include measures of accuracy (percent recovery), precision (relative percent difference, RPD), and sample contamination (blank determinations). Data that fail any of these checks will be flagged for further evaluation. A Data Quality Review (DQR) may be initiated with the laboratory for any anomalous data.

8.3 Statistical Analysis

Upon completion of the data validation, the data will be submitted for statistical analysis in compliance with 40 CFR §257.93. The detailed statistical analysis plan for the Facility will be included in **Appendix J**.





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TABLES

Groundwater Level Data Meramec Surface Impoundments

Meramec Energy Center, St. Louis County, MO

	Loca	tion ⁴	Top of Casing ⁷	Ground Surface ⁷	_	und Event 1 8/2016	Ü	nd Event 2 /2016		nd Event 3 /2016	Ü	nd Event 4 2016	Backgroui 11/10	nd Event 5 /2016	· ·	nd Event 6 2017	Backgroui 3/7/	nd Event 7 2017	Ü	nd Event 8 /2017
Well ID	Northing	Easting	Feet MSL ⁵	Feet MSL ⁵	DTW ³	GWE ⁴	DTW ³	GWE ⁴	DTW ³	GWE ⁴	DTW ³	GWE ⁴	DTW ³	GWE ⁴	DTW ³	GWE ⁴	DTW ³	GWE ⁴	DTW ³	GWE ⁴
MW-1	937676.9	865954.1	406.43	404.1	4.83	401.60	2.61	403.82	5.57	400.86	4.72	401.71	5.36	401.07	7.08	399.35	5.55	400.88	2.46	403.97
MW-2	937325.1	864864.5	398.62	396.1	12.76	385.86	3.54	395.08	14.79	383.83	11.69	386.93	16.42	382.20	19.10	379.52	13.25	385.37	7.72	390.90
MW-3	936750.8	864447.2	397.12	394.6	11.30	385.82	2.07	395.05	13.27	383.85	10.15	386.97	14.93	382.19	17.62	379.50	11.81	385.31	6.23	390.89
MW-4	935618.0	864629.8	404.10	402.0	18.17	385.93	9.13	394.97	20.02	384.08	16.48	387.62	21.65	382.45	24.43	379.67	18.93	385.17	13.08	391.02
MW-5	934874.4	864781.0	402.93	400.8	16.94	385.99	7.93	395.00	18.67	384.26	15.65	387.28	20.27	382.66	23.14	379.79	17.83	385.10	11.69	391.24
MW-6	933905.2	865153.5	418.12	415.8	32.26	385.86	23.33	394.79	33.56	384.56	30.56	387.56	35.11	383.01	38.29	379.83	33.64	384.48	26.49	391.63
MW-7	934334.4	866242.5	417.94	415.7	32.01	385.93	23.04	394.90	33.32	384.62	30.37	387.57	34.68	383.26	37.79	380.15	33.52	384.42	26.39	391.55
MW-8	935303.6	866797.8	423.37	421.0	36.68	386.69	27.46	395.91	38.07	385.30	35.14	388.23	39.60	383.77	42.59	380.78	37.57	385.80	31.27	392.10
BMW-1	935220.4	867989.4	419.08	416.8	24.40 ⁸	396.72 ⁸	19.78	399.30	28.16	390.92	24.96	394.12	27.41	391.67	32.64	386.44	28.51	390.57	22.49	396.59
BMW-2	937927.1	866342.2	409.02	406.8	14.21	394.81	11.22	397.80	15.45	393.57	14.58	394.44	15.36	393.66	17.29	391.73	15.71	393.31	11.39	397.63
Mississippi River	934893.52 ²	868520.62 ²	NA	NA	NA	386.59	NA	395.52	NA	384.25	NA	387.53	NA	382.37	NA	380.70	NA	385.77	NA	390.10

Notes:

1.) Groundwater monitoring wells surveyed by Zahner & Associates, Inc. on February 4, 2016 and April 28, 2016.

- 2.) * Mississippi River gauge location is estimated.
- 3.) DTW Depth to water measured in feet below top of casing.
- 4.) GWE Groundwater elevation measured in feet above mean sea level.
- 5.) MSL Feet above mean sea level.
- 6.) Horizontal Datum: State Plane Coordinates NAD83 (2000) Missouri East Zone feet.
- 7.) Vertical Datum: NAVD88 feet.
- 8.) Groundwater elevation data based on orginal BMW-1 location that has been abandoned.
- 9.) NA Not Applicable.
- 10.) Mississippi River Level is provided by Ameren.

Prepared JSI Check JS/RJF Reviewed MNH

Generalized Hydraulic Properties of Uppermost Aquifer Meramec Surface Impounments Meramec Energy Center, St. Louis County, MO

	Meramec Monitoring Wells												
	(MW-2, MW-3, MW-4, MW-5, MW-6, MW-7, MW-8, BMW-1, BMW-2)												
		Average	Estimated	Mean	Mean		Estimated						
Baseline	Baseline	Groundwater	Hydraulic	Hydraulic	Hydraulic	Estimated	Groundwater						
Sampling	Sampling	Flow Direction	Gradient	Conductivity	Conductivity	Effective	Velocity						
Event	Event Date	(Azimuth)	(Feet/Foot)	(Feet/Day)	(cm/sec)	Porosity	(Feet/Day)						
1	3/28/2016	232.5	0.0022	37.02	1.3E-02	0.35	0.23						
2	5/13/2016	249.1	0.0012	37.02	1.3E-02	0.35	0.13						
3	7/18/2016	240.1	0.0025	37.02	1.3E-02	0.35	0.27						
4	9/7/2016	244.8	0.0022	37.02	1.3E-02	0.35	0.23						
5	11/10/2016	242.3	0.0032	37.02	1.3E-02	0.35	0.34						
6	1/6/2017	233.9	0.0030	37.02	1.3E-02	0.35	0.31						
7	3/7/2017	230.9	0.0023	37.02	1.3E-02	0.35	0.24						
8	6/14/2017	244.0	0.0019	37.02	1.3E-02	0.35	0.20						

Estimated Results (USEPA Tool)						
Resultant Groundwater Flow Direction	239					
(Azimuth)						
Estimated Annual Net Groundwater Movement (Feet/Year)	87					

Prepared By: JSI Checked By: JS/RJF Reviewed By:

Notes:

- 1. Azimuth and Hydraulic Gradient calculated using the United States Environmental protection agency (USEPA) On-Line Tools for Site Assessment Calculation for Hydraulic Gradient (magnitude and direction) available at https://www3.epa.gov/ceampubl/learn2model/part-two/onsite/gradient4plus-ns.html
- 2. Hydraulic conductivity value is the geometric mean of slug test results for the Meramec monitoring wells (except MW-1).
- 3. An effective porosity of 0.35 was used based on grain size distributions and published values (Fetter 2000, Cohen 1953, and Johnson 1967).
- 4. Azimuth is measured clockwise in degrees from north.
- 5. cm/sec Centimeters per second.

Monitoring Well Construction Details Meramec Surface Impoundments Meramec Energy Center, St. Louis County, MO

		Location ⁴		Top of Casing Elevation	Ground Surface Elevation	Top of Screen	Bottom of Screen	Base of Well	Total Depth
Well ID	Date Installed	Northing	Easting	(FT MSL) ⁵	(FT MSL) ⁵	(FT MSL) ⁵	(FT MSL) ⁵	(FT MSL) ⁵	(FT BGS) ⁵
MW-1	1/23/2016	937676.9	865954.1	406.43	404.1	370.2	365.4	365.0	39.1
MW-2	1/23/2016	937325.1	864864.5	398.62	396.1	367.0	362.2	361.8	34.3
MW-3	1/22/2016	936750.8	864447.2	397.12	394.6	369.2	364.4	364.0	30.6
MW-4	1/22/2016	935618.0	864629.8	404.10	402.0	364.1	359.3	358.9	43.1
MW-5	1/22/2016	934874.4	864781.0	402.93	400.8	350.4	340.6	340.2	60.6
MW-6	1/21/2016	933905.2	865153.5	418.12	415.8	373.4	363.6	363.2	52.7
MW-7	1/24/2016	934334.4	866242.5	417.94	415.7	373.2	363.4	363.0	52.7
MW-8	1/24/2016	935303.6	866797.8	423.37	421.0	355.8	346.0	345.6	75.4
BMW-1	4/7/2016	935220.4	867989.4	419.08	416.8	366.4	356.6	356.2	60.6
BMW-2	1/25/2016	937927.1	866342.2	409.02	406.8	369.3	364.5	364.1	42.7

Notes:

- 1.) All elevations and coordinates were surveyed on January 14, and April 28th, 2016 by Zahner and Associates, Inc.
- 2.) FT MSL = Feet Above Mean Sea Level.
- 3.) FT BGS = Feet Below Ground Surface.
- 4.) Horizontal Datum: State Plane Coordinates NAD83 (2000) Missouri East Zone Feet.
- 5.) Vertical Datum: NAVD88 Feet.

Prepared By: JSI Checked By: JS Reviewed By: MNH

Groundwater Quality Monitoring Parameters Meramec Surface Impoundments Meramec Energy Center, St. Louis County, MO

	Monitoring Parameter	Background ²	Detection ³	Assessment ⁴
Field Parameters	Temperature, pH, Conductivity and Dissolved Oxygen	Х	Х	Х
	Boron	X	Х	X
	Calcium	Х	Х	Х
	Chloride	Х	Х	Х
Appendix III ¹	Fluoride	Х	Х	Х
	Sulfate	Х	Х	Х
	рН	Х	Х	Х
	Total Dissolved Solids (TDS)	Х	Х	Х
	Antimony	X		Х
	Arsenic	Х		Х
	Barium	Х		Х
	Beryllium	Х		Х
	Cadmium	Х		Х
	Chromium	X		Х
	Cobalt	Х		Х
Appendix IV ¹	Fluoride	Х		Х
	Lead	Х		Х
	Lithium	Х		Х
	Mercury	Х		Х
	Molybdenum	Х		Х
	Selenium	Х		Х
	Thallium	Х		Х
	Radium 226 & 228	Х		Х

Notes:

- 1.) Analyte lists match requirements for monitoring from USEPA Rule 40 CFR parts 257 and 261.
- 2.) Background will be performed through October 2017 until at least 8 samples are collected.
- 3.) Approximately 6 months will separate each semi-annual sampling event.
- 4.) If necessary, assessment monitoring will be performed in accordance with USEPA Rule.

Prepared By: JS Checked By: MWD Reviewed By: MNH

Analytical Methods and Practical Quantitation Limits Meramec Surface Impoundments Meramec Energy Center, St. Louis County, MO

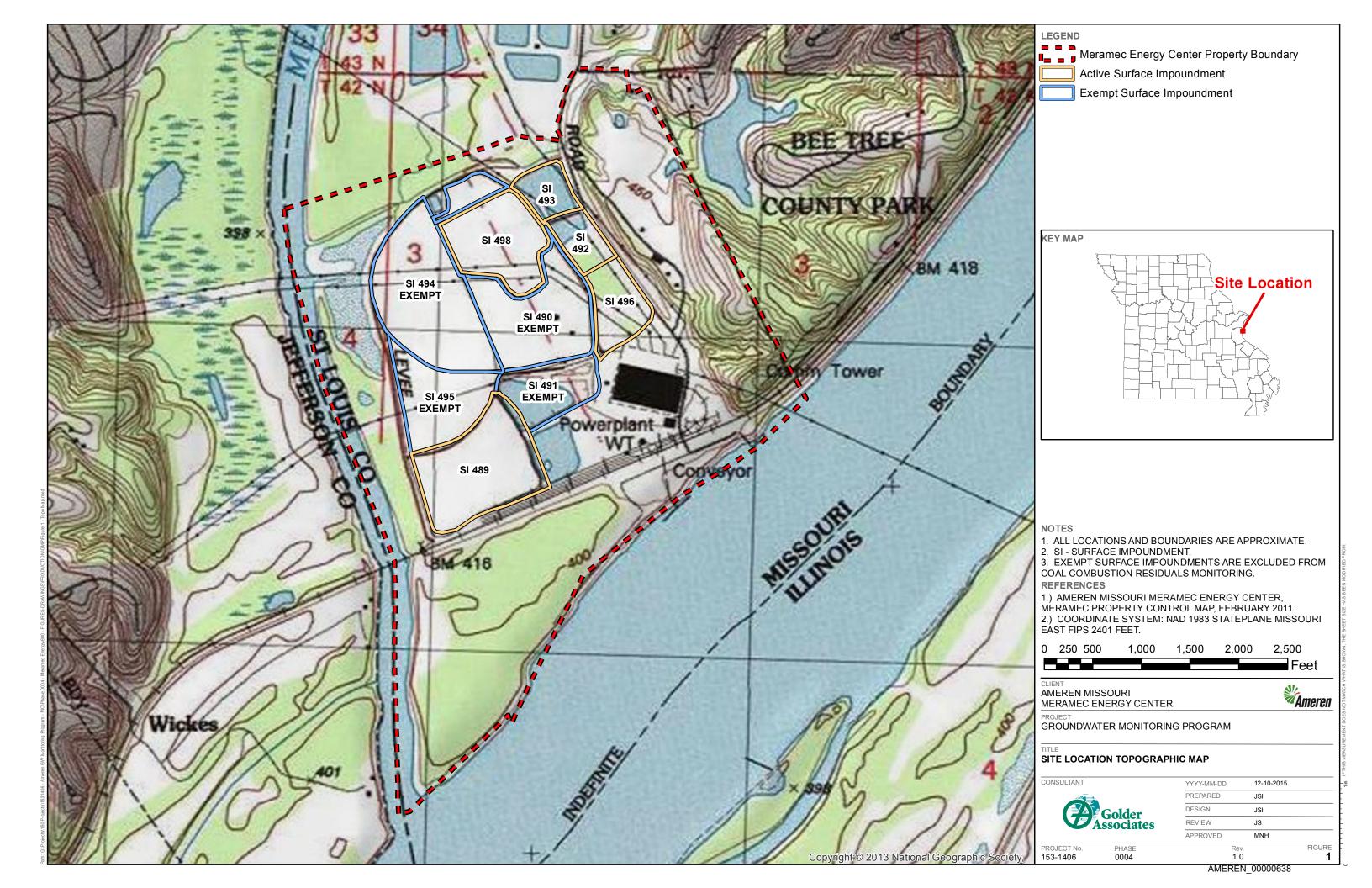
Analyte	Method Reference	Preservative	Hold Times	PQL (μg/L)	MCL (mg/L)
Appendix III - Detection Moni	itoring				
Boron	SW-846 6010/MCAWW 200.7	HNO3	6 months	20.0	NA
Calcium	SW-846 6010/MCAWW 200.7	HNO3	6 months	500.0	NA
Chloride	EPA 300.0/325.5/MCAWW 300/SW846 9251/9056	NA	28 days	500.0	NA
Fluoride	EPA 300.0, 300.1	NA	28 days	-	4
рН	4500 H+B-2000	NA	NA	-	NA
Sulfate	EPA 300.0/SW846 300	NA	28 days	2000.0	NA
Total Dissolved Solids (TDS)	2540 C-1997/SM18-20 2540 C	NA	7 days	10000.0	NA
Appendix IV - Assessment Mo	onitoring	•		•	
Antimony	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.006
Arsenic	nic SW-846 6010/6020/MCAWW 200.7/200.8		6 months	1.0	0.01
Barium	Barium SW-846 6010/6020/MCAWW 200.7/200.8		6 months	2.0	2
Beryllium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.004
Cadmium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	0.5	0.005
Chromium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.5	0.1
Cobalt	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	4.0	NP
Fluoride	EPA 300.0	N/A	28 days	-	4
Lead	SW-846 6020	HNO3	6 months	0.005	0.015
Lithium	SW-846 6010		6 months	-	NA
Mercury	SW-846 7470	HNO3	28 days	-	0.002
Molybdenum	SW-846 6010		6 months	-	NP
Selenium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.05
Thallium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	0.2	0.002
Radium 226 & 228	SW-846 903.1/SM 6500 904	-	-	1.0 (pCi/L)	5.0 (pCi/L)

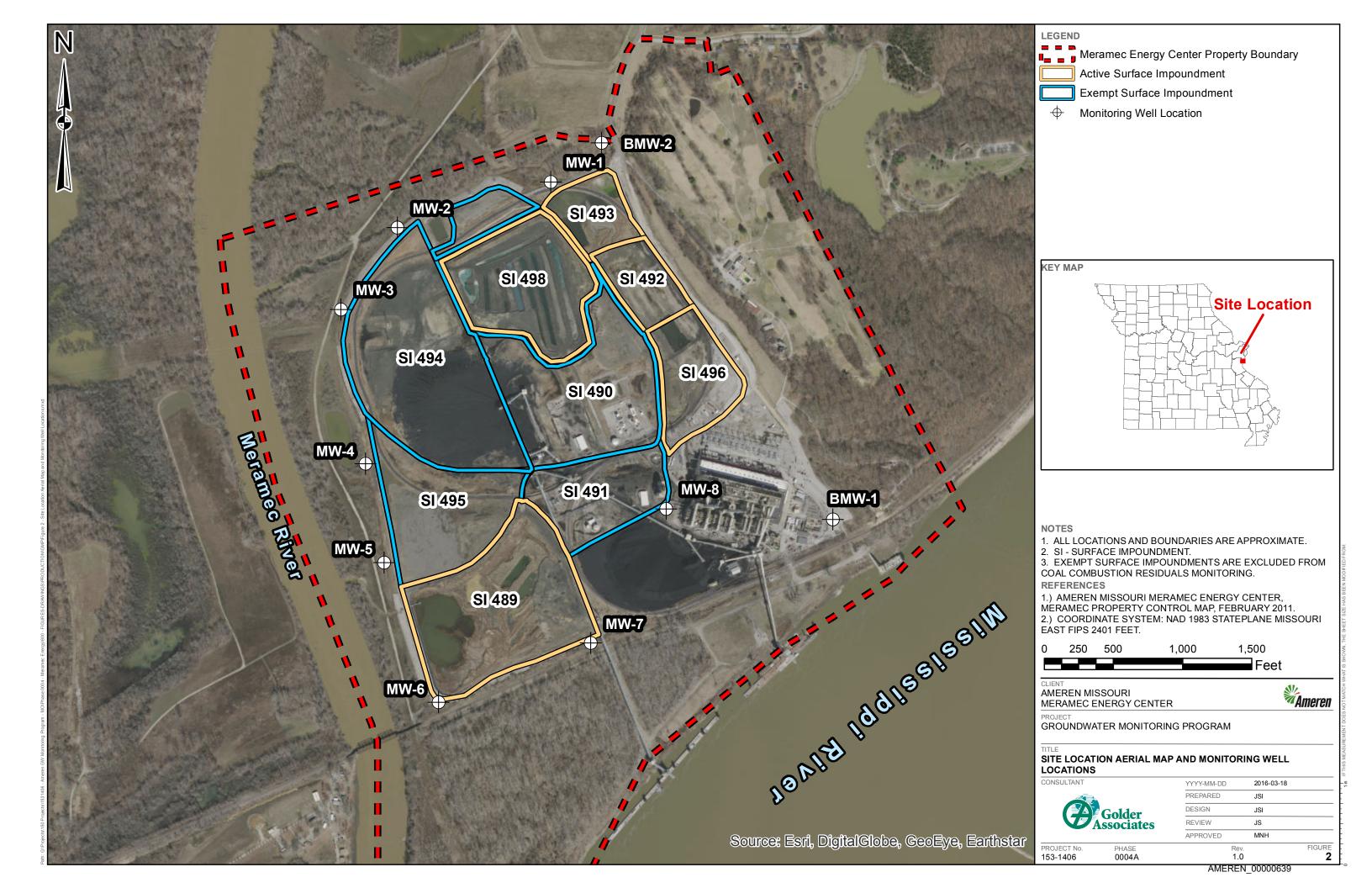
Notes:

- 1.) NA not applicable.
- 2.) Analyte lists matches requirements for detection and assessment monitoring from United States Environmental Protection Agency (USEPA) Rule 40 CFR parts 257 and 261.
- 3.) SW-846 denotes Test Methods for Evaluating Solid Waste, Physical- Chemical Methods, EPA publication SW-846, 3rd edition, and subsequent updates.
- 4.) MCAWW denotes Methods for the Chemical Analysis of Water and Wastes (MCAWW), United States Environmental Protection Agency (USEPA) published in the 1983.
- 5.) EPA 300 denotes Methods for the Determination of Organic Compounds in Drinking Water Environmental Monitoring Systems Laboratory, Office of Research and Development, USEPA, Cincinnati, Ohio 45268. EPA-300/4-88/039, December 1988 (Revised July 1991).
- 6.) SM18-20 denotes Standard Methods for the Examination of Water and Wastewater, 18th, 19th, and 20th Editions, published by the American Public Health Association, Water Environment Federation, and the American Water Works Association.
- 7.) Other industry-used or agency-approved methods may be used provided that they produce the necessary level of precision and accuracy for data use and reporting.
- 8.) Updates to the methods listed here are approved for use.
- 9.) PQL Practical Quantitation Limit.
- 10.) MCL Maximum Contaminant Level from USEPA 2014 Edition of the Drinking Water Standards and Health Advisories. October 2014. http://water.epa.gov/drink/contaminants/index.cfm.
- 11.) Dash (-) Indicates no information available.
- 12.) μg/L Micrograms per liter.
- 13.) pCi/L Picocuries per liter.
- 14.) NP Not Promulgated.15.) mg/L Milligrams per liter.

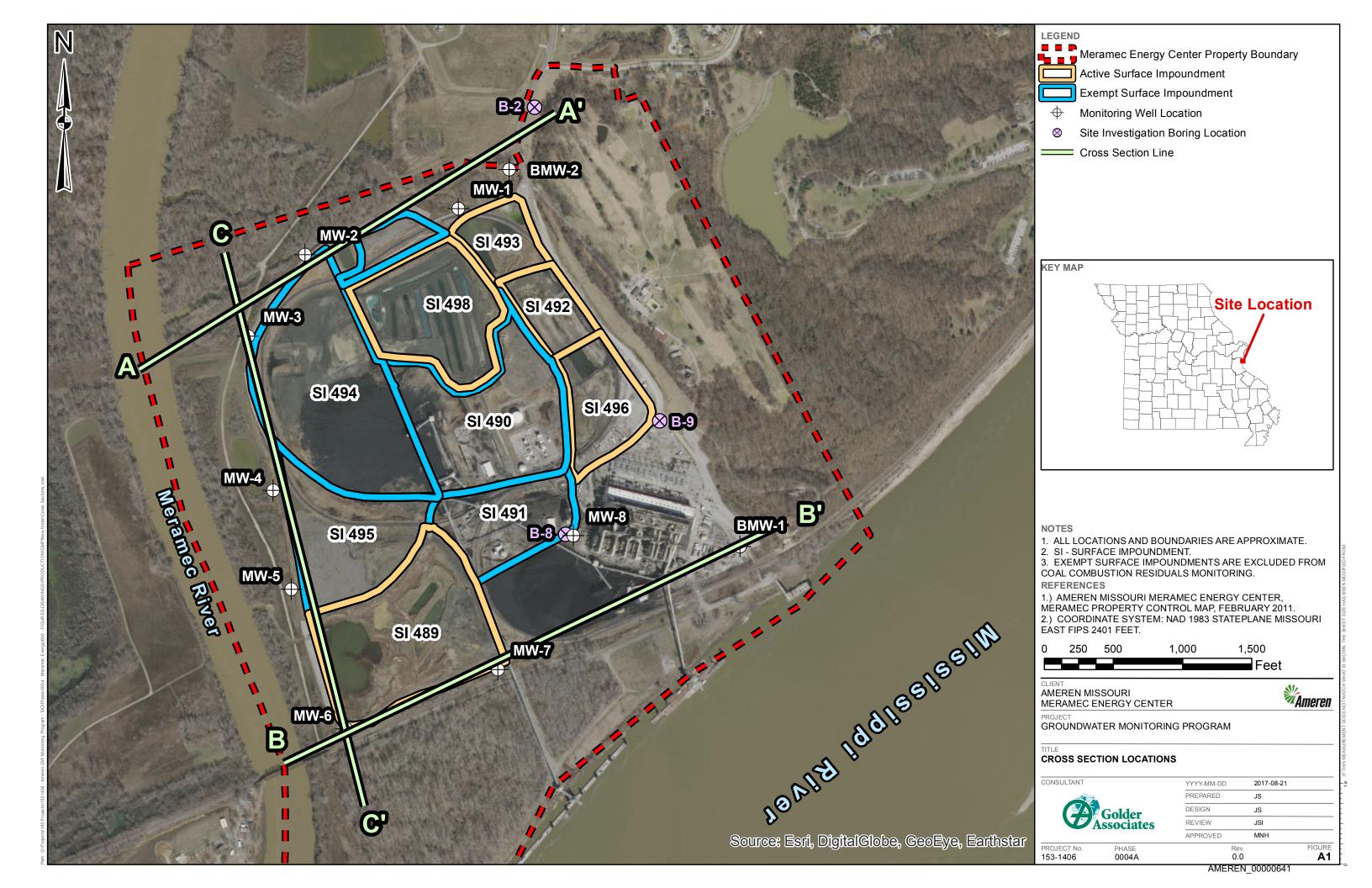
Prepared By: JS Checked By: JSI Reviewed By: MNH

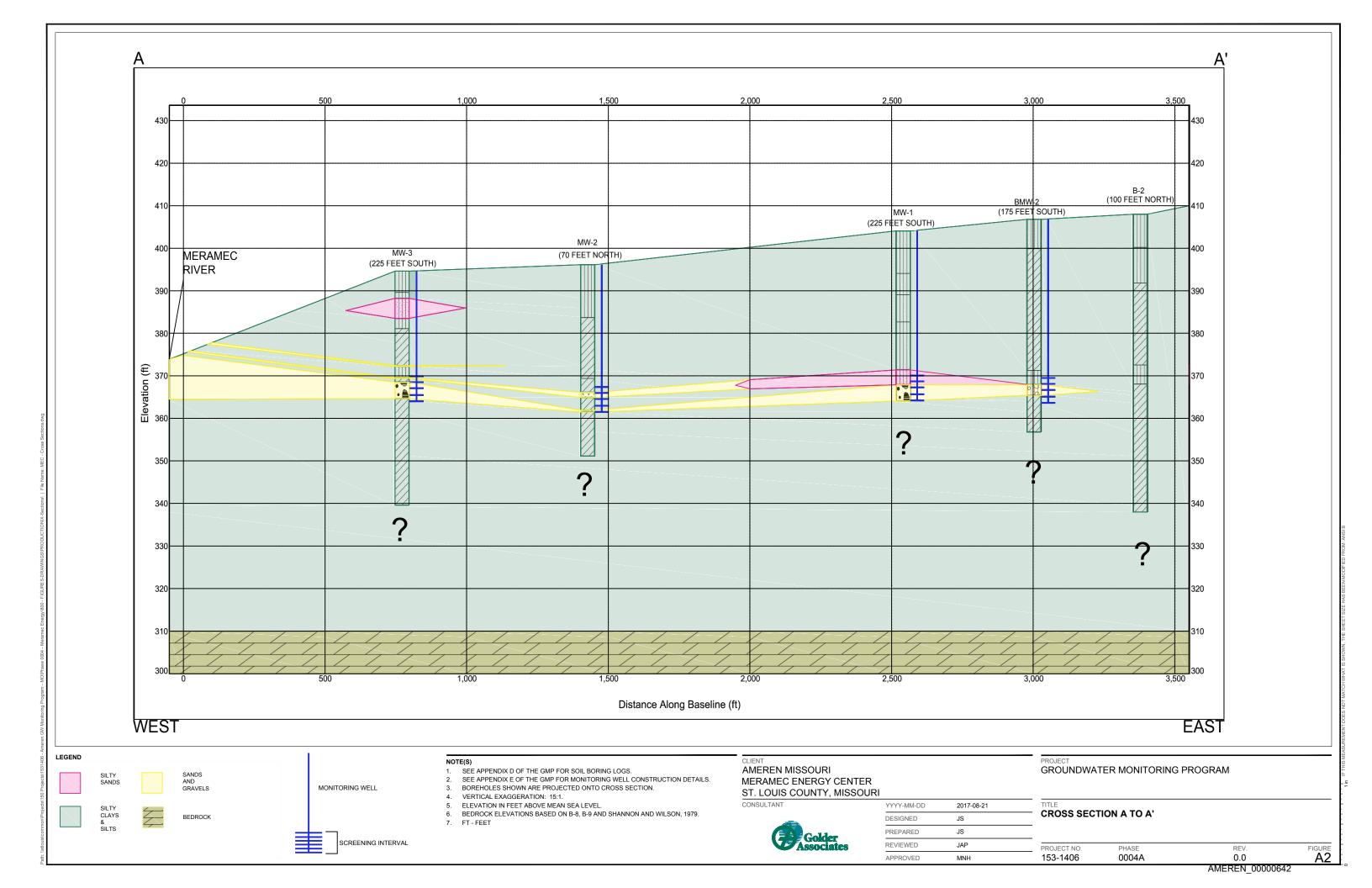
FIGURES

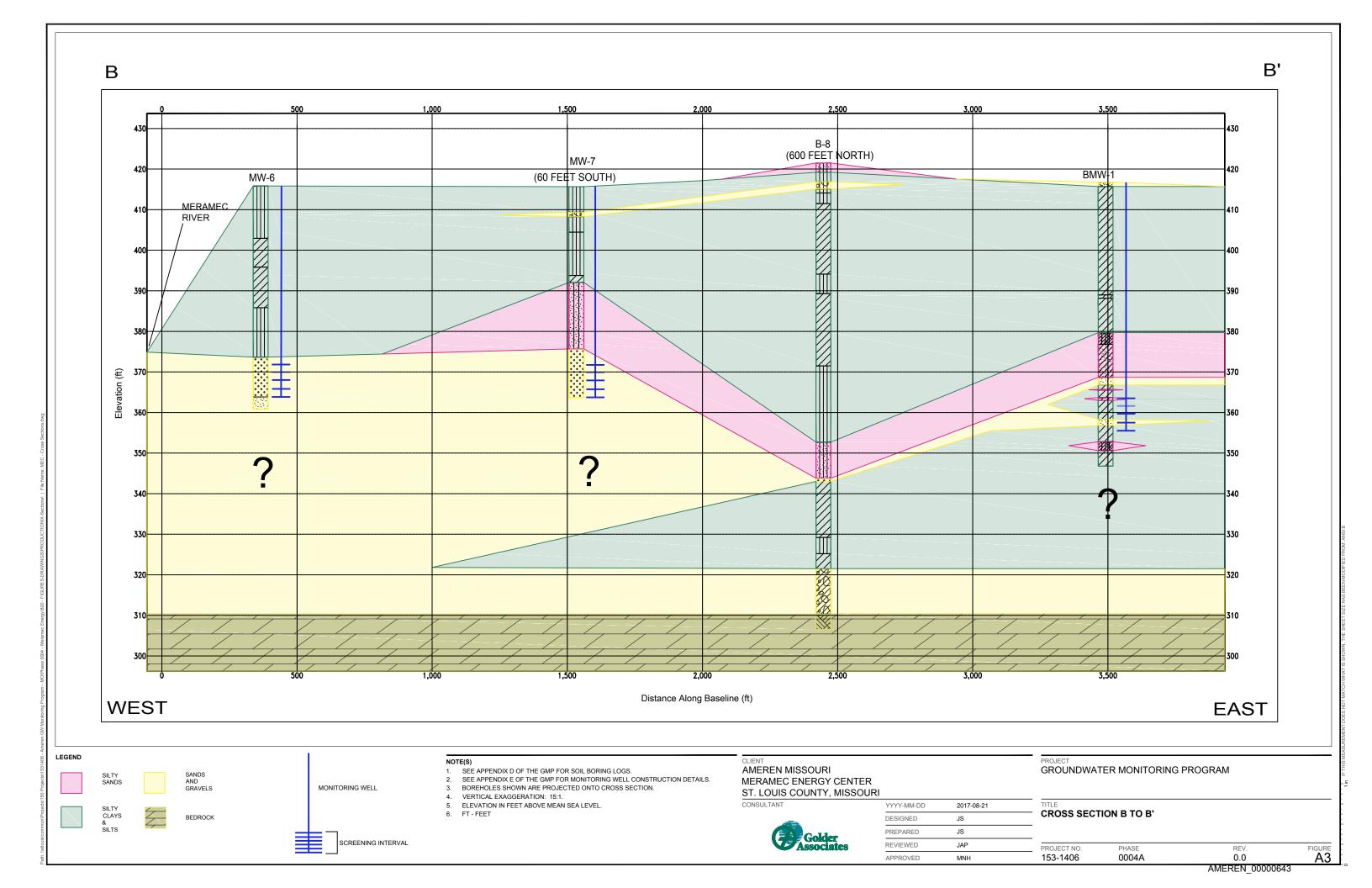


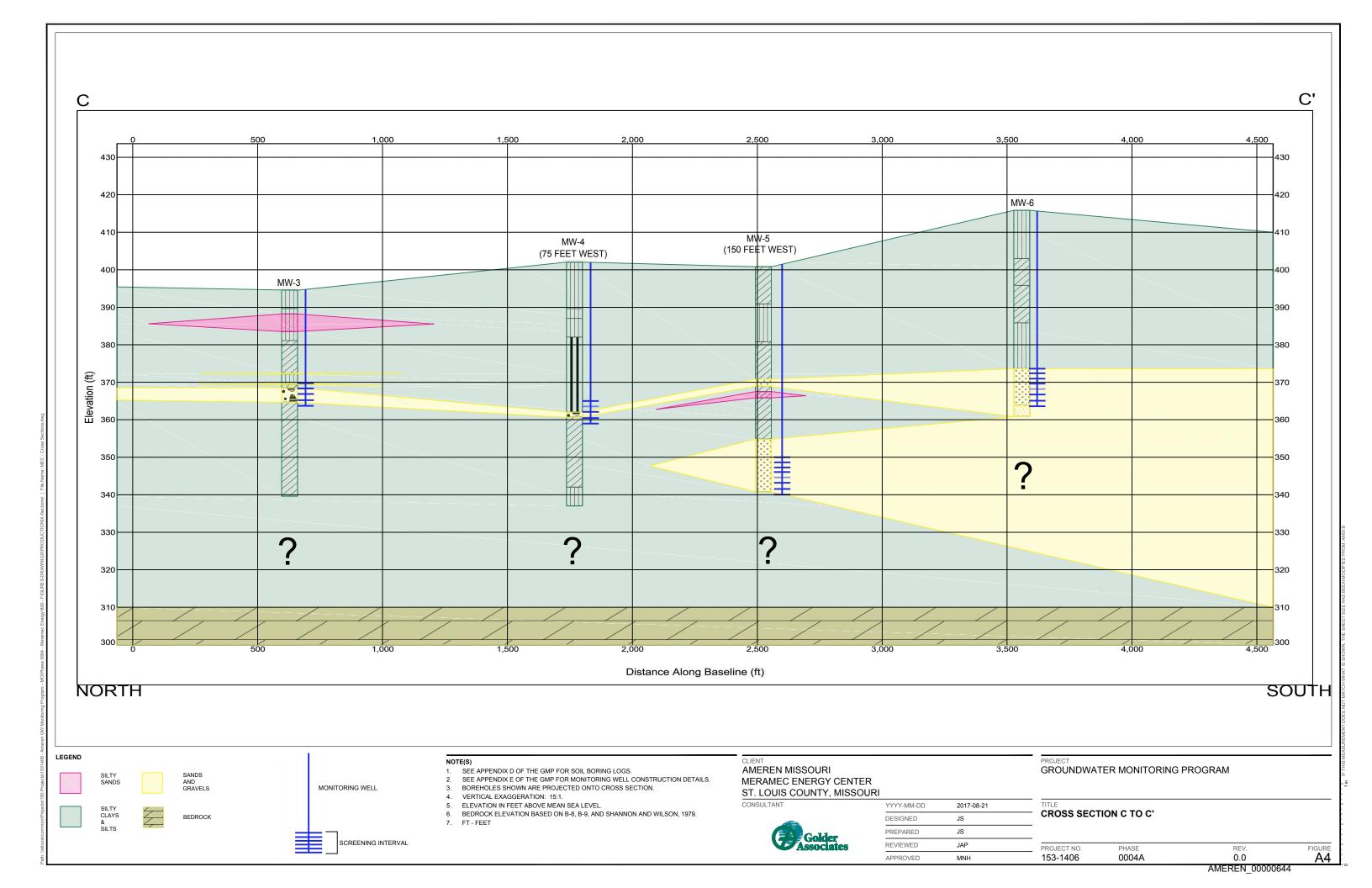


APPENDIX A CROSS SECTIONS

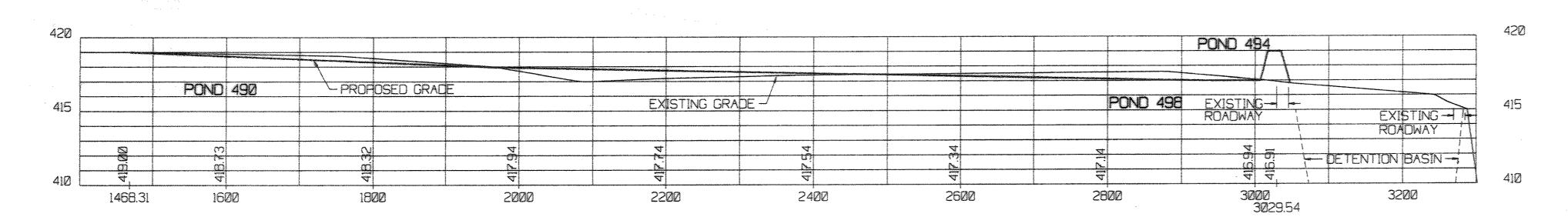




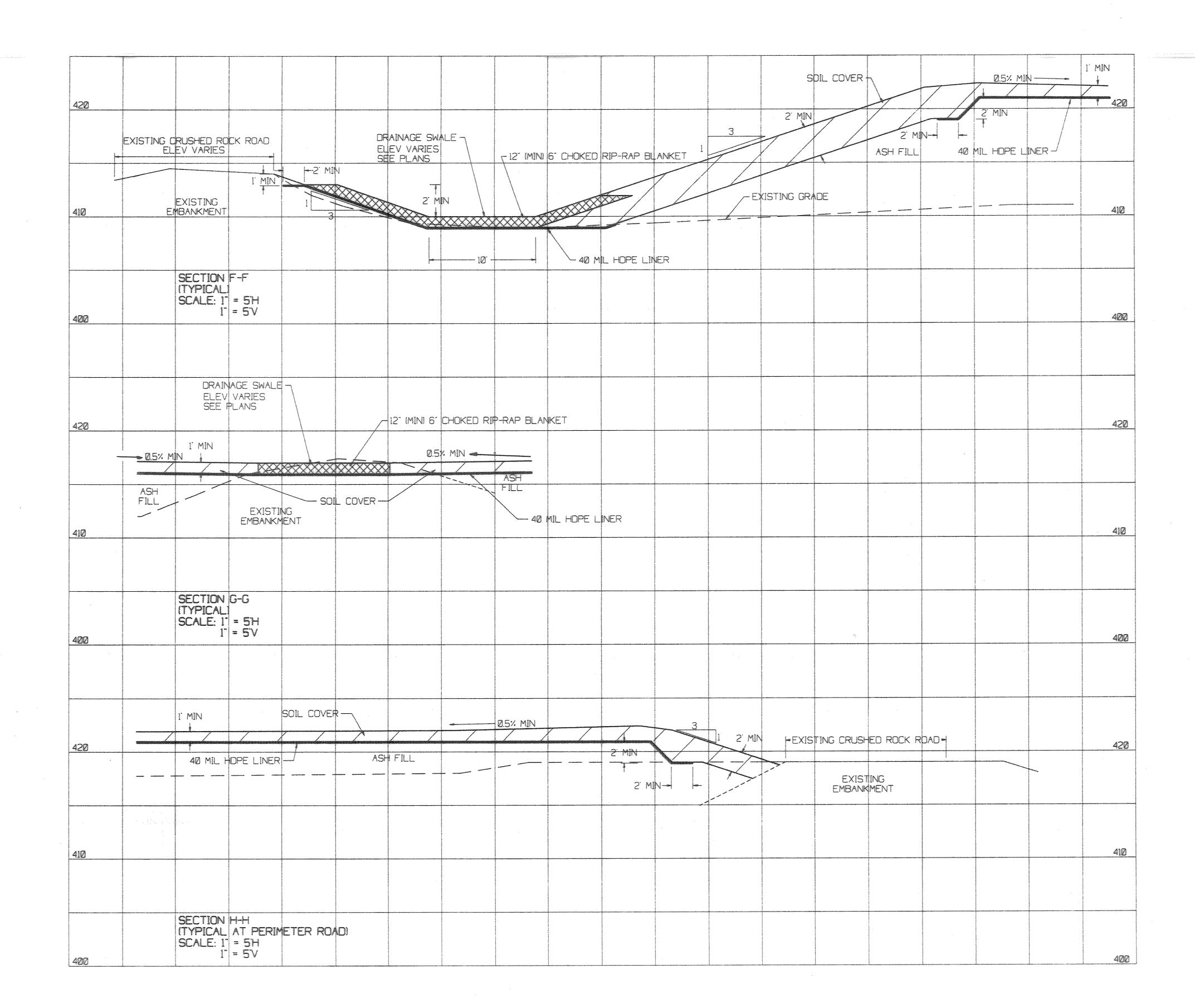


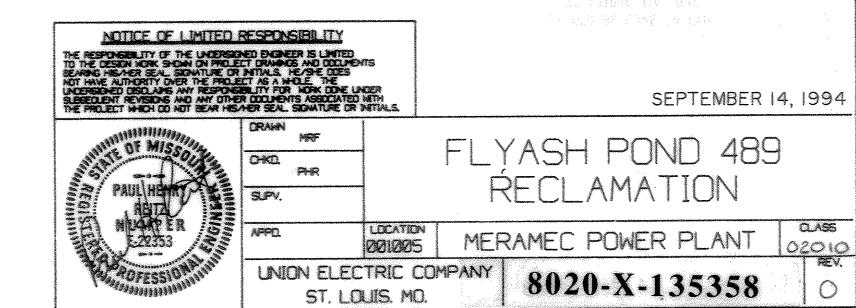


EXISTING AMEREN SUR	APPENDIX B	IDMENT DRAWIN	IGS



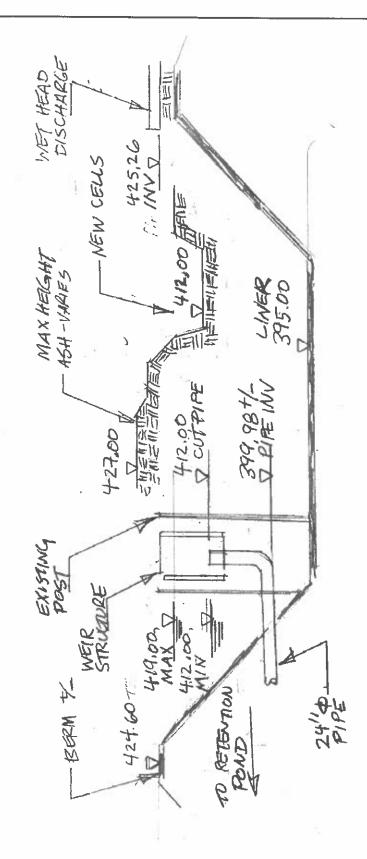
SECTION E-E (ROAD PROFILE) SCALE I" = 100H I" = 5'V





SHEET 3 OF 3

AMEREN_00000646



MR-DWG-FPD-000006-002

21-Oct-11 21-Oct-11 07-Nov-11 00 01 02

Release for AMS review Release for Ameren review Revised

Meramec Power Station 8200 Fine Road St. Louis, Missouri 63129



Ash Pond No. 498 Hydraulic profile

SK-005-R2

APPENDIX C HISTORICAL HYDROGEOLOGICAL AND RIVER LEVEL INFORMATION

Excerpts From Woodward-Clyde Consultants, 1988

TABLE 1
WATER LEVEL ELEVATIONS (FT MSL)

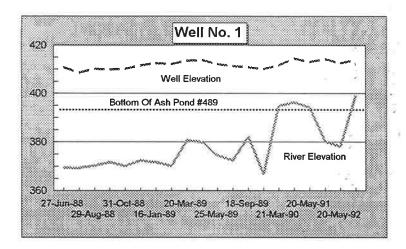
Date	Boring	g Bori	na Danin	- 0- 1		•	785	
(1988)	B-1	B-2		Boring B-4	Boring B-5	Boring B-6	Boring B-7	Mississippi River Level
1/11	413.3 (ATD)			v		ş		376.7
1/12								376.9
1/13				8				377.2
1/14			376.5 (ATD)					376.9
1/15								377.1
1/16						9		376.1
1/17								375.9
1/18		S ₄		381.7 (ATD)		8 0 886 8		376.5
1/19		<u> • </u>			390.1 (ATD)			377.1
1/20					377.1			379.3
1/21					381.1			382.2
1/22				380.7		390.3	DRY	381.9
1/23						(ATD)	(ATD)	001.7
1/24					W			382.9
1/25								382.5
1/26					a			381.4
								380.7
1/27					ň.		9	379.2
1/28			379.8	380.2	380.5	379.3	DRY	379.4
1/30						8		379.4
								379.8
1/3 ₁ 2/ ₁	412.8	403.5	. 379.4	379.7	379.8	379.8	DRY	379.7
-/1								381.8

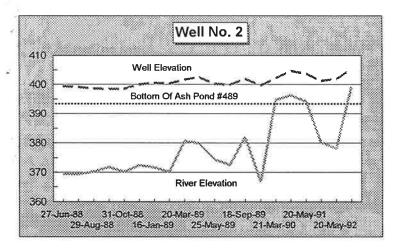
TABLE 1 (continued) WATER LEVEL ELEVATIONS (FT MSL)

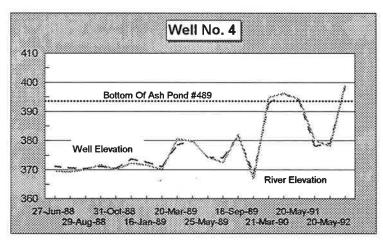
							,		
Date (1988	Boring B-1	g Boring B-2	Boring B-3	Boring B-4	Boring B-5	Boring B-6	Boring B-7	Mississippi River Level	
2/2						_		385.3	
2/3									
2/4				ę.				385.3	
2/5	414.8	404.3	385.1	385.0	204.0	204.0		384.7	
2/6			333,1	303.0	384.9	384.8	DRY	383.7	
2/7								382.7	
								380.6	
2/8								379.8	
2/9	413.9			380.7	380.6	380.6	DRY	380.2	
2/10					2	4.		379.0	
2/11								379.3	
2/12							-7		
2/13								378.7	
2/14					. 3			377.9	
2/15								378.0	
2/16								378.4	
			N		â.			377.7	
2/17	413.4	403.7		379.2	379.1	379.1	DRY	377.8	
NOTEC								· · • =	

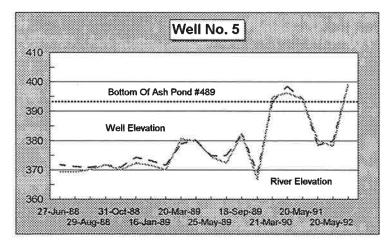
NOTES: 1. ATD = at time of drilling

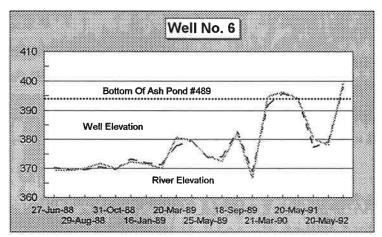
^{2.} Mississippi River elevation for site is approximate; value was calculated by linear interpolation between measured reiver levels at Jefferson Barracks, which is approximately 7.2 miles upstream from the site; and Waters Point which is approximately 3.0 river miles downstream from the site (U.S. Army Corps of Engineers data). There was generally about a four to five foot difference in elevation between the river level at Jefferson Barracks and the river level at Waters Point.



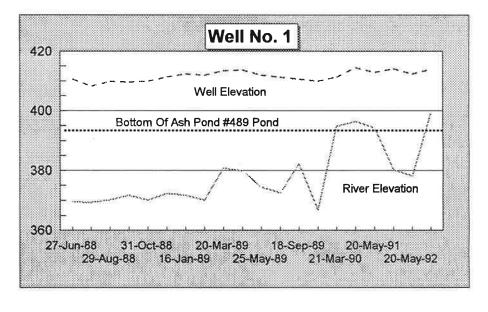




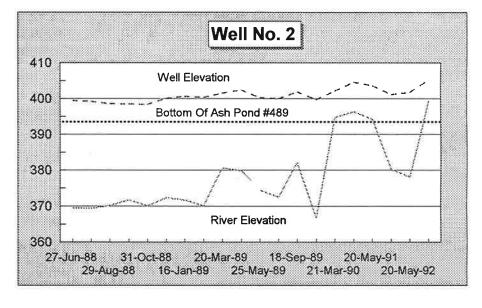




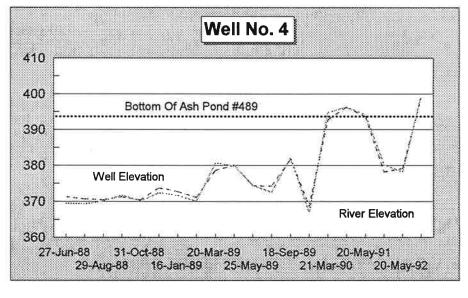
Date	Time	Well Number	Well Water Level	River Water Level
27-Jun-88	1110	1	410.63	369.48
25-Jul-88	1100	1	408.31	369.36
29-Aug-88	1125	1	409.92	370.18
26-Sep-88	1055	1	409.69	371.74
31-Oct-88	950	1	409.96	370.14
05-Dec-88	920	1	411.39	372.38
16-Jan-89	925	1	412.37	371.68
13-Feb-89	930	1	411.96	370.08
20-Mar-89	820	1	413.46	380.68
17-Apr-89	1030	1	413.63	379.85
25-May-89	1230	1	411.89	374.43
26-Jun-89	1030	1	411.22	372.53
18-Sep-89	1042	1	410.57	382.13
12-Dec-89	1000	1 **	410.03	366.74
21-Mar-90	1008	1	411.39	394.78
13-Jun-90	1022	1	414.34	396.33
20-May-91	1007	1	412.84	394.18
21-Nov-91	857	1	414.06	380.23
20-May-92	840	1	412.36	378.15
14-Jun-93	853	1	413.87	399.28



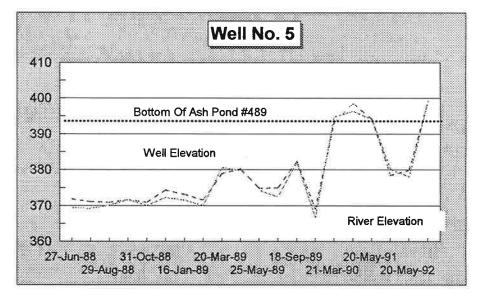
Date	Time	Well Number	Well Water Level	River Water Level
27-Jun-88	1350	2	399.43	369.48
25-Jul-88	1310	2	399.16	369.36
29-Aug-88	1305	2	398.55	370.18
26-Sep-88	1310	2	398.53	371.74
31-Oct-88	1040	2	398.44	370.14
05-Dec-88	1100	2	400.08	372.38
16-Jan-89	1040	2	400.59	371.68
13-Feb-89	1015	2	400.37	370.08
20-Mar-89	915	2	401.54	380.68
17-Apr-89	1220	2	402.41	379.85
25-May-89	1300	2	400.30	374.43
26-Jun-89	1115	2	399.97	372.53
18-Sep-89	1110	2	401.90	382.13
12-Dec-89	1036	2	399.71	366.74
21-Mar-90	1040	2	402.17	394.78
13-Jun-90	1050	2	404.58	396.33
20-May-91	1041	2	403.60	394.18
21-Nov-91	1022	2	401.12	380.23
20-May-92	940	2	401.78	378.15
14-Jun-93	927	2	405.22	399.28



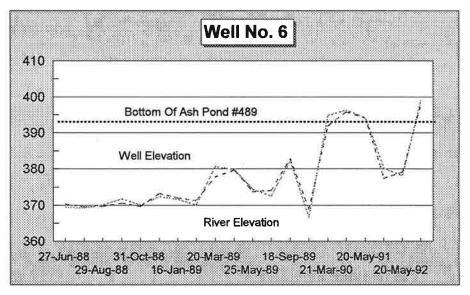
Date	Time	Well Number	Well Water Level	River Water Level
27-Jun-88	1500	4	371.28	369.48
25-Jul-88	1505	4	370.67	369.36
29-Aug-88	1455	4	370.48	370.18
26-Sep-88	1440	4	371.28	371.74
31-Oct-88	1305	4	370.46	370.14
05-Dec-88	1300	4	373.73	372.38
16-Jan-89	1330	4	372.66	371.68
13-Feb-89	1230	4	371.14	370.08
20-Mar-89	1215	4	378.63	380.68
17-Apr-89	1305	4	380.08	379.85
25-May-89	1400	4	374.37	374.43
26-Jun-89	1300	4	374.22	372.53
18-Sep-89	1304	4	381.73	382.13
12-Dec-89	1214	4	368.62	366.74
21-Mar-90	1120	4	392.72	394.78
13-Jun-90	1244	4	396.28	396.33
20-May-91	1242	4	393.61	394.18
21-Nov-91	1317	4	378.22	380.23
20-May-92	1243	4	379.17	378.15
14-Jun-93	1007	4	398.67	399.28



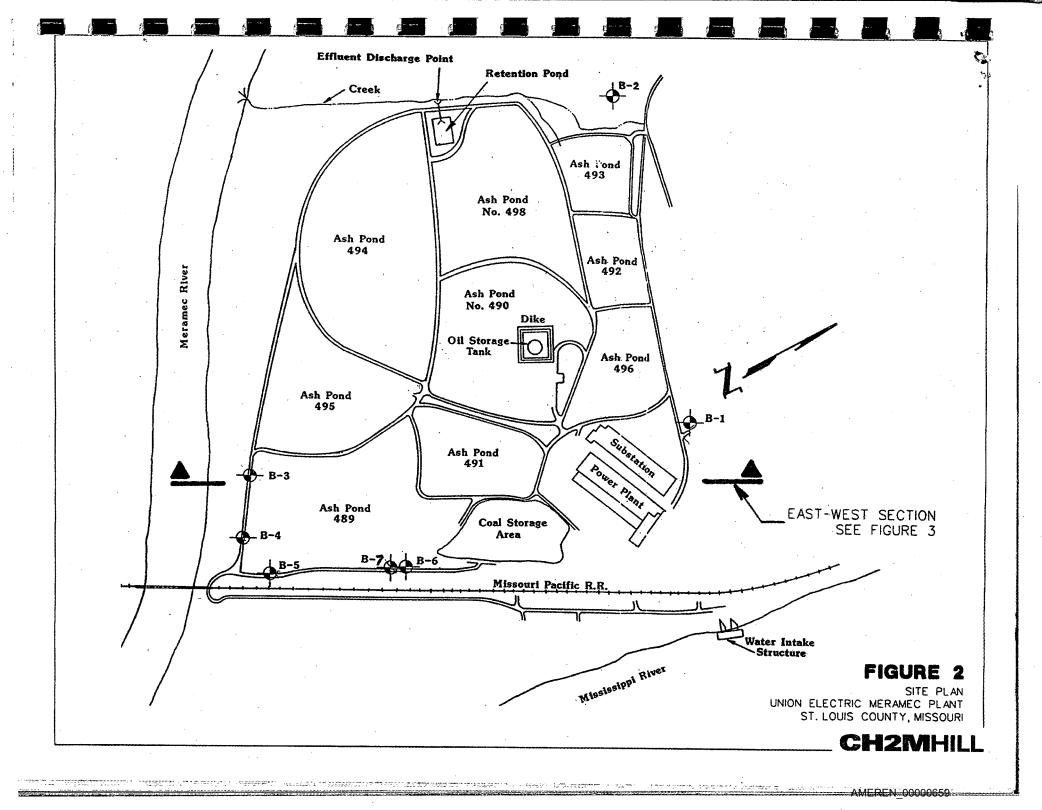
Date	Time	Well Number	Well Water Level	River Water Level
27-Jun-88	1610	5	371.89	369.48
25-Jul-88	1550	5	371.16	369.36
29-Aug-88	1550	5	370.99	370.18
26-Sep-88	1605	5	371.78	371.74
31-Oct-88	1350	5	370.98	370.14
05-Dec-88	1320	5	374.41	372.38
16-Jan-89	1415	5	373.25	371.68
13-Feb-89	1415	5	371.68	370.08
20-Mar-89	1305	5	378.98	380.68
17-Apr-89	1545	5	380.26	379.85
25-May-89	1430	5	374.96	374.43
26-Jun-89	1340	5	375.06	372.53
18-Sep-89	1334	5	382.33	382.13
12-Dec-89	1253	5 🐃	369.12	366.74
21-Mar-90	1143	5	393.14	394.78
13-Jun-90	1305	5	398.52	396.33
20-May-91	1317	5	394.24	394.18
21-Nov-91	1354	5	378.55	380.23
20-May-92	1336	5	379.91	378.15
14-Jun-93	1035	5	399.21	399.28

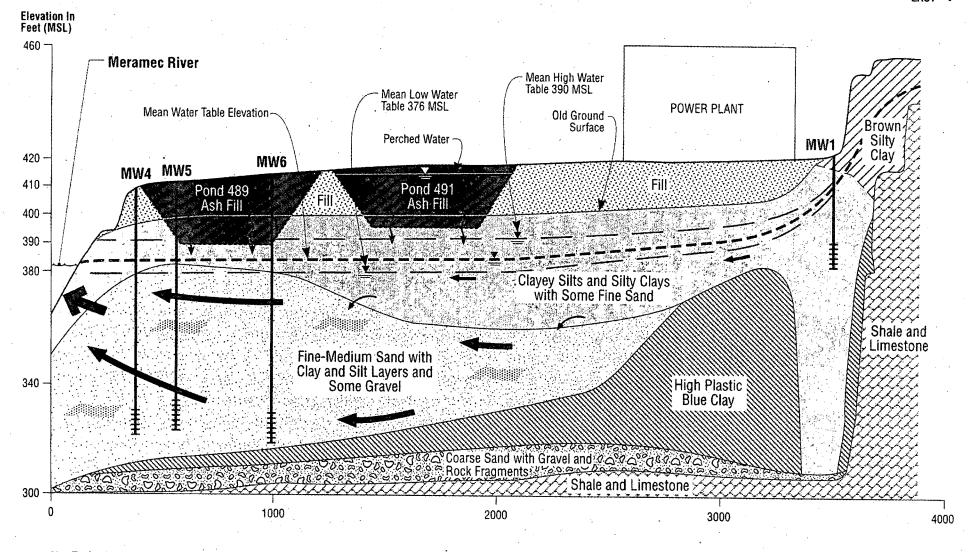


Date	Time	Well Number	Well Water Level	River Water Level
27-Jun-88	1705	6	370.38	369.48
25-Jul-88	1705	6	369.62	369.36
29-Aug-88	1705	6	369.73	370.18
26-Sep-88	1705	6	370.61	371.74
31-Oct-88	1515	6	369.75	370.14
05-Dec-88	1400	6	373.29	372.38
16-Jan-89	1600	6	371.99	371.68
13-Feb-89	1505	6	371.36	370.08
20-Mar-89	1400	6	377.84	380.68
17-Apr-89	1625	6	379.70	379.85
25-May-89	1600	6	373.84	374.43
26-Jun-89	1500	6	374.07	372.53
18-Sep-89	1356	6	382.77	382.13
12-Dec-89	1323	6 🐷	368.92	366.74
21-Mar-90	1208	6	391.89	394.78
13-Jun-90	1326	6	395.88	396.33
20-May-91	1338	6	394.14	394.18
21-Nov-91	1336	6	377.41	380.23
20-May-92	1045	6	379.12	378.15
14-Jun-93	1107	6	398.06	399.28



Excerpt From CH2MHILL, 1997





Not To Scale

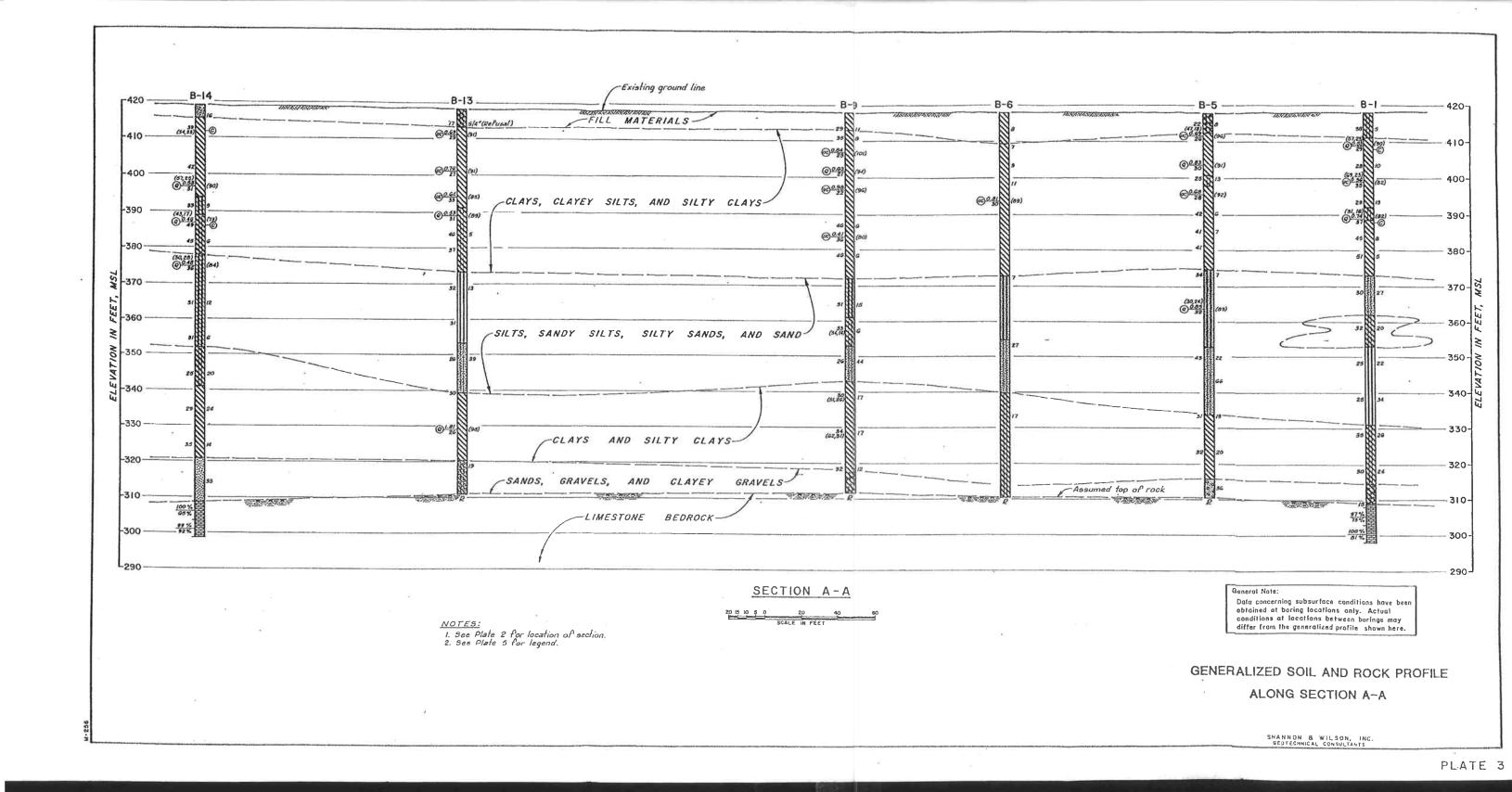
FIGURE 3

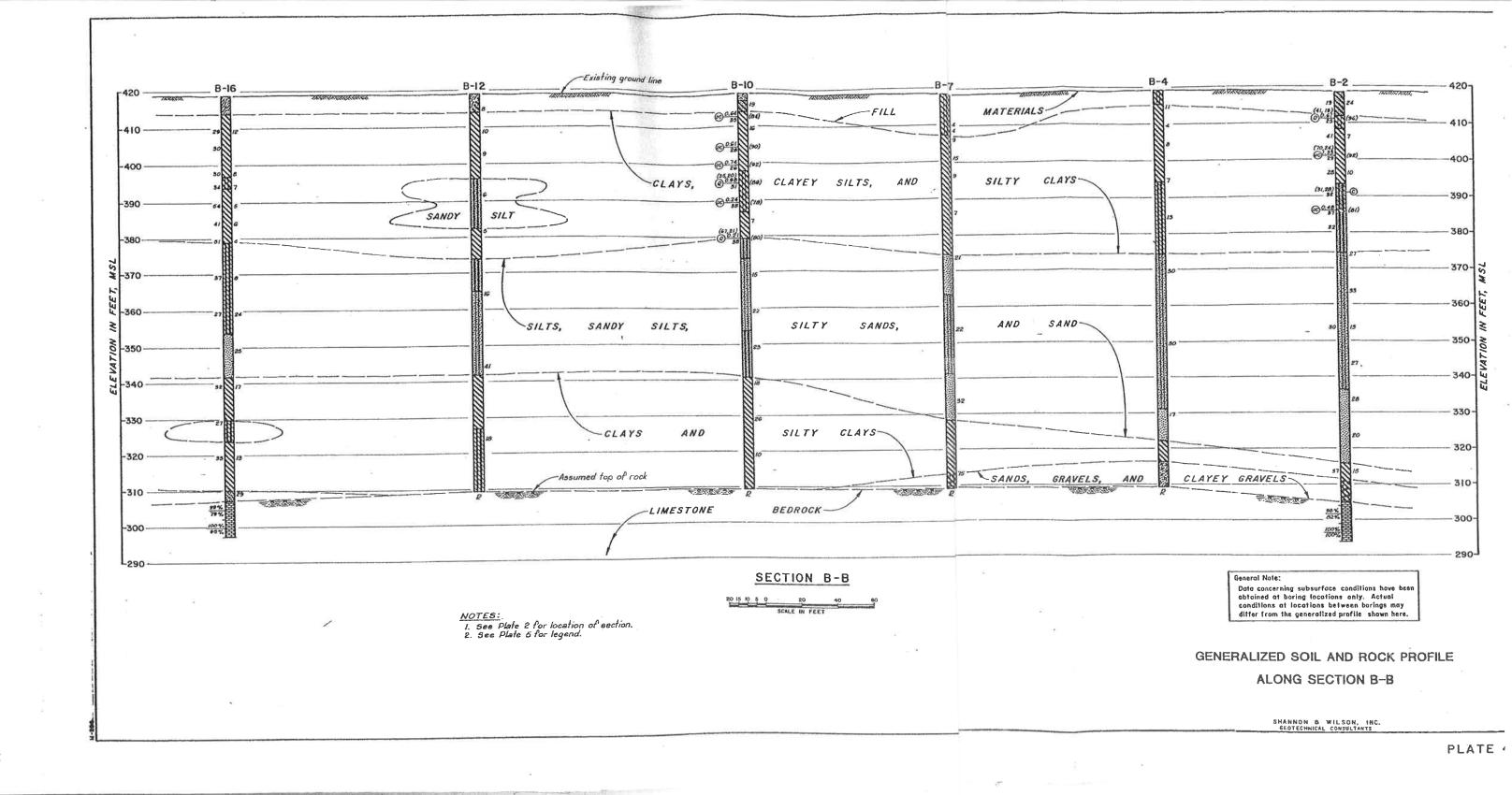
Conceptual Site Model
Union Electric Meramec Plant, St. Louis County, MO

E143874.SR.ZZ Cross-Section 12-3-97 mil

CH2MHILL

Excerpt From Shannon & Wilson, Inc., 1979





APPENDIX D CCR MONITORING WELL BORING LOGS

RECORD OF BOREHOLE BMW-1 SHEET 1 of 3 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 416.79 DRILLING INETTIOD. 6 GGIIG DRILLING DATE: 4/7/2016 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 LOCATION: Meramec Energy Center COORDINATES: N: N/A E: N/A SAMPLES METHOD SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS BORING REC ATT NUMBER DESCRIPTION USCS TYPE DEPTH - 0 (0-1.1) CONCRETE 415.9 (1.1-27.8) (CL) SILTY CLAY, medium to high plasticity fines, trace fine sand; greenish black (5GY 2/1); cohesive, w~PL, firm 1.9 5.0 1 SO 412.0 - 5 (5.0) SAA (Same As Above), medium gray (N5) mottled with moderate yellowish brown (10YR 5/4) $\,$ SO 407.0 10 (10.0) SAA, stiff 10.0 5.0 5.0 SO 3 403.4 (13.6) SAA, dark gray (N3) 13.6 CL Sonic 402.0 - 15 (15.0) SAA, trace organic fragments (wood) 6 4 SO 10/10/17 397.0 20 (20.0) SAA, some non-plastic fines; firm 20.0 Run #4, Silty clay in sample appears to be swelling when brought to the surface resulting in recovery over 100%. Measured field recovery: 6.0/5.0. Estimated actual recovery: 5.0/5.0 CO.GDT MEC LOGS.GPJ GLDR 5 SO - 25 (25.0) SAA, medium gray (N5) mottled with moderate yellowish brown (10YR 5/4) $\,$ 25.0 BOREHOLE MWD 5.0 5.0 SO 6 Run #5, Silty clay in sample appears to be swelling when brought to the surface resulting in recovery over 100%. Measured field recovery: 5.3/5.0. Estimated actual recovery: 5.0/5.0 (27.8-28.6) (ML) CLAYEY SILT, low plasticity fines, trace fine sand, light brownish gray (5YR 6/1) mottled moderate yellowish brown (10YR 5/4); cohesive, w<PL, ML 388.4 RECORD OF soft CL - 30 Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JSI/JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE BMW-1 SHEET 2 of 3 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 416.79 DRILLING INETTIOD. 6 GGIIG DRILLING DATE: 4/7/2016 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 LOCATION: Meramec Energy Center COORDINATES: N: N/A E: N/A SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS NUMBER DESCRIPTION TYPE USCS DEPTH - 30 Run #6, Silty clay in sample appears to be swelling when brought to the surface resulting in recovery over 100%. Measured field recovery: 5.7/5.0. Estimated actual recovery: 5.0/5.0 (28.6-37.1) (CL) SILTY CLAY, medium to high plasticity fines, trace fine sand; medium gray (N5) to light brownish gray (5YR 6/1) mottled with moderate yellowish brown (10YR 5/4); cohesive, w<PL, soft (*Continued*) CL 10.0 10.0 - 35 7 SO (37.1-40.0) (ML) sandy CLAYEY SILT, medium plasticity fines, some fine sand; medium gray (N5); cohesive, w<PL, soft МН 40 (40.0-48.1) (SC) CLAYEY SAND, fine sand, low plasticity fines; medium gray (N5); non-cohesive, wet, loose SC Sonic 10.0 10.0 - 45 8 SO 6 (48.1-50.0) (SP) SAND, fine sand, trace non-plastic fines; brownish gray (5YR 4/1); non-cohesive, wet, loose SP 10/10/17 50 (50.0-51.1) (CL) SILTY CLAY, medium to high plasticity fines, trace fine sand; medium gray (N5); cohesive, w>PL, firm CL 365.9 CO.GDT (51.1-51.3) (SC) CLAYEY SAND, fine sand, medium plasticity fines; medium gray (N5); cohesive, w<PL, firm 365.7 51.3 (51.3-53.1) (CL) SILTY CLAY, medium to high plasticity, trace fine sand; medium gray (N5); cohesive, w<PL, firm CL MEC LOGS.GPJ GLDR 363.9 53.1 (53.1-53.8) (SC) CLAYEY SAND, fine sand, medium plasticity fines; medium gray (N5); cohesive, w<PL, firm (53.8-58.5) (CL) SILTY CLAY, low to medium plasticity, 363.2 53.8 some fine sand; medium gray (N5); cohesive, w~PL, firm 9.2 10.0 - 55 10 SO BOREHOLE MWD CL RECORD OF (58.5-60.0) (SP) SAND, fine sand, trace non-plastic fines; brownish gray (5YR 4/1); non-cohesive, wet, SP compact 357.0 Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JSI/JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE BMW-1 SHEET 3 of 3 DRILLING METHOD: 6" Sonic DRILLING DATE: 4/7/2016 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center ELEVATION: 416.79 INCLINATION: -90 DATUM: NAVD88 AZIMUTH: N/A COORDINATES: N: N/A E: N/A SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 60 (60.0-64.0) (CL) SILTY CLAY, medium plasticity fines, some fine sand; medium gray (N5); cohesive, w~PL, firm 60.0 CL 353.0 64.0 (64.0-66.2) (ML) sandy CLAYEY SILT, low plasticity fines, fine sand; medium gray (N5); non-cohesive, wet, 10.0 10.0 - 65 9 SO ML 350.8 66.2 (66.2-70.0) (CL) SILTY CLAY, medium to high plasticity, trace fine sand; medium gray (N5) to brownish gray (5YR 4/1); cohesive, w>PL, stiff CL - 70 END OF BORING AT 70.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG BMW-1. - 75 GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 80 - 85 LOGGED: JSI/JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE BMW-2 SHEET 1 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/25/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 406.80 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 937,927.10 E: 866,342.24 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT DESCRIPTION NUMBER TYPE USCS DEPTH - 0 (0.0-6.9) (ML) CLAYEY SILT, medium plasticity fines, some organics (roots), trace fine sand; dark yellowish brown (10YR 4/2) to dusky yellowish brown (10YR 2/2); cohesive, w~PL, firm 1 SO ML - 5 (6.9-35.6) (CL) SILTY CLAY, medium to high plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2); cohesive, w~PL, firm - 10 3 SO (12.5) SAA (Same As Above) except, stiff Sonic 391.8 - 15 (15.0) SAA except, firm 6 4 SO CL GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 20 385.0 21.8 (21.8) SAA except, low plasticity fines; medium dark gray (N4); w<PL $\,$ so - 25 5 Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE BMW-2 SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/25/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 406.80 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 937,927.10 E: 866,342.24 SOIL/ROCK PROFILE SAMPLES **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 30 (6.9-35.6) (CL) SILTY CLAY, medium to high plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2); cohesive, w~PL, firm (Continued) CL 10.0 10.0 - 35 6 SO (35.6-38.8) (ML) CLAYEY SILT, low plasticity fines, some sub-angular fine to coarse gravel; dark gray (N3); cohesive, w<PL, firm ML 368.0 38.8 (38.8-41.4) (GM) SILTY GRAVEL, fine to coarse sub-angular gravel, non-plastic fines, trace fine sand; brownish gray (5YR 4/1); non-cohesive, wet, compact Sonic 366.8 40 GM (40.0) SAA except, some fine to coarse sub-rounded 40.0 50 365.4 41.4 (41.4-50.0) (CL) SILTY CLAY, high plasticity fines; dark gray (N3); cohesive, w>PL, stiff 7.7 10.0 - 45 SO CL CO.GDT 10/10/17 50 END OF BORING AT 50.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG BMW-2. RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR - 55 GOLDER STL LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE MW-1 SHEET 1 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/23/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 404.10 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 937,676.92 E: 865,954.06 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 0 (0.0-10.0) (ML) SILT, non-plastic fines, some fine sand, some organics (roots); dark yellowish brown (10YR 4/2); cohesive, w<PL, soft 2.7 5.0 bgs 2/16/2016 1 SO 399.1 5.0 - 5 ML (5.0) SAA (Same As Above) except, firm (10.0-15.0) (ML) CLAYEY SILT, low to medium plasticity fines, some fine sand; moderate yellowish brown (10YR 5/4) to dark yellowish brown (10YR4/2); cohesive, w~PL, soft to firm 10 SO ML 3 Sonic 389.1 15.0 - 15 (15.0-21.4) (ML) SILT, non-plastic fines, trace fine sand; moderate yellowish brown (10YR 5/4); cohesive, w<PL, 6 4 SO ML GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 20 (21.4-32.7) (ML) SILT, non-plastic to low plasticity fines, trace fine sand; medium dark gray (N4); cohesive, w<PL, - 25 5 SO ML Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE MW-1 SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/23/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 404.10 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 937,676.92 E: 865,954.06 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 30 (21.4-32.7) (ML) SILT, non-plastic to low plasticity fines, trace fine sand; medium dark gray (N4); cohesive, w<PL, ML (32.7-36.2) (SM) SILTY SAND, fine to coarse well graded sand, non-plastic to low plasticity fines, trace sub-rounded gravel; brownish gray (5YR 4/1); non-cohesive, wet, compact SM 10.0 10.0 - 35 6 SO (36.2-40.0) (GW) sandy GRAVEL, fine to coarse sub-rounded gravel, fine to coarse sub-rounded sand, some non-plastic to low plasticity fines; brownish gray (5YR 4/1); non-cohesive, wet, compact GW 40 END OF BORING AT 40.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG MW-1. - 45 GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 50 - 55 LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE MW-2 SHEET 1 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/23/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 396.13 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 937,325.09 E: 864,864.51 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 0 (0.0-12.4) (ML) SILT, non-plastic fines, trace fine sand, some organics (roots); dark yellowish brown (10YR 4/2); non-cohesive, moist, compact 3.2 5.0 1 SO 391.1 5.0 - 5 (5.0) SAA (Same As Above) except, dark yellowish brown (10YR 4/2) to brownish black (5YR 2/1) MI - 10 4.7 5.0 (12.4-26.8) (CL) SILTY CLAY, low to medium plasticity fines, trace fine sand; medium dark gray (N4) mottled dark yellowish brown (10YR 4/2); cohesive, w~PL, stiff 3 SO Sonic 381.1 - 15 (15.0) SAA except, firm to stiff 6 CL GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 20 SO - 25 25.0 (25.0) SAA except, firm 369.3 (26.8-30.0) (CL) SILTY CLAY, medium plasticity fines, some fine sand; medium dark gray (N4); cohesive, 10.0 10.0 SO 5 w~PL, soft CL 366.1 Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE MW-2 SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/23/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 396.13 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 937,325.09 E: 864,864.51 SOIL/ROCK PROFILE SAMPLES **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 30 (30.0-31.2) (SW) SAND, fine to coarse sub-rounded sand, trace low plasticity fines; brownish gray (5YR 4/1); non-cohesive, wet, compact 30.0 SW (31.2-34.2) (CL) SILTY CLAY, medium to high plasticity fines, trace fine sand; medium dark gray (N4); cohesive, w~PL, firm 10.0 10.0 5 SO CL (34.2-34.6) (GM) SILTY GRAVEL, fine to coarse GM 361.5 34.6 361.1 sub-rounded gravel, low plasticity fines, trace fine to coarse sub-rounded sand; dark yellowish brown (10YR - 35 4/2); non-cohesive, wet, compact (34.6-45.0) (CL) SILTY CLAY, medium to high plasticity fines, trace fine sand; medium dark gray (N4); cohesive, w~PL, firm (35.0) SAA except, stiff CL 10.0 10.0 40 6 SO Sonic 6 351.1 45.0 - 45 END OF BORING AT 45.0 FEET BELOW GROUND SURFACE. FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG MW-2. RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 50 - 55 GOLDER STL LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE MW-3 SHEET 1 of 2 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 394.63 DRILLING DATE: 1/22/16
DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 LOCATION: Meramec Energy Center COORDINATES: N: 936,750.84 E: 864,447.17 SAMPLES SOIL/ROCK PROFILE BORING METHOD DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-5.0) (ML) SILT, non-plastic to low plasticity fines, some fine sand; dark yellowish brown (10YR 4/2); cohesive, w<PL, firm 2.9 5.0 ML 1 SO - 5 (5.0-6.4) (ML) CLAYEY SILT, low to medium plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2) to dusky yellowish brown (10YR 2/2); cohesive, w~PL, ML (6.4-11.1) (SM) SILTY SAND, fine poorly graded sand, non-plastic fines; dark gray (N3); non-cohesive, wet, compact SM 10 Water Level 11.07 ft bgs 2/16/2016 383.5 (11.1-13.5) (ML) CLAYEY SILT, low to medium plasticity fines, trace fine sand; brownish black (5YR 2/1); cohesive, w<PL, firm ML 4.9 5.0 SO 3 (13.5-22.2) (CL) SILTY CLAY, medium to high plasticity fines; dark yellowish brown (10YR 4/2); cohesive, w>PL, 379.6 - 15 (15.0) SAA (Same As Above) except, w~PL, firm Sonic 4 SO CL 10/10/17 20 CO.GDT SP MEC LOGS.GPJ GLDR (22.2-22.4) (SP) SAND, fine sand, some non-plastic 372.2 fines; dark yellowish brown (10YR 4/2); non-cohesive, wet, compact (22.4-25.0) (ML) CLAYEY SILT, low to medium plasticity ML fines, trace fine sand; dark gray (N3); cohesive, w<PL, 369.6 25.0 9.1 10.0 - 25 (25.0-25.2) (SP) SAND, fine sand, some non-plastic fines; moderate yellowish brown (10YR 5/4); 5 SO SF CL non-cohesive, wet, compact 25.2 BOREHOLE MWD (25.2-26.1) (CL) SILTY CLAY, low to medium plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2); 26.1 cohesive, w<PL, firm (26.1-30.0) (GW) sandy GRAVEL, fine to coarse sub-rounded gravel, fine sand, trace non-plastic fines; dark yellowish brown (10YR 4/2); non-cohesive, wet, RECORD OF 364.6 Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE MW-3 SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/22/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 394.63 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 936,750.84 E: 864,447.17 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 30 (30.0-55.0) (CL) SILTY CLAY, medium to high plasticity fines, trace sub-rounded gravels; moderate brown (5YR3/4); cohesive, w~PL, stiff 30.0 359.8 10.0 10.0 - 35 (34.8) SAA except, olive gray (5Y 4/1) 34.8 6 SO 354.6 40 (40.0) Run #7, Driller adds 5 feet of sample rod to the sampler in order to sample a 15 feet run to total depth. (40.0) SAA except, less gravel 40.0 Sonic CL 6 - 45 10.7 15.0 SO GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 50 - 55 END OF BORING AT 55.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH

RECORD OF BOREHOLE MW-4 SHEET 1 of 3 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/22/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A DATUM: NAVD88 ELEVATION: 402.03 AZIMUTH: N/A INCLINATION: -90 LOCATION: Meramec Energy Center COORDINATES: N: 935,618.00 E: 864,629.82 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-12.4) (ML) CLAYEY SILT, low to medium plasticity fines, some fine sand; dark yellowish brown (10YR 4/2); cohesive, w~PL, firm 3.5 5.0 1 SO 397.0 5.0 - 5 (5.0) SAA (Same As Above) except, trace fine sub-angular gravel; w<PL MI 10 4.6 5.0 3 SO (12.4-15.0) (ML) CLAYEY SILT, low to medium plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2) to dark gray (N3); cohesive, w<PL, firm ML Sonic 387.0 15.0 - 15 (15.0-20.0) NO RECOVERY (15.0-20.0) Run # 4, No recovery from 6 15-20 ft. Driller says sample slipped through the retaining bit. Some CLAYEY SILT found in bit, 15-20 is likely same as above but very soft. ML 4 SO RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 20 (20.0-40.0) (ML) CLAYEY SILT, low to medium plasticity fines, trace fine sand; brownish gray (5YR 4/1); cohesive, w~PL, stiff 9.4 10.0 so - 25 ML 5 375.7 26.3 (26.3) SAA except, soft, w<PL 372.0 Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE MW-4 SHEET 2 of 3 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/22/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 402.03 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 935,618.00 E: 864,629.82 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) (20.0-40.0) (ML) CLAYEY SILT, low to medium plasticity fines, trace fine sand; brownish gray (5YR 4/1); cohesive, w~PL, stiff (Continued) (30.0) SAA except, some fine sand; w~PL, firm - 30 30.0 10.0 10.0 - 35 ML 6 SO 40 (40.0-41.3) (GW) GRAVEL, sub-rounded gravel, some medium plasticity fines, trace fine to coarse sub-rounded sand; moderate yellowish brown (10YR 5/4); non-cohesive, wet, compact GW 360.7 41.3 (41.3-60.0) (CL) SILTY CLAY, medium to high plasticity fines, trace fine sand; dark gray (N3); cohesive, w~PL, firm Sonic 10.0 10.0 - 45 SO 6 GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 352.0 - 50 (50.0) SAA except, trace coarse sub-rounded gravel; CL 347.7 (54.3) SAA except, no gravel, some fine sand; stiff 54.3 9.8 10.0 so - 55 8 342.0 Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

P	ROJECT	: Ameren CCR GW Monitoring DRILLING NUMBER: 153-1406.0004A DRILLING	CORD OF METHOD: 6" Sor DATE: 1/22/16 S: Mini Sonic (CDI	nic	DATU AZIMU	M: NAVD JTH: N/A	88	.618.00 E	SHEET 3 of 3 ELEVATION: 402.03 INCLINATION: -90 : 864,629.82
		SOIL/ROCK		, , , ,			SAMPLE		
DEPTH	BORING METHOD	DESCRIPTION	USCS	GRAPHIC LOG	ELEVATION	NUMBER	TYPE	REC ATT	REMARKS
- 60		(60.0-65.0) (ML) SILT, low plasticity fines, trace			(ft) 60.0			ļ.,,	-
-		sub-angular gravel, trace fine sand; brownish gray (5 4/1); cohesive, w <pl, firm<="" td=""><td>YR</td><td></td><td></td><td></td><td></td><td></td><td>-</td></pl,>	YR						-
-	Sonic		ML			9	so	<u>5.0</u> 5.0	-
									_
- 65					337.0				
- 65		END OF BORING AT 65.0 FEET BELOW GROUND SURFACE.	1 1		65.0				
		FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG MW-4.	'						-
-									-
									_
- 70									_
70									
									-
									-
-									-
-									-
- 75									_
-									-
-									-
-									-
_									-
- 80									_
GDT 1									-
A CO									-
- GLD									-
GS.GP									-
O D S 85									_
MD -									-
OLE M									_
OREH									_
OF B									_
COR									
DER STL R	SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade DRILLER: J. Drabek LOGGED: JS CHECKED: JSI REVIEWED: PJJ/MNH CHECKED: PJJ/MNH								

RECORD OF BOREHOLE MW-5 SHEET 1 of 3 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/21/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 400.83 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 934,874.35 E: 864,780.96 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-10.0) FILL - (CL) SILTY CLAY, medium plasticity fines, trace fine sand, some organics (tree and grass roots); dark yellowish brown (10YR 4/2); cohesive, w~PL, firm SO 395.8 - 5 CL (5.0) SAA (Same As Above) except, greenish black (5GY 2/1); stiff 10 (10.0-20.0) FILL - (ML) CLAYEY SILT, non-plastic to low plasticity fines, trace fine sand; brownish black (5YR 2/1) to grayish black (N2), ASH; cohesive, w<PL, soft SO 3 Sonic 385.8 - 15 ML (15.0) SAA except, medium dark gray (N4) mottled moderate yellowish brown (10YR 5/4) 6 ft bgs 2/16/2016 SO RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 20 (20.0-30.0) (CL) SILTY CLAY, low plasticity fines; dusky yellowish brown (10YR 2/2) to dark gray (N3); cohesive, w<PL, firm - 25 CL 5 SO 370.8 Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

GOLDER STL

RECORD OF BOREHOLE MW-5 SHEET 2 of 3 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/21/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 400.83 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 934,874.35 E: 864,780.96 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 30 30.0 (30.0-31.9) (SW) SAND, fine to coarse sub-rounded sand, fine sub-rounded gravel; dark yellowish brown (10YR 4/2); non-cohesive, wet, compact SW (31.9-33.3) (CL) SILTY CLAY, low to medium plasticity fines, trace fine sand; medium dark gray (N4); cohesive, w~PL, firm CL (33.3-35.0) (SC) CLAYEY SAND, fine to coarse sub-rounded sand, low to medium plasticity fines; medium dark gray (N4); non-cohesive, wet, compact SC 10.0 10.0 - 35 6 SO (35.0-46.0) (CL) SILTY CLAY, low to medium plasticity fines; dark gray (N3); cohesive, w~PL firm 40 CL SO Sonic - 45 (46.0-60.6) (SW) SAND, fine to coarse sub-rounded sand, some sub-rounded gravel; dark gray (N3); non-cohesive, wet, compact RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 50 8 SO SW - 55 2.4 5.6 SO 9 Log continued on next page LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

GOLDER STL

RECORD OF BOREHOLE MW-5 SHEET 3 of 3 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOCATION: Meramec Energy Center DRILLING METHOD: 6" Sonic DRILLING DATE: 1/21/16 DRILL RIG: Mini Sonic (CDD1415) DATUM: NAVD88 AZIMUTH: N/A ELEVATION: 400.83 INCLINATION: -90 COORDINATES: N: 934,874.35 E: 864,780.96 BORING METHOD SOIL/ROCK PROFILE SAMPLES DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER USCS TYPE DEPTH - 60 SW SO 9 END OF BORING AT 60.6 FEET BELOW GROUND SURFACE. FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG MW-5. - 65 - 70 - 75 GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 80 - 85 LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE MW-6 SHEET 1 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/21/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 415.84 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 933,905.19 E: 865,153.48 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-12.9) FILL - (ML) sandy SILT, non-plastic fines, fine sand; dusky yellowish brown (10YR 2.2); non-cohesive, 1 SO 410.8 5.0 - 5 (5.0) SAA (Same As Above) except, some organics (tree and grass roots) ML 405.8 10 (10.0) SAA except, wet 10.0 4.9 5.0 SO 3 402.9 12.9 (12.9-15.0) FILL - (CL) SILTY CLAY, medium to high plasticity fines, trace fine sand; moderate brown (5YR 3/4); cohesive, w<PL, soft CL Sonic 400.8 - 15 (15.0-20.0) NO RECOVERY (15.0-20.0) Run # 4, No recovery from 6 15-20 ft. Driller says sample slipped through the retaining bit. Some SILTY CLAY found in bit, 15-20 is likely same as above but very soft. CL 4 SO RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 20 (20.0-30.0) (CL) SILTY CLAY, medium to high plasticity (20.0-30.0) Run #5, poor recovery because fines, trace fine sand; duskly yellowish brown (10YR 2/2); cohesive, w~PL, firm driller dropped contents of bag on ground 3.0 10.0 - 25 CL 5 SO 385.8 Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

GOLDER STL

RECORD OF BOREHOLE MW-6 SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/21/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 415.84 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 933,905.19 E: 865,153.48 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 30 (30.0-42.2) (ML) sandy SILT, non-plastic fines, fine sand; dark yellowish brown (10YR 4/2); non-cohesive, 30.0 (30.0) Run 6, (40.0) Driller adds 5 feet of sample rod to the Sample:
sample a 15 feet run.

Water Level 31.32
ft bgs 2/16/2016 sample rod to the sampler in order to - 35 ML 40 Sonic 373.6 42.2 (42.2-52.0) (SW) SAND, fine to coarse sub-rounded sand, trace non-plastic fines; dark yellowish brown 6 (10YR 4/2); non-cohesive, wet, compact 370.8 - 45 (45.0) SAA except, no fines; medium gray (N5) SW GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 50 SO 363.8 52.0 (52.0-55.0) (SP) SAND, fine sand; medium gray (N5); non-cohesive, wet, compact SP - 55 END OF BORING AT 55.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE MW-7 SHEET 1 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/23/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A DATUM: NAVD88 ELEVATION: 415.67 AZIMUTH: N/A INCLINATION: -90 LOCATION: Meramec Energy Center COORDINATES: N: 934,334.40 E: 866,242.50 SOIL/ROCK PROFILE SAMPLES **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-6.3) (ML) SILT, non-plastic to low plasticity fines, trace sub-angular gravel in upper 0.5 ft; dusky brown (5YR 2/2); cohesive, w<PL, stiff 1 SO ML 410.7 5.0 - 5 (5.0) SAA (Same As Above) except, firm 409.4 6.3 (6.3-7.4) (GM) SILTY GRAVEL, fine to coarse sub-angular gravel, non-plastic fines, trace fine to coarse GM sub-rounded sand; dusky yellowish brown (10YR 2/2); non-cohesive, wet, compact 408.3 7.4 (7.4-11.2) (ML) CLAYEY SILT, low plasticity fines, some fine sand; dark yellowish brown (10YR 4/2); cohesive, ML 10 (11.2-21.9) (ML) sandy SILT, non-plastic to low plasticity fines, fine sand, trace sub-rounded gravel; dusky yellowish brown (10YR 2/2); cohesive, w<PL, soft 4.0 5.0 SO 3 Sonic - 15 6 ML 2.7 5.0 SO RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 20 (21.9-23.6) (CL) SILTY CLAY, medium to high plasticity fines; dark yellowish brown (10YR 4/2); cohesive, w~PL, CL (23.6-40.0) (SP & ML) SAND & SILT, fine sand, non-plastic fines; dark yellowish brown (10YR 4/2); non-cohesive, wet, compact 4.9 10.0 - 25 5 SO SP & ML Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

GOLDER STL

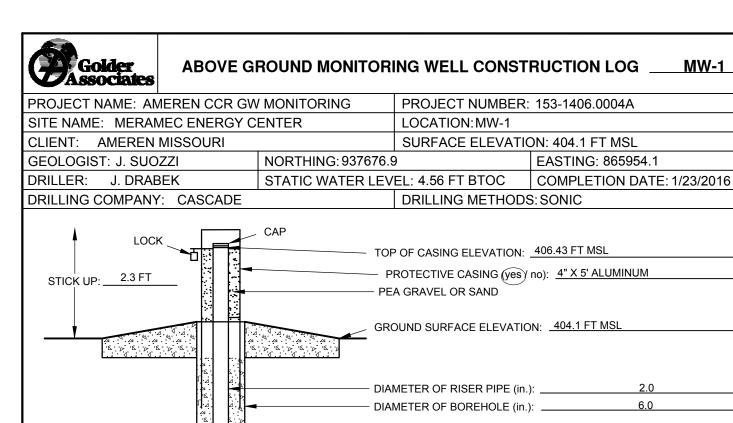
RECORD OF BOREHOLE MW-7 SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/23/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 415.67 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 934,334.40 E: 866,242.50 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 30 (23.6-40.0) (SP & ML) SAND & SILT, fine sand, non-plastic fines; dark yellowish brown (10YR 4/2); non-cohesive, wet, compact (Continued) <u>6.5</u> 10.0 - 35 SP 6 SO & ML 40 (40.0-52.7) (SW) SAND, fine to coarse sub-rounded sand, trace sub-rounded fine gravel; dusky yellowish brown (10YR 4/2); non-cohesive, wet, compact 6" Sonic - 45 7 SO SW GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 365.7 - 50 (50.0) SAA except, no gravel 50.0 8 SO 363.0 52.7 END OF BORING AT 52.7 FEET BELOW GROUND SURFACE. FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG MW-7. - 55 LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE MW-8 SHEET 1 of 3 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/24/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A DATUM: NAVD88 ELEVATION: 421.03 AZIMUTH: N/A INCLINATION: -90 LOCATION: Meramec Energy Center COORDINATES: N: 935,303.55 E: 866,797.84 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-0.9) FILL - (GW) sandy GRAVEL, fine to coarse sub-angular gravel, fine sand; dark gray (N3); GW non-cohesive, dry, loose (0.9-1.2) FILL - (SW) SAND, fine to coarse sub-rounded sand; moderate yellowish brown (10YR 5/4); 419.8 1.2 non-cohesive, dry, loose (1.2-7.1) (ML) sandy SILT, non-plastic fines, fine sand, trace sub-rounded gravel; dusky yellowish brown (10YR 2/2); non-cohesive, dry, compact 4.8 5.0 1 SO ML 416.0 - 5 (5.0) SAA (Same As Above) except, some sand, some (7.1-10.0) (ML) CLAYEY SILT, low plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2); cohesive, w<PL, stiff ML 10 $\overline{(10.0\text{-}20.0)} \ \overline{(\text{CL})} \ \overline{\text{SILTY}} \ \overline{\text{CLAY}}, \ \overline{\text{high plasticity fines}}; \\ brownish gray (5YR 4/1); cohesive, w~PL, stiff$ Sonic - 15 CL 3 SO 6 10/10/17 20 (20.0-21.7) (SC) CLAYEY SAND, fine to coarse sub-rounded sand, medium plasticity fines; brownish gray (5YR 4/1); non-cohesive, wet, compact SC CO.GDT (21.7-30.0) (CL) SILTY CLAY, high plasticity fines, trace fine sand; medium dark gray (N3); cohesive, w>PL, very MEC LOGS.GPJ GLDR <u>4.7</u> 10.0 - 25 SO CL RECORD OF BOREHOLE MWD 391.0 Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE MW-8 SHEET 2 of 3 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/24/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 421.03 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 935,303.55 E: 866,797.84 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 30 (30.0-32.8) (ML) sandy SILT, non-plastic fines, fine sand; dark yellowish brown (10YR 4/2); non-cohesive, 30.0 ML (32.8-40.0) (CL) SILTY CLAY, low plasticity fines; brownish gray (5YR 4/1); cohesive, w<PL, stiff 9.2 10.0 - 35 5 SO Water Level 35.86 ft bgs 2/16/2016 CL 40 (40.0-50.0) (CL) SILTY CLAY, medium plasticity fines; medium dark gray (N3); cohesive, w~PL, firm Sonic 10.0 10.0 - 45 CL 6 SO 6 372.5 48.5 (48.8) SAA except, soft 371.8 49.2 (49.2) SAA except, firm GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 50 (50.0-68.0) (ML) sandy SILT, non-plastic fines, fine sand; medium dark gray (N4); non-cohesive, wet, compact ML so - 55 Log continued on next page LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE MW-8 SHEET 3 of 3 DRILLING METHOD: 6" Sonic DRILLING DATE: 1/24/16 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0004A LOÇATION: Meramec Energy Center DATUM: NAVD88 ELEVATION: 421.03 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 935,303.55 E: 866,797.84 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 60 (50.0-68.0) (ML) sandy SILT, non-plastic fines, fine sand; medium dark gray (N4); non-cohesive, wet, compact (Continued) ML 10.0 10.0 - 65 8 SO (68.0-75.5) (SM) SILTY SAND, fine poorly graded sand, non-plastic fines; medium dark gray (N4); non-cohesive, wet, compact Sonic - 70 50 SM 10.0 10.0 - 75 9 SO (75.5-75.9) (SW) SAND, fine to coarse sub-rounded SW (75.5-75.9) (SW) SAND, fine to coarse sub-rounded sand, trace coarse sub-rounded gravel; brownish gray (5YR 4/1); non-cohesive, wet, compact (75.9-80.0) (CL) SILTY CLAY, low plasticity fines, trace fine sand; medium dark gray (N4); cohesive, w~PL, stiff 345.1 75.9 CL GOLDER STL RECORD OF BOREHOLE MWD MEC LOGS.GPJ GLDR_CO.GDT 10/10/17 - 80 END OF BORING AT 80.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG MW-8. - 85 LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

APPENDIX E CCR MONITORING WELL CONSTRUCTION DIAGRAMS



BOTTOM OF FILTER PACK (ft. bgs): 39.1
 TYPE AND AMOUNT OF BACKFILL: 0.9 FT - NATURAL CAVE IN

- CONCRETE SEAL DEPTH (ft. bgs): 2.5

ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL.

125 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FT (2000)
MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON FEBRUARY 4, 2016.
FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. I	NGRAM
DATE CHECKED:	4/25/2016

TOTAL DEPTH OF BOREHOLE: 40.0 FT



Golder Associates	ABOVE G	ROUND MONITOR	ING WELL CONSTR	RUCTION LOGMW-	-2		
PROJECT NAME: AM	MEREN CCR GW	/ MONITORING	PROJECT NUMBER:	153-1406.0004A			
SITE NAME: MERAN	MEC ENERGY C	ENTER	LOCATION:MW-2				
CLIENT: AMEREN			SURFACE ELEVATION: 396.1 FT MSL				
GEOLOGIST: J. SUO		NORTHING: 937325.		EASTING: 864864.5			
DRILLER: J. DRAE				COMPLETION DATE: 1/23/20)16		
DRILLING COMPANY			DRILLING METHODS				
LOCK STICK UP: 2.5 FT		PE P	P OF CASING ELEVATION: ROTECTIVE CASING (yes) r A GRAVEL OR SAND DUND SURFACE ELEVATION METER OF RISER PIPE (in.): METER OF BOREHOLE (in.): NCRETE SEAL DEPTH (ft. bg PE AND AMOUNT OF ANNUL P OF BENTONITE SEAL DEPTH PE AND AMOUNT OF BENTO P OF SAND PACK DEPTH (ft. bgs P OF SCREEN DEPTH (ft. bgs	398.62 FT MSL no): 4" X 5' ALUMINUM N: 396.1 FT MSL 2.0 6.0 s): 2.5 AR SEAL: NONE TH (ft. bgs): 2.5 DNITE SEAL: 3 "BENTONITE CHIPS - bgs): COARSE: 27.0 FINE: 20 PE: NONE 2: X 4.8' SCHEDULE 40 PVC			
			E OF SAND PACK:				
			OUNT OF SAND:				
		ВО	TTOM OF SCREEN DEPTH (f	t. bgs): 33.9			
		во	FTOM OF WELL DEPTH (ft. b	gs):34.3			
TOTAL DEPTH OF BOREHOLE: 45.0 F	T	ВО ⁻ ТҮР	TTOM OF FILTER PACK (ft. b PE AND AMOUNT OF BACKF	gs):35.0 ILL: 10.0 FT - 1.5 BAGS BENTONITE	E CHIPS		
150 GALLONS OF H2O UMISSOURI EAST ZONE.	JSED DURING DRIL VERTICAL DATUM	LING. HORIZONTAL DATU	ED BY ZAHNER AND ASSO	I SEA LEVEL. ATES NAD83 US SURVEY FT (2000) CIATES, INC ON FEBRUARY 4, 2016,			

CHECKED BY: J. INGRAM DATE CHECKED: 4/25/2016

PREPARED BY: OF SUOZZI



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG MW-3 **Associates** PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0004A SITE NAME: MERAMEC ENERGY CENTER LOCATION: MW-3 CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 394.6 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 936750.8 EASTING: 864447.2 DRILLER: J. DRABEK STATIC WATER LEVEL: 13.56 FT BTOC COMPLETION DATE: 1/22/2016 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK . - TOP OF CASING ELEVATION: 397.12 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ___2.5 FT - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 394.6 FT MSL DIAMETER OF RISER PIPE (in.): DIAMETER OF BOREHOLE (in.): ___ - CONCRETE SEAL DEPTH (ft. bgs): 2.5 — TYPE AND AMOUNT OF ANNULAR SEAL: ______ NONE TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 – TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ " BENTONITE CHIPS - 5 BAGS - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 23.0 FINE: 22.0 - CENTRALIZER (yes (no) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): 25.4 TYPE OF SCREEN: 2" X 4.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: _____COARSE: 2 BAGS FINE: \frac{1}{3} BAG

ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL.

150 GALLONS OF H2O USED DURING DRILLING, HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FT (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON FEBRUARY 4, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

- BOTTOM OF SCREEN DEPTH (ft. bgs): _____

- BOTTOM OF FILTER PACK (ft. bgs): _

BOTTOM OF WELL DEPTH (ft. bgs): ______30.6

TYPE AND AMOUNT OF BACKFILL: 23.5 FEET - 3 BAGS BENTONITE CHIPS

CHECKED BY: J. INGRAM DATE CHECKED: 4/25/2016

TOTAL DEPTH

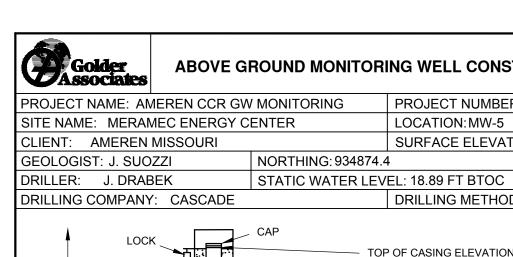
OF BOREHOLE: 55.0 FT



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG PROJECT NUMBER: 153-1406.0004A PROJECT NAME: AMEREN CCR GW MONITORING SITE NAME: MERAMEC ENERGY CENTER LOCATION: MW-4 CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 402.0 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 935618.0 EASTING: 864629.8 STATIC WATER LEVEL: 20.25 FT BTOC DRILLER: J. DRABEK COMPLETION DATE: 1/22/2016 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC LOCK TOP OF CASING ELEVATION: 404.10 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM 2.1 FT STICK UP: _ - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 402.0 FT MSL DIAMETER OF RISER PIPE (in.): 2.0 6.0 DIAMETER OF BOREHOLE (in.): _____ 2.5 CONCRETE SEAL DEPTH (ft. bgs): ______ - TYPE AND AMOUNT OF ANNULAR SEAL: _____ NONE - TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 - TYPE AND AMOUNT OF BENTONITE SEAL; $\frac{3}{8}$ BENTONITE CHIPS - $6\frac{1}{2}$ BAGS TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 35.7 FINE: 34.0 CENTRALIZER (yes (no) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): ____ TYPE OF SCREEN: 2" X 4.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): _____ 0.010 IN SIZE OF SAND PACK: _____ COARSE: #1 FINE: #0 COARSE: 2 BAGS FINE: 1/3 BAG AMOUNT OF SAND: ____ BOTTOM OF SCREEN DEPTH (ft. bgs): 42.7 BOTTOM OF WELL DEPTH (ft. bgs): _____ BOTTOM OF FILTER PACK (ft. bgs): ___ TOTAL DEPTH 65.0 FT - TYPE AND AMOUNT OF BACKFILL: 20.0 FT - 3 $\frac{1}{3}$ BAGS BENTONITE CHIPS OF BOREHOLE: ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 200 GALLONS OF H2O USED DURING DRILLING, HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FT (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON FEBRUARY 4, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM DATE CHECKED: 4/25/2016

PREPARED BY THE THE PREPARED BY THE PREPARED B



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG MW-5

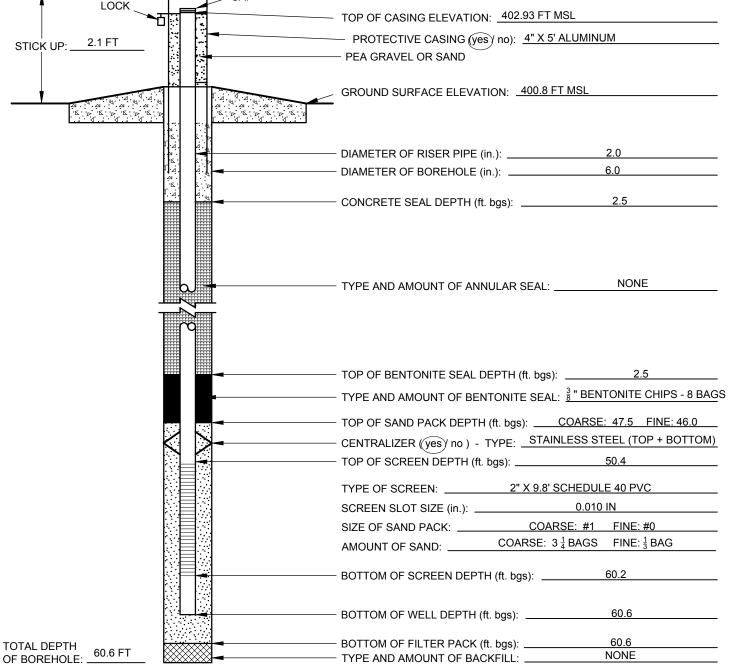
PROJECT NUMBER: 153-1406.0004A LOCATION: MW-5

COMPLETION DATE: 1/22/2016

SURFACE ELEVATION: 400.8 FT MSL

NORTHING: 934874.4 EASTING: 864781.0

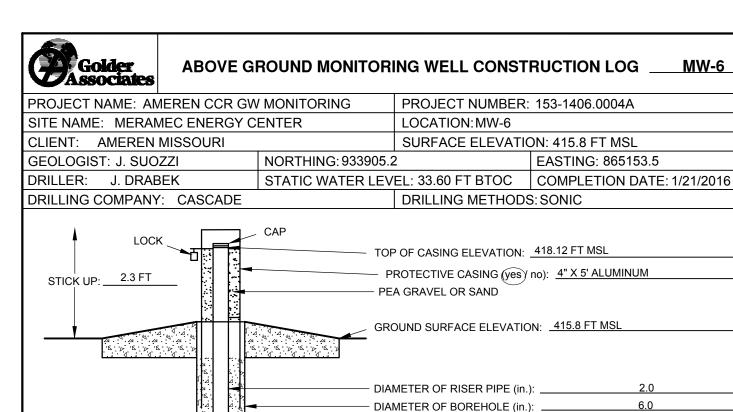
DRILLING METHODS: SONIC



ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL.

250 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FT (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON FEBRUARY 4, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM DATE CHECKED: 4/25/2016



- TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ " BENTONITE CHIPS - 7 BAGS - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 39.7 FINE: 39.0 CENTRALIZER (yes) no) - TYPE: STAINLESS STEEL (TOP + BOTTOM) TOP OF SCREEN DEPTH (ft. bgs): 42.5 TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: COARSE: 3.5 BAGS FINE: \$\frac{1}{3}\$ BAG BOTTOM OF SCREEN DEPTH (ft. bgs): 52.3

BOTTOM OF WELL DEPTH (ft. bgs): ______52.7

TYPE AND AMOUNT OF BACKFILL: 2.3 FEET -NATURAL BACKFILL

BOTTOM OF FILTER PACK (ft. bgs): ____

- CONCRETE SEAL DEPTH (ft. bgs): 2.5

TYPE AND AMOUNT OF ANNULAR SEAL:

ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL.

300 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FT (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON FEBRUARY 4, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J.	INGRAM
DATE CHECKED:	

TOTAL DEPTH

OF BOREHOLE: 55.0 FT

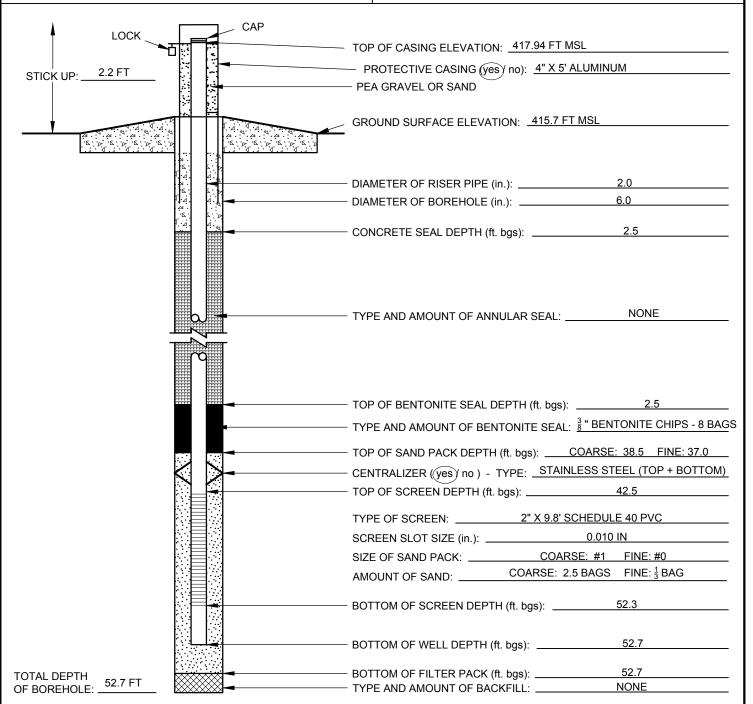
NONE



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG MW-7

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0004A SITE NAME: MERAMEC ENERGY CENTER LOCATION: MW-7 CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 415.7 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 934334.4 EASTING: 866242.5 DRILLER: J. DRABEK STATIC WATER LEVEL: 33.26 FT BTOC COMPLETION DATE: 1/24/2016

DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC



ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL.

200 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FT (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON FEBRUARY 4, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM DATE CHECKED: 4/25/2016



DRILLING COMPANY: CASCADE

ABOVE GROUND MONITORING WELL CONSTRUCTION LOG MW-8

DRILLING METHODS: SONIC

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0004A SITE NAME: MERAMEC ENERGY CENTER LOCATION: MW-8 CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 421.0 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 935303.6 EASTING: 866797.8 DRILLER: J. DRABEK STATIC WATER LEVEL: 38.20 FT BTOC COMPLETION DATE: 1/24/2016

CAP LOCK TOP OF CASING ELEVATION: 423.37 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ___2.4 FT - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 421.0 FT MSL DIAMETER OF RISER PIPE (in.): DIAMETER OF BOREHOLE (in.): ___ CONCRETE SEAL DEPTH (ft. bgs): _____ – TYPE AND AMOUNT OF ANNULAR SEAL: $\frac{3}{8}$ "BENTONITE CHIPS - 3.5 BAGS - TYPE AND AMOUNT OF ANNULAR SEAL: HIGH SOLIDS BENTONITE 4 BAGS - TYPE AND AMOUNT OF BENTONITE SEAL: $rac{3}{8}$ " BENTONITE CHIPS - 1 BAG - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 63.0 FINE: 62.5 - CENTRALIZER (yes) no) - TYPE: STAINLESS STEEL (TOP + BOTTOM) TOP OF SCREEN DEPTH (ft. bgs): 65.2 TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: _____COARSE: 2.5 BAGS FINE: \frac{1}{3} BAG BOTTOM OF SCREEN DEPTH (ft. bgs): BOTTOM OF WELL DEPTH (ft. bgs): ______75.4 BOTTOM OF FILTER PACK (ft. bgs): ______

ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL.

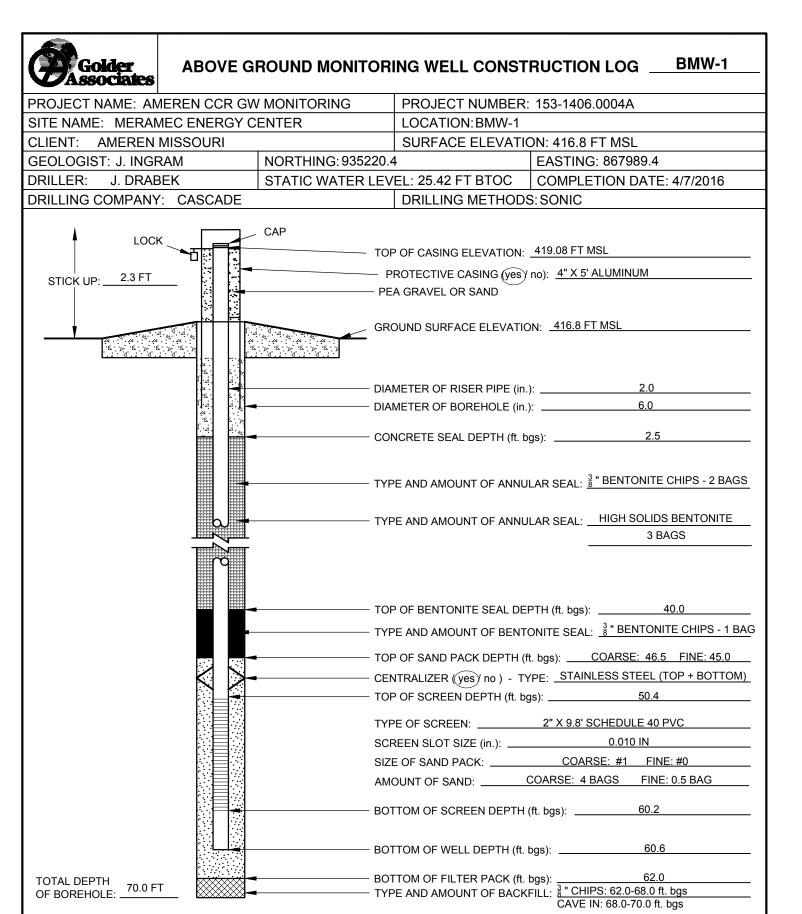
250 GALLONS OF H2O USED DURING DRILLING, HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FT (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON FEBRUARY 4, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

TYPE AND AMOUNT OF BACKFILL: NONE

CHECKED BY: J. INGRAM DATE CHECKED: 4/25/2016

TOTAL DEPTH

OF BOREHOLE: 80.0 FT



ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL.

200 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FT (2000)

MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON APRIL 28, 2016.

FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM

DATE CHECKED: 6/2/2016



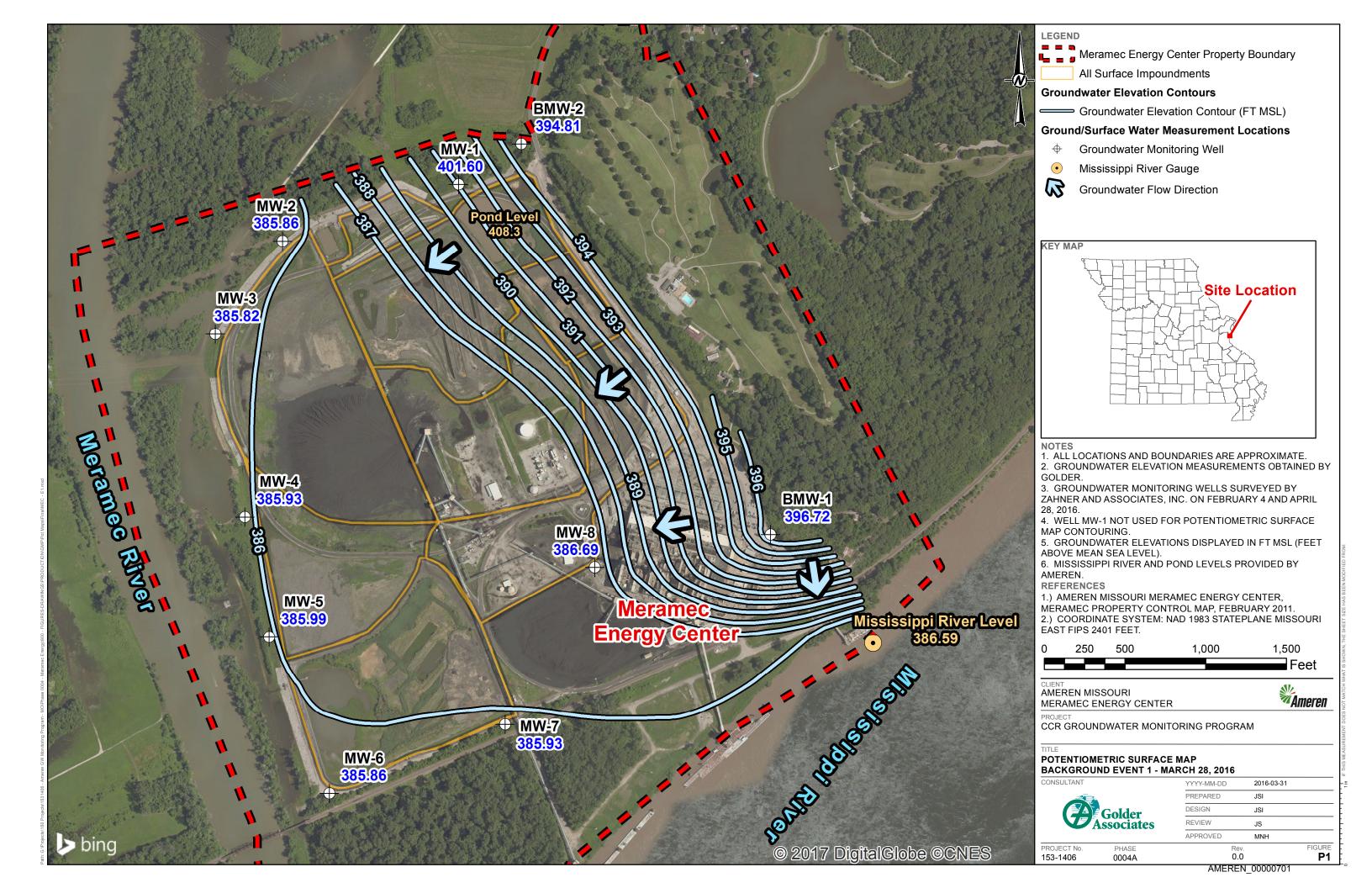
ABOVE GROUND MONITORING WELL CONSTRUCTION LOG BMW-2

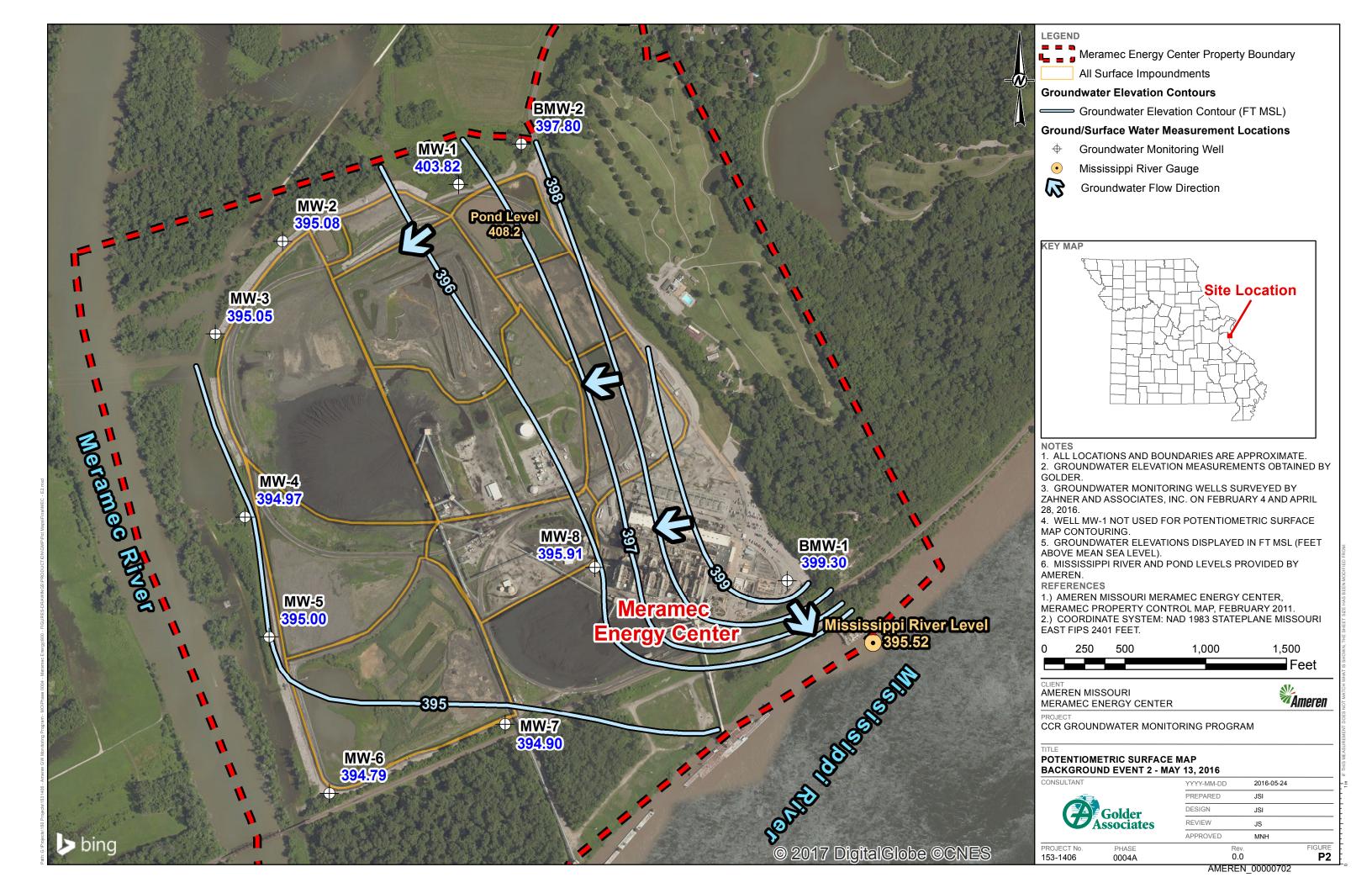
PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0004A SITE NAME: MERAMEC ENERGY CENTER LOCATION: BMW-2 CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 406.8 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 937927.1 EASTING: 866342.2 DRILLER: J. DRABEK STATIC WATER LEVEL: 14.11 FT BTOC COMPLETION DATE: 1/25/2016 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK - TOP OF CASING ELEVATION: 409.02 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ___2.2 FT - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 406.8 FT MSL DIAMETER OF RISER PIPE (in.): DIAMETER OF BOREHOLE (in.): ___ - CONCRETE SEAL DEPTH (ft. bgs): 2.5 TYPE AND AMOUNT OF ANNULAR SEAL: NONE TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 6 $\frac{1}{2}$ BAGS - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 34.7 FINE: 34.0 - CENTRALIZER (yes (no)) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): 37.5 TYPE OF SCREEN: 2" X 4.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: _____COARSE: 1.75 BAGS FINE: \frac{1}{3} BAG BOTTOM OF SCREEN DEPTH (ft. bgs): 42.3 - BOTTOM OF WELL DEPTH (ft. bgs): 42.7 - BOTTOM OF FILTER PACK (ft. bgs): 44.0
- TYPE AND AMOUNT OF BACKFILL: BENTONITE CHIPS - 1 BAG - 6.0 FT TOTAL DEPTH OF BOREHOLE: 50.0 FT ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 120 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FT (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON FEBRUARY 4, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

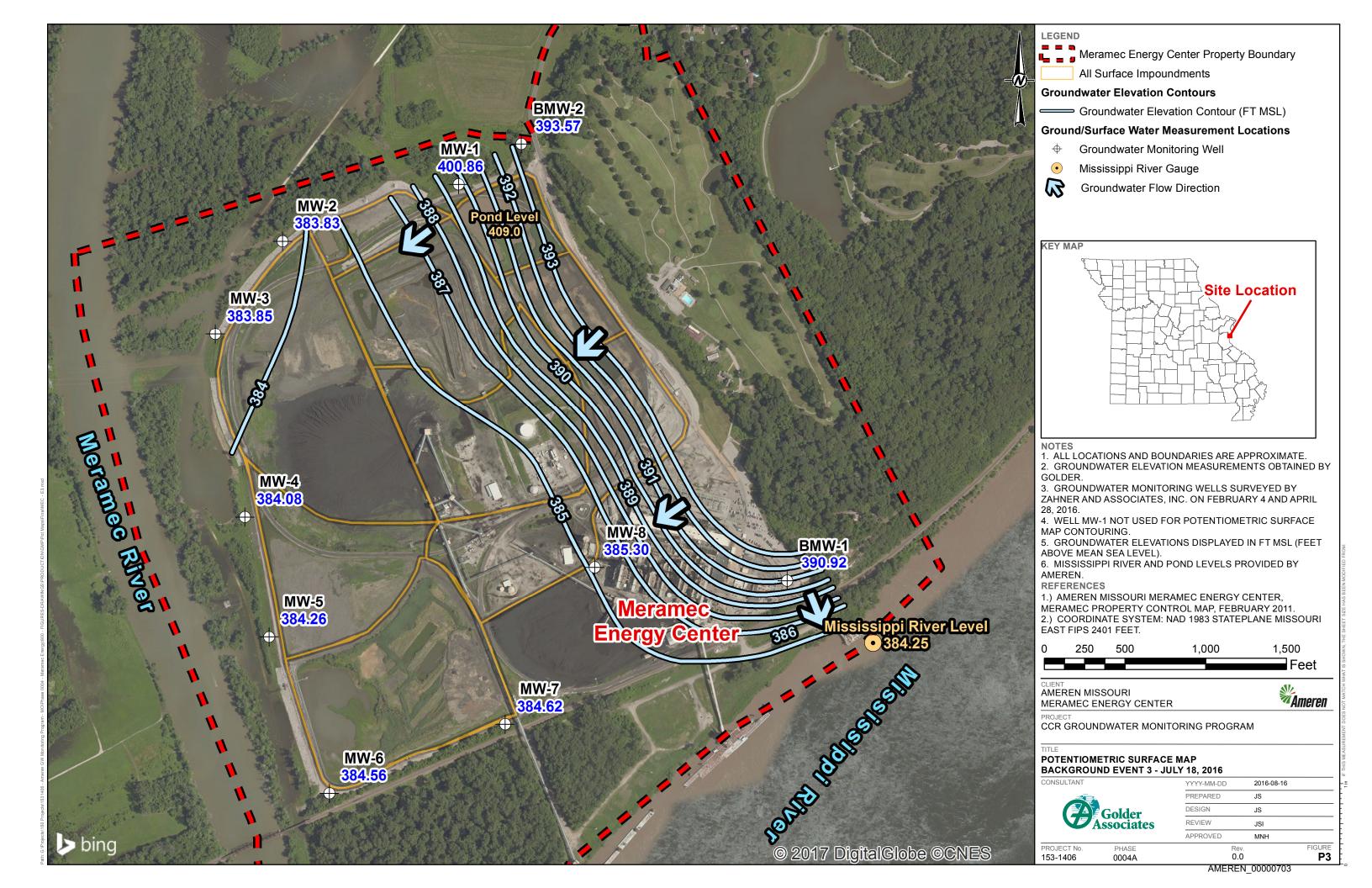
CHECKED BY: J. INGRAM

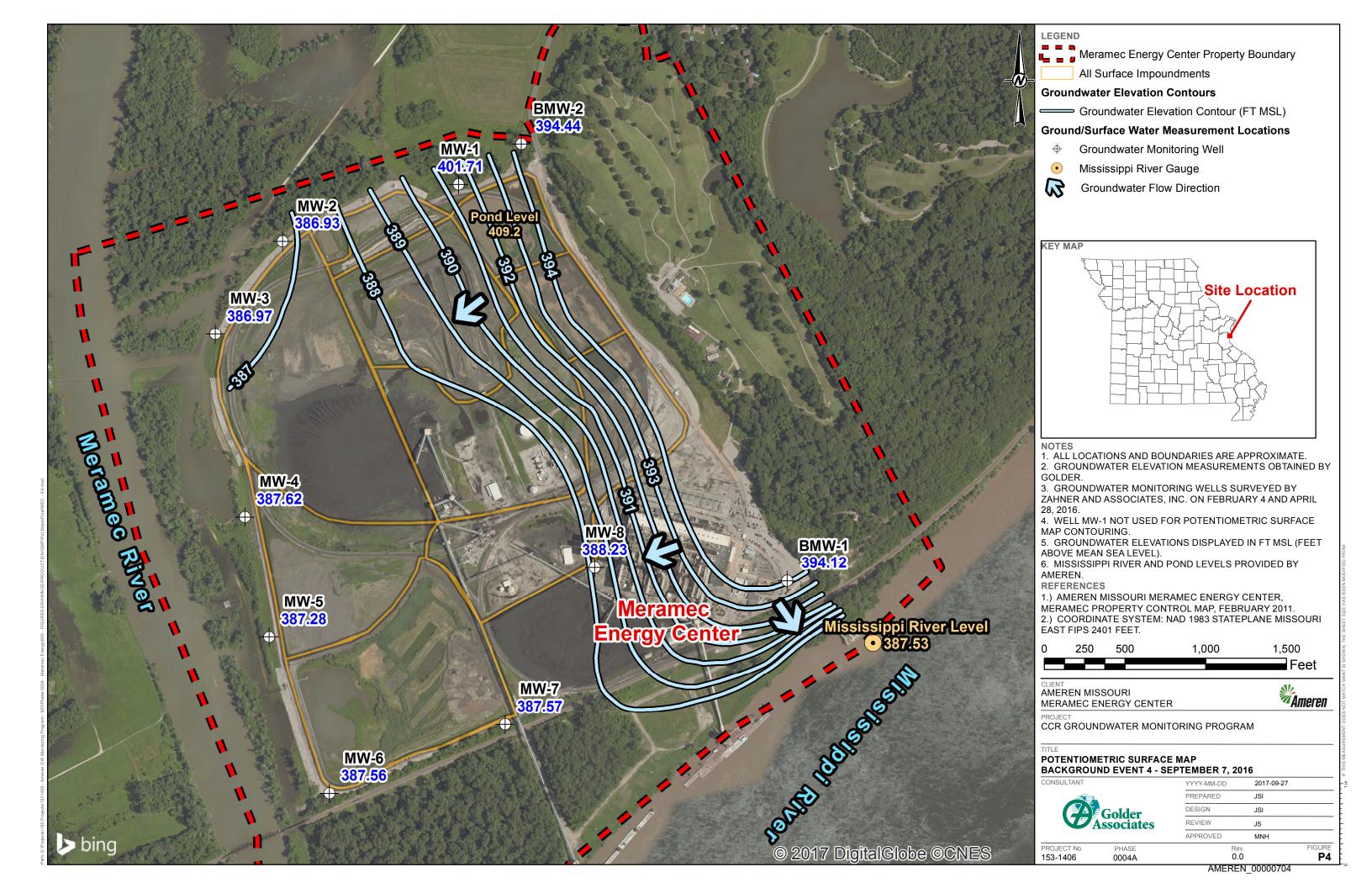
DATE CHECKED: 4/25/2016

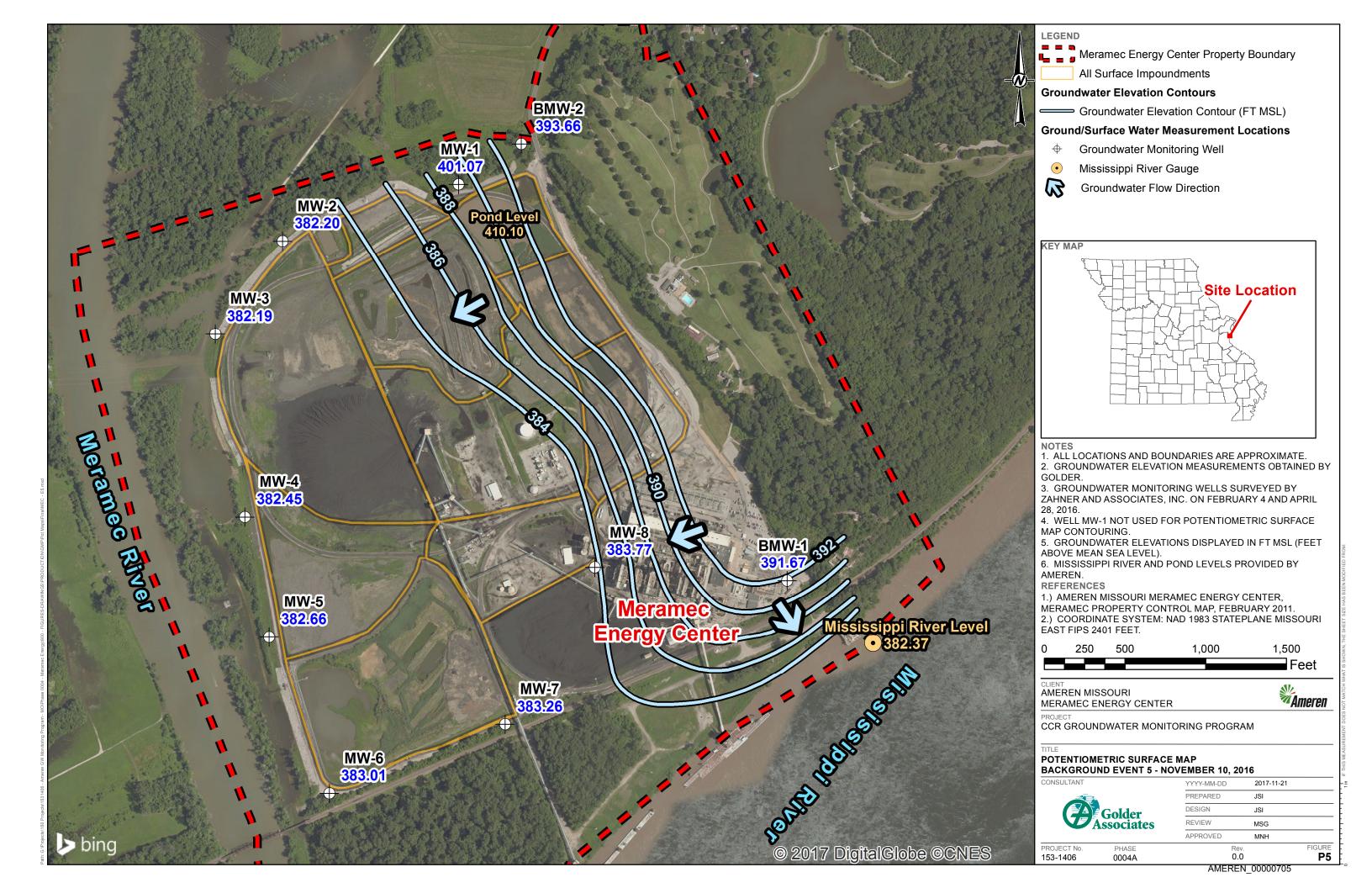
APPENDIX F POTENTIOMETRIC SURFACE MAPS FROM BACKGROUND CCR SAMPLING EVENTS

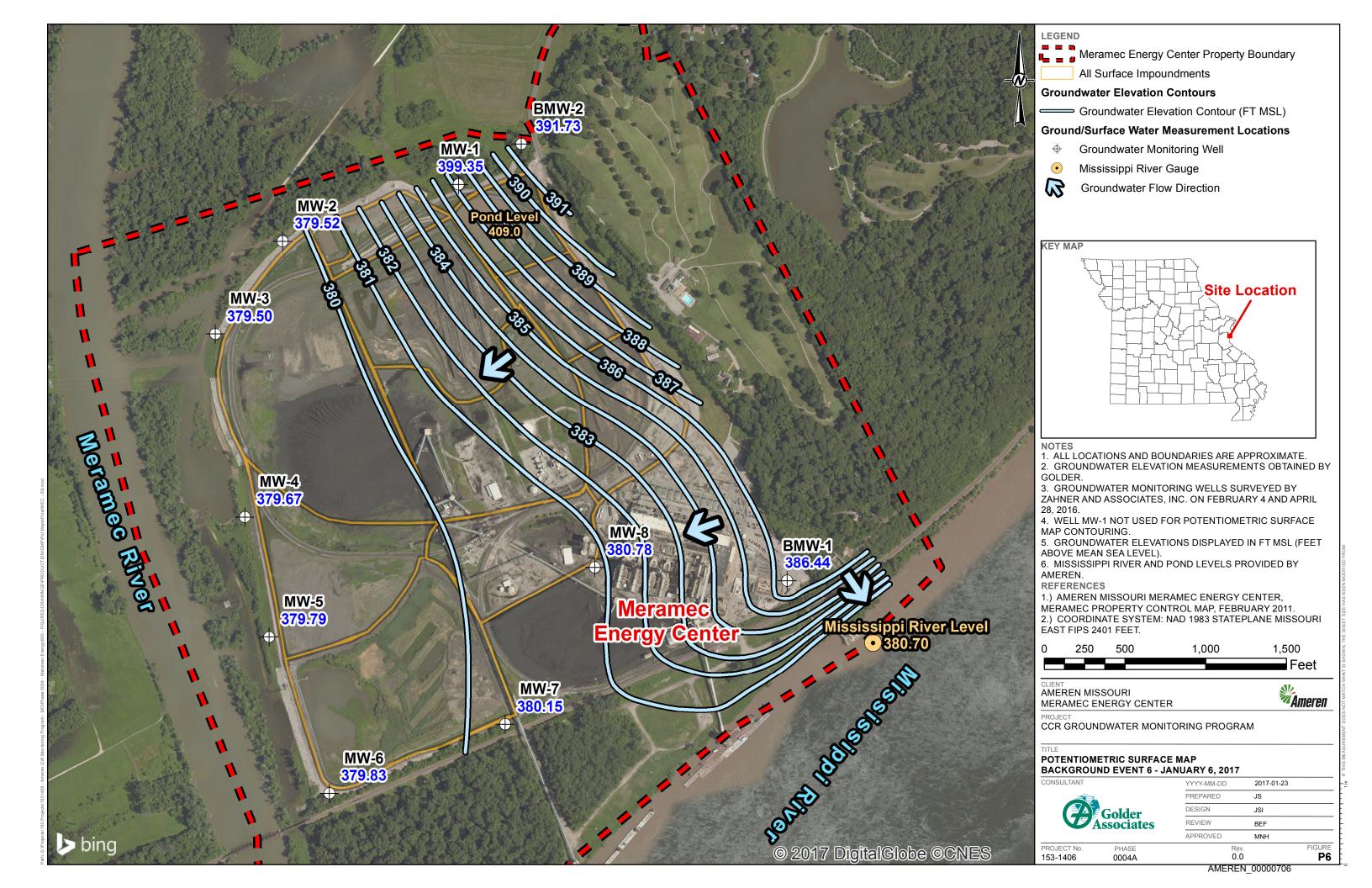


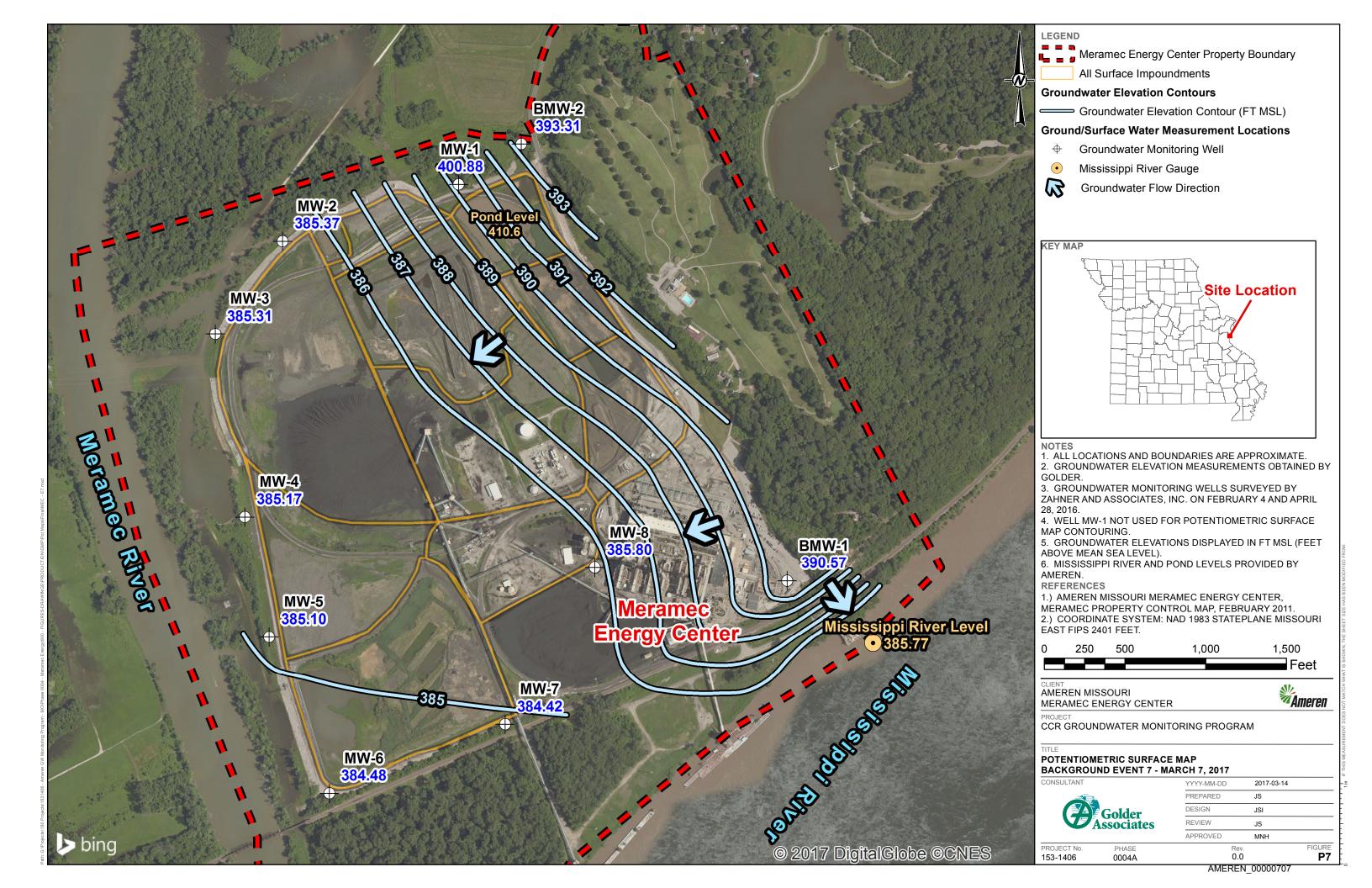


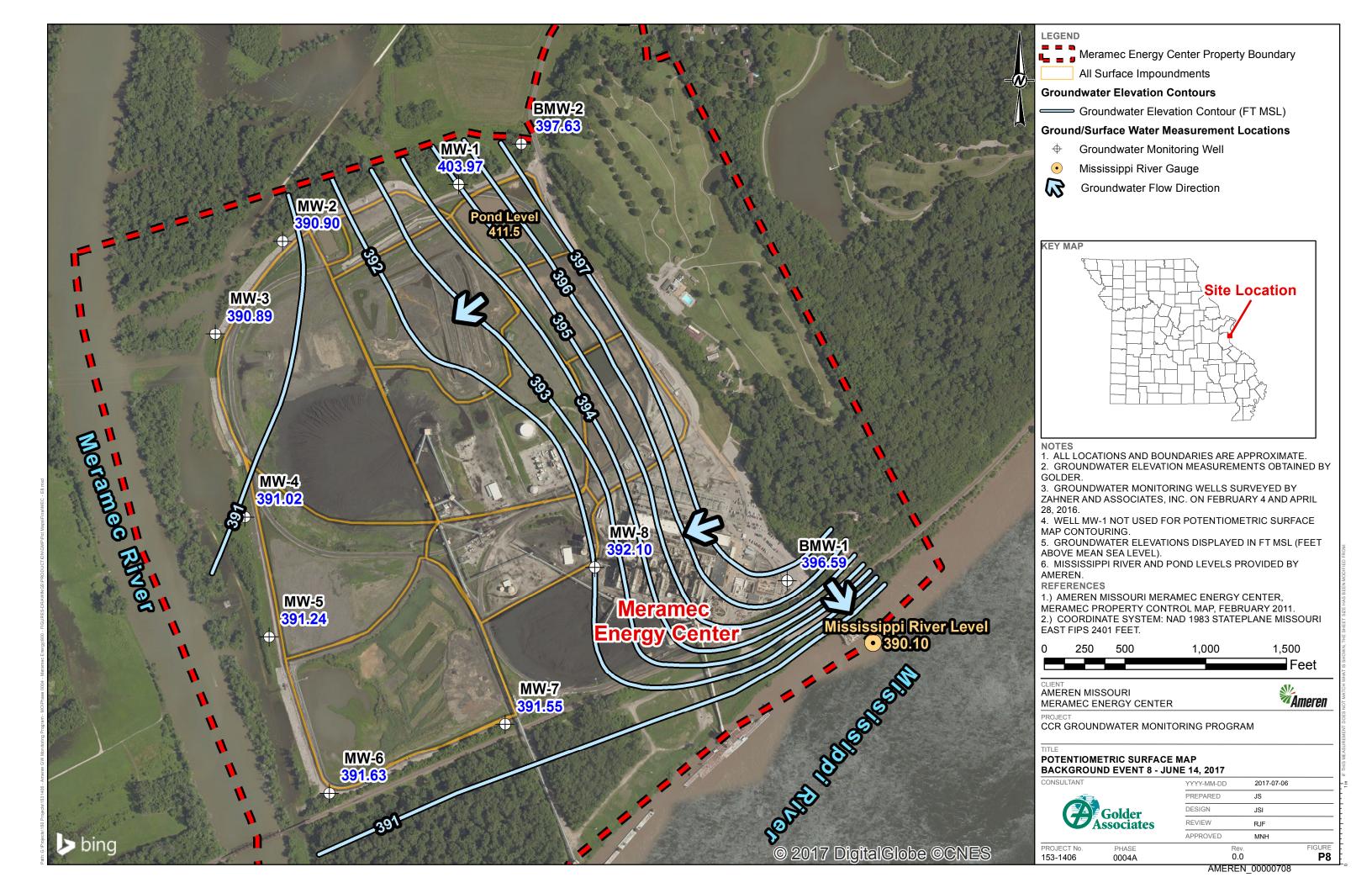








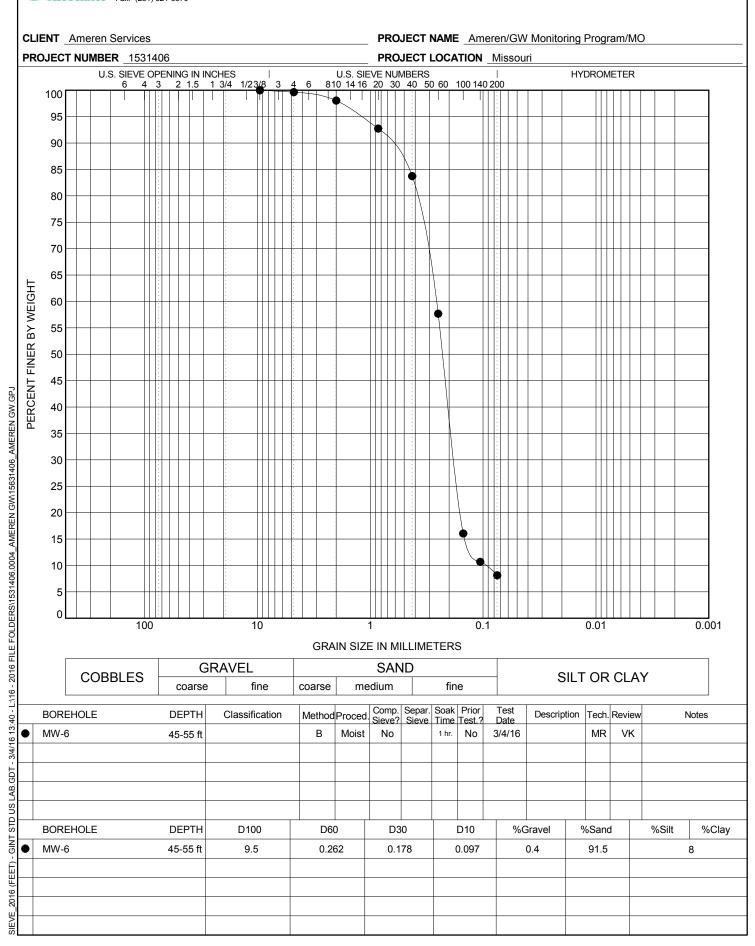




APPENDIX G GRAIN SIZE DISTRUBUTION

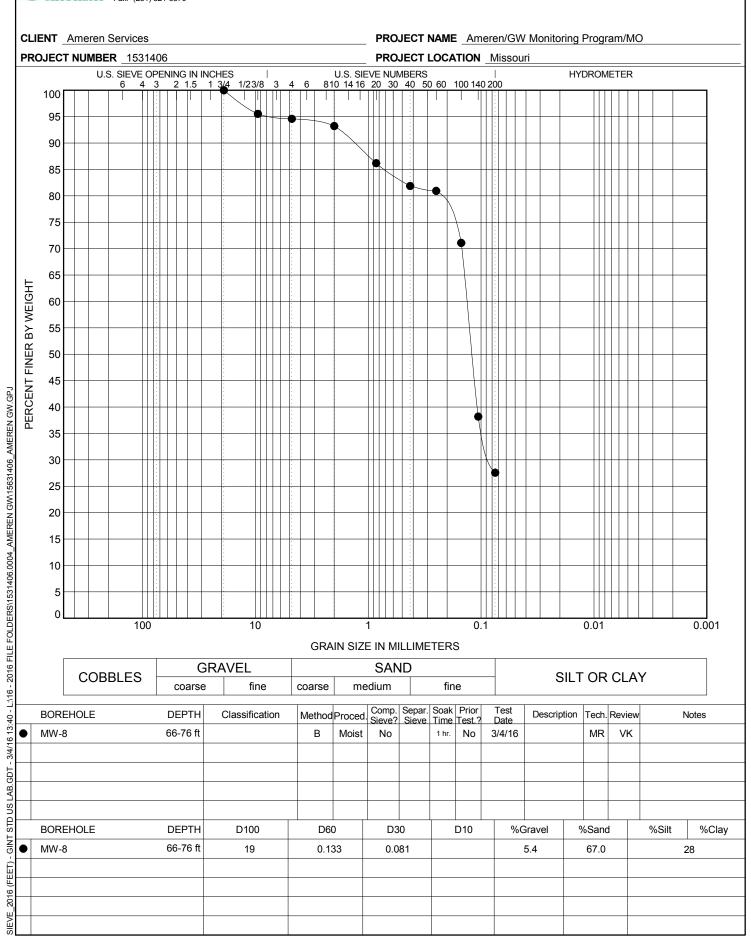
500 Century Plaza Drive, Suite 190 Houston, Texas 77073 Telephone: (281) 821-6868 Fax: (281) 821-6870

GRAIN SIZE DISTRIBUTION ASTM D6913



500 Century Plaza Drive, Suite 190 Houston, Texas 77073 Telephone: (281) 821-6868 Fax: (281) 821-6870

GRAIN SIZE DISTRIBUTION ASTM D6913



APPENDIX H WELL DEVELOPMENT FORMS

Project	Ref: A	meren GV	V Monito	oring	-		Project	No.: 153-	1406.000)4	
Locat	ion	MW-	1								
Monitore	ed By:	75	5	Date	2/5/16		Time	072	ζ]	
Well F	Piezom	eter Data	а								
Depth of	Well (fron	(circle one) top of PVC-or	r ground)		41.25			feet			
Depth of	Water (fré	m top of PVC	or ground)		4,45			feet			
Radius of	Casing				2			inches			
Casing V	olume							feet cubic feet	L 12 G	eal the offen drilling	
Outling v	oranic				8.45.	3= 2	5.4	gallons	ال الالو)	
Devel	opmen	ıt / Purgi	na Dis	charg	e Data					gal the from drilling 150-4 gal total	
Purging N	•			J	Water	Me.				1	
Start Pur	ging		.3	Date	2/5/16	1	Time	1839	5		
Stop Purg	ging			Date	215/16		Time	1139	•	j	
Monitorin	g										
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments	
2/5/16	1017	75	13.46	os.F	1-065	126	1.02	-62.7	4.63	Benove svige block.	cloudy
	1030	95	13.88	7.61	1.057	13.8	0.86	-73.8	4.67	Clear	
T WILLIAM	1045	135	13.79	7.39	1.057	9.11	0.76	-79.1	4.75	clear	
	1115	155	13.78	7.35	1.061	7.37	0.83	-83-1	4.79	Clear	1
[] - J	1130	175	13.88	7.32	1-962	7.43	0.81	-77.5	4.48	cler	
						<u> </u>			w.		1
							4. 6	Mes'	-		1
						 		2	0		ł
								ie.			1
						-		 			
					-sk						1
						-			<u> </u>		1
						<u> </u>					1

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Project Ref: Ameren GW Monitoring

Locat	ion	MW-	2							
Monitore	ed By:	722		Date	2/1/16		Time	084	0	
Well F	Piezom	eter Data	1			Fin	nITD			
Depth of	Well (from	top of PVC or	ground)		36.75		.४५	feet		
Depth of	Water (fror	n top of PVC	or ground)		13.91	-		feet		
Radius of	Casing				2			inches		
								feet		Man a chart
Casing V	olume				2.3 -	24 -		cubic feet gallons	+	150 gal Hzo From OMM
Devel	opmen	t / Purgir	ng Dis	charge	e Data					113 9
Purging N	/lethod				Vaterra					
Start Purg	ging			Date	2/1/16		Time	0930		_ *
Stop Purg	ging			Date	2/1/16	-1	Time	1440		
Monitorin	g				,					
Date	Time	Volume Discharge (gals)	Temp (° <u>C</u>)	рН	Spec.Cond. (<u>►</u> S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
2/1/16	1202	60	-	_	-	_	-	-	13.98	Remove surge block
	1222	70	14.04	9.01	1.142	85.4	501	-13.8	13.95	Cloudy
	1240	80	13.75	8.80	1.144	14.5	0.86	-128.1	14.09	clear
 	1300	110	13.82	8.50	1-145	7.30	0.64	-120.9	14.11	Clear
	1330	140	13.85	8.34	1-146	6.81	0.66	-101.9	14.12	clear
	1345	155	13.72	8,21	1.149	6.97	0.56	-86.2	14.14	clear
	1400	170	13.78	8.00	1.151	6.85	0.65	-123.3	14.13	Clear
	1415	185	13.69	7.85	1-148	5.96	0.71	-117.4	14.13	Cleur
	1430	210	13.80	7.84	1.150	6.81	0-78		14.12	Clear
	1170	at 10	13.07	7.7	1.171	6.61	9.76	-110.1	17/10	clear
	ļ					ļ				
								-		
	,									
						ļ				

Project No.: 153-1406.0004



Project	Ref: A	meren GV	V Monito	oring			Project I	No.: 153-	1406.000)4
Locat	ion	MW-3				j _e		9	*]
Monitore	ed By:	75		Date	2/4/16		Time	07	14]
Well F	Piezom	eter Data	a		, .					
		(circle one)			71 88					
•	,	top of PVC or			33,03			feet		
epth of	Water (fror	m top of PVC	or ground)		12.08			feet		
Radius of	Casing				2			inches		
							17	feet		
Casing V	olume				5 - 2 -	17		cubic feet	ا بد	50 gal 420 From
					5.7.3:	= 17.1		gallons	Τ .	150 5 al 420 from = 168 gal 420
Devel	opmen	t / Purgi	ng Dis	charge	e Data					Jai Ma
ourging N	fethod		_		Waterso					
Start Purg	ging			Date	2/4/16		Time	0802		1
Stop Purg				Date	2/4/16		Time	1330		i
Monitorin	g				,					
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
21416	09715	7.5	12.26	7.12	1-144	71000	1.65	12.1	12-10	Slightly moddy
1 111	1030	83	11.39	6.95	1.152	71000	0-54	-53.4	11.00	4254 20004
	1045	90	11.90	6-95	1.160	71000	0.62		12.01	yesin moddy
	1100	97	12.21	6.86	1.148	71000	0.68	-45.1	12.09	muddy
	1115	120	13.02	6.75	1.148	141	0.72	-40.0	12.06	cloudy
200	1130	155	12.33	6-13	1.158	71000	1.23	-38.7	12.00	Remove surge block, moldy
	1200	165	12.80	6.48	1.155	239	1.05	- 53.4	, mg ,	Slightly modely
	1225	175	12.95	6.69	1.158	58.4	0.85	-57.3	11.96	cloudy,
	1140	190	13.66	6.67	1.150	291	0.62	-62.7	12.01	VEST closely
	1255	205	13.43	6.68	1.152	25.0	0.70	-69.3	11.91	clear
	13/0	215	13.80	6.71	1.154	9.93	0.73	-68.1	11.90	Clear
	1325	225	13.80	6.70	1.152	8.15	0.68	-65.6	11.26	clear
						1			12	
						- 1				
					6			9.0		The labor was a second

post deu't TD: 33.09



Project Ref: Ame	ren GW Mon	itoring	- 1		Project	No.: 153-	1406.000	04
Location N	w-4							
Monitored By:	JS	Date	2/8/16		Time	0729		
Well Piezomete	er Data							1
•	rcle one)	1)	45.25] feet		
Depth of Well (from top	•					7		
Depth of Water (from to	o of PVC or grou	nd)	17.94			feet		
Radius of Casing			/2			inches		\
		-				feet		
Casing Volume				A: :		cubic feet	1000	cal Ho from dilling
			7 .3:	21 221		gallons	4 (80	7
Development /	Purging D	scharg	e Data				ž	gal Hzo from diffling 221 gal Hzo total
Purging Method	7/ "	-	Mate	AVVI			1,7	
Start Purging		Date	2/8/16	N. El	Time	082	8	
Stop Purging		Date	2/8/16		Time	\$700		
Monitoring								
	/olume Tem	I nH	Spec.Cond.	Turbidity (NTU)	Dissolved Oxygen	Redox Potential	WL (ft BTOC)	Appearance of Water and Comments
	(gals) \ \ —	J. Cal		()	(mg/L)	(+/- mV)	< ₆ <	

Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments	
816	1021	85	13.11	7.68	1.320	71000	0.99	-69:0	18.20	muddy	
	036	90	1.36	9.61	1-318	7/000	1.54	-84-2	18.36	middy	
	1050	19995	5 86	7,41	1.312	71000	2.04	-73.3	18.82	myddy	
	1105	97	6.68	7.21	1-307	71000	1.57	-48.2	18.39	modely	
	120	18	11.75	7.36	1.327	71000	7.08	-69.0	18.40	muldy	
	1135	103	11.32	7.18	1.334	71000	3.20	-46.4	18.36	Signally muldy, Kemore Surge	6/00
	1150	120	11-46	7.30	1.342	124	1.93	-62-8	18.37	Very claudy	
	1210	165	11.03	7.08	1-340	139	1.50	-61.2	18.40	very cloudy	
-	1225	190	11.47	7.24	1.323	104	1.24	-69.0	18.40	cloudy dump purge water	
	1310	193	4.29	6.99	1.327	124	1.98	-36.4	17/98	Cloudy	
	1330	220	9.64	7.29	1,333	217	1.73	-51.0	18.16	very cloudy	
	345	230	956	7.29	1.316	-	0.86	-59.1	18.21	very cloudy	
	1400	245	10.34	7.25	1.316	163	0.91	1.5	18.25	very cloudy, fow Flow	
	1415	255	10.28	7.23	1.325	51.1	0.66		18.24	Glovdy	
	1430	270	9.20	7.18	1.354	48.6	1.13	-76.5	18.26	Slightly cloudy	
	1456	275	2-82	7.20	1,342	42.4	2.53		18.19	Slight down	
	15/5	279	6-25	7.20	1.340	70.2	2.01	-59.3	18.25	Styldy cloudy	
	1530	290	7.50	7.19	1.338	30.8	0-63	-68.4	18.27	Chear	
	1545	300	9.98	1.26	1.327	48.5	1.02	-11.1	18.28	Slighty closely	
	1600	307	10.05	7.24	1.332	64.1	0.76	-71.5	18.31	slighty cloudy	
	1615	317	9.68	7.75	1.340	70.5	1.06		18.32	cloudy	
	1630	335	9.41	7.24	1.320	38.0	1.30	-73.5	1835	slightly cloudy	
	1645	345	8-66	7.24	1.325	24.5	1.35	71.4	18.36	Clear	
	1650=	350	8.43	7.24	1.328	23.6	1.18	-69.2	18.36	clear	
						-					
											

post Devil TD: 45.17



14	•	44 1 5				-		* -	."	1 40
Locat	ion	MW- 5	- 91							18 To 10
Monitore	ed By:	- 2 S		Date	2/9/16	1.7	Time	0800		
Well F	Piezom	eter Data	1		1					
		(circle one)								
Depth of	Well (from	top of PVC or	ground)		62.70			feet		
Depth of	Water (fror	n top of PVC	or ground)		17.98			feet		
Radius of	Casing				R			inches		
	-						•	feet		
Casing V	olume				-		_	cubic feet		to form doubling
_					11.2.3			gallons -	1250	dal His day
Devel	opmen	t / Purgiı	ng Dise	charge	e Data				284	gal total
Purging N	/lethod	_	_	_	Water	<u></u>	-			
Start Purg				Date	2/9/16		Time	0840	•	and the state of
							3	1240	4	
Stop Purg	jing			Date	2/9/16		Time	1240		
Monitorin	g									
		Volume					Dissolved	Redox		
Date	Time	Discharge	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Oxygen	Potential	WL (ft BTOC)	Appearance of Water and Comments
		(gals)	(,		(3/ciii)	(1110)	(mg/L)	(+/- mV)	B100)	
2/9/16	0945	160	13.18	8.77	1.270	71000	0.64	-105.6	18.89	muddy
	1000	195	13.21	8.51	1.263	39,2	1.12	-1094	18.61	strath clardy, know so
	1010	225	13.40	8.28	1.270	21.8	0.92	-124.8	18.60	clear
		240	12.18	8.44	1.297	78-1	1.68	-124.7		Cloudy

Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments	
2/9/16	0945	160	13.18	8.77	1.270	71000	0.64	-105.6	18-89	muddy	
	1000	195	13.21	8.51	1.263	39,2	1.12	-1094	18.61	stypthy cloudy, know su	ye black
,	1010	225	13.40	8.28	1.270	21.8	0.92	-124.8	18.60	clear	
	1045	240	12.18	8.44	1.297	78-1	1.68	-124.7		Cloudy	
	1055		12.91	8.60	1.267	76.7	0.83	-125-8	18.45	cloudy	
	1105	385	13.23	8.32	1.772	43.7	0.76	-1309	18.45	SIATHS Churchy	0 5
C. YUY.	1115	300	12.40	8.13	1.261	55.3	1.33	-124.4	18.29	signif cloudy	*
	1129	303	12.50	8.01	1.265	52.8	1.28	-108.6	18.29	5/32 thy clo dy kuflow	
	1135	306	12.38	2.03	1.270	25.0	1.27	-103.7	18.26	Clear	
	1145	310	12.55	7.90	1.266	20.0	1.26	-92.2	18.25	chear	100
	1205	320	12.31	7.38	1.268	14.4	1-13	-86-2	18.29	Clear	and and
	1215	325	12.36	7.57	1.270	14.4	1.10	-84.9	18.30	clear	
	1225	330	12.33	7.38	1-273	13.5	1.08	-91.1	18.29	clear	
	1235	337	12-41	7.37	1.277	13.0	1.65	-89-4	18.22	clear	3.24
									30		The Section of
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						<u> </u>					1.7
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post Devit TD: 62-72

Project Ref: Ameren GW Monitori	ng	Project No.: 153-1406.0004	
Location MW- & Monitored By: \(\sqrt{5} \)	Date 2/3/16	Time #3 5 8	
Well Piezometer Data (circle one)			
Depth of Well (from top of PVC or ground)	55.42	feet	
Depth of Water (from top of PVC or ground)	33.36	feet	
Radius of Casing	2	inches feet	a from drilling
Casing Volume	7.3 . 3 = 21.	feet cubic feet #300 g 1 Hz gallons 322 g 1	4otal
Development / Purging Disch	narge Data	SAZ gar	
Purging Method	Waterra		
Start Purging	Date 2/3/16	Time 1322	
Stop Purging	Date 2.13/16	Time 1630	

Monitoring

vionitorin	9									
Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
13/16	1340	50	13,45	7.58	1.474	71000	1.48	-41.2	34.39	muddy
	1355	95	14-46	7.24	1.607	71000	1.13	-54.2	34.30	mold
	1410	130	13.80	7.08	1.666	71600	1.30		34.19	muddy
	1425	175	14.30	4.07	1-690	71000	1.61	-50.7	34.02	muddig
	1440	220	14.10	6.96	1.686	74.1	1.22	-50.1	34.41	Cloudy
Charle	1515	255	14.08		1.723	48.7	1.87		34.20	closely, removes ungeblock
	1529	305	14.42	7.03	1.693	13.9	1.27	-60.3	34.17	class
	1540	335	14.06	6.98	1-688	11.5	1.33	-43.6	33.56	clear plan flow
	1550	346	13.70	6.98	1-702	198	1.28	-409		clear
	1600	343		6-99	1.701	19.5	1-23	-46.1	33.50	Cleav
	1610	352	13.71	6.96	1-699	15.4	1.08		33.51	clear
	1620	360	13.75	6.99	1.699	14.1	1.26		33.46	clear
	1630	367	13.77	6.97	1.699	13.4	1.23	-49.3	33-44	clear
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Post TD: 55.45

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Sheet	_ ` c	of '	



Project	Ref: A	meren GW	/ Monito	ring			Project N	lo.: 153-	1406.000	4
Locati	ion	MW-7	1.0830	30				,1		
Monitore	d By:	55	1-5	Date	1/27/16		Time	1028		d
Dep.** of Radius of Casing Vo	water (from Water (from Casing Clume Copmen Method Iging Iging	eter Data (circle one) top of PVC or n top of PVC	ground) or ground)			ZZ.E	Time	feet feet inches feet cubic feet gallons	+2	od gal Hro used obel 222.5
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (_S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
1/29/6	1037	38	14.60	9.16	1.462	71000	1-31	-262.3	32.11	mvdd y
1	10年0	75	5.00	8.81	1.706	71000	1-61	-260.2	32105	Muddy
	1105	92	14.86	9.70	1.848	71000	1.50	-260.1	31.92	modely
	1120	167	14.65	8.32	1-851	71000	1-42	-7.64.1	31.69	muddy
	1134	125	14.90	8.06	2.004	71000	1.06	225.4		muddy, surge black remove
16 1 16	1155	175	14.95	7.73	2.083	17.6	0.89	-767.1	32.21	clear
	IAID	-	-	-	A		- 01		-	paise devit
	1305	175	14.25	8.50	2.148	33.3	2.81		31.81	clear , resume a unge
	1325	215	14-74		2.182	12.4	1.31		32.14	clear
-	1335	242	15.12	7.96	2.200	11-3	6.98	-261.1	32.02	clear
	1345		15.00	7-72	2.200	10.2	6-92	-256.7	32.05	clear , fourton
	1355	255	15.07	7.67	2.217	16.3	1.14	-	31.90	clear, four flow
	1415	265	5.00	7.84	2.220	8 45	1.03	-261,5		alear / Implow
	1425	265	14.77	7.74	2.217	7.76	1.32	-241.8	31.90	clear, Low flow
	440				2.219	9.12		~ 700 D	31.80	clear, four flow
	1455	270	14.19	711	2.212	9.22	1.76	-1652	31 20	clear, for flow
		273	4.12	7.17	2-210	9.10	1.30			clear, Low flow
1	1515	274	14.17	7.14	2.217	9.08		-183-h	21.73	Clear, Low Place
	-	7.0	1157			1.0		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	3.12	
									100	
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	2 24									
100										

post TD- 52.92

Project	Ref: A	meren GW	Monito	ring		4.	Project N	o.: 153-1	406.0004	25
Locati	on [MW-1	84	200						
Monitore		35		Date [2/3/16	100	Time	073	5	
Well P	iezome	eter Data								
		(circle one)			1 - 000	/ /4.				
Depth of V	Vell (from t	op of PVC or	ground)	Į	78.80	1,000		feet		
Depth of V	Vater (from	top of PVC o	r ground)	[87-78	19 3	A	feet		XV. The Control of th
Radius of	Casing			[2	1, 30,		inches		
	7554			[`	feet		and I was from death
Casing Vo	lume			-10		7 3-0		cubic feet	4	1280 gal 190 til
Juding ve					10-5 83 =	31,5		gallons		
					1 34					282 gal Hzo total
Develo	pmen	t / Purgir	ng Disc	charge	Data					
Purging M	lethod				Wattern					
				Date	2/3/16		Time	0754		
Start Purg							Time	1336		
Stop Purg	ing			Date	2/10/16		Time	1 7 7 5		
Monitoring	1									
Mouroni	9		_	_	-					
Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
2/3/16	0833	90	13.47	8.03	1.181	71000	0.56	-15.4	40.98	very andly, gray
V 3/18	0845	110	13,12	7.89	1.163	7/000	0-54	-32.6	41.32	very muldy/stry, gray
17.70	0855	145	3.54	7.11	1.191	71800	0.63	12 54.9	46.84	Very dutte gray
	0910	175	13.67	7.69	1189"	7/000	0-72	-77-1	40.97	very middy gray
	0925	210	13.42	7.60	1.191	71000	0.80	-94.6	41.65	very mostly, a vay
	0940	235	13.49	7.53	1194	71006	0.66	-48.1	41.44	Remove surge block , V. muddy
	1005	250	13.55	7.36	1.190	71000	0.67	-100.1	41.19	very muldy, gray
	1020	3/0	13.16	7-56	1.202	71000		-89.0	41.20	very mody gray
	1035	340	13-24	7.47	1-200	7/006	0.90	-93.4	39.41	100
	1650	355	14.07	7.44	1-194	71000	1.00	-93.3	1	very mody, gray
	1105	373	13-65	1	1.198	71000	0.69	-89-2	41.00	yeary mudding gray
	11110	415	13.40	7.39	1.196		0.72	-90.4	38.46	Very muldy Gray RON Flow
	1145	435	10.33	7.42	1.176	71000	0.65	-86.6	38.39	very muldy, dark grave
	1200	443	10.12	7.46	1.168	71000	1.77	-87.8	38.40	yery mucky, dark gray
214/11	1339	443	-	1.70	1.168	-	-		17.10	TD: 78.25, Startowne
~ UID	1616	448	-	-	-	-		-	17.36	10:77.77 Frank evere
2 14/11	I P W PB	VIA	Was a second	-		-	1	1		
214/16		149	-	-		7/000		_	3.8.20	
2/10/16		530	-	-		7/000	=		39.19	FINT DUCYE, TO: 71-66



Project Ref: Ame	eren GW	Monito	ring			Project N	No.: 153-1	406.000	4
Location	BMW	-26						1.	
Monitored By:	55		Date	2/5/16		Time	124	<u> </u>	
Well Piezomet	er Data								
Depth of Well (from top		ground)	100		43.99		feet		
Depth of Water (from to	op of PVC o	r ground)		13.99			feet		i.
Radius of Casing				2			inches		
Casing Volume 7.3.3 = 21.9						7	feet cubic feet gallons	+120	gal HzD from dr. iling 2 g-1 Hz 0 to tal
Development /	Purgin	g Disc	harge	e Data				14	2 g-1 H20 ts fal
Purging Method				Waters	^				
Start Purging			Date	2/3/16		Time	1300		
Stop Purging			Date	2/5/16		Time	1544		
Monitoring				·					All and a second
E .	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments

										9	WIOTHOTH
	Appearance of Water and Comments	WL (ft BTOC)	Redox Potential (+/- mV)	Dissolved Oxygen (mg/L)	Turbidity (NTU)	Spec.Cond. (S/cm)	рН	Temp (°)	Volume Discharge (gals)	Time	Date
	nuddy	14.66	-44.2	0.81	71000	0.877	7-59	13.42	30	1320	a 5/16
	Juddy	14.80	-50-8	0.64	71000	0.876	7.43	13.57	45	1335	
	moddy		-75.4	0.83	71000	0.816	7.49	13.41		1350	
	muddy		-68.0	0.80	7:1000	D. 834	7.46	13.40	75	1405	
	clear	14.99	-53-6	0.78	294	0 839	7.41	13.32	90	1420	
1	o lear	14.89		0.97	737	6 841		13.02	105	1435	
	Clear	14-21	-63.3	089	27.5	0.841	7.52	1312	120	1450	
A		15.50		0.92	34.7	0.857	7,44	12.87	135	1505	
	clear	15.60		0.96	16.0	0.863	7.41	13.50	150	1520	
	clesv	15.59	-58.4	0.97	13.1	0.870	7.35	13.31	165	1535	
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Project Ref: Ameren GW Monitoring

Locati	ion	BMW-	1a								
Monitore	ed By:	35		Date	4/8/16		Time	090	٥]	
Well F	Piezom	eter Data	ı								
		(circle one)			72.40			1			
Depth of '	Well (from	top of PVC or	ground)		62.90		/_	feet	2		
Depth of '	Water (fror	n top of PVC	or ground)		25.23			feet			
Radius of	Casing				2			inches			
								feet			
Casing V	olume						-	cubic feet	. 7	an altion	Lustling
					10.4 .	3= 31.	.ر	gallons	7 -	o gant.	
										222	- 1 total
Devel	opmen	t / Purgii	ng Dis	charge	e Data					734	gal total
Purging N	/lethod				Water	'a					
Start Purg	ging			Date	4/8/16		Time	0931	. 1]	
Stop Purg	aina			Date	4/8/16		Time	1630]	
					4 57.5					•	4. 4. 3
Monitorin	g —										Q(Hain)
Date	Time	Volume Discharge (gals)	Temp (°)	рΗ	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Wa	ater and Comments
	0953	5	12.58	7.26	1.468	71000	5.54	212.0	39.30	Very moddy /4	SAY, Q: 14min
719	0943	&	1324	7.05	1.521	71000	4.49	63.2	32.52		11 /1: / 4/min
	0953	10	13.42	6.96	1.521	71600	4.07	8.5	32.59		11 Q:14/min
-103	003	12	13.04	7.00	1.540	71000	3.77	-20.0	32-67		1 Q:094/min
	1013	15	14.14	6.99	1-552	71000	2.87	-26.1	31-46		1 0:14min
	1033	20	13-68	6.33	1.616	71000	3.61	9.6	35.95	14 (1 11	9
CAMPA	1053	30	14.42	6.83	1.657	71000	2.32	-29.6	35-10	muddy gray	10:24min
	1113	58	14.13	6.93	1.665	71000	2.31	9,1	77.13	muddy) gray	2=2.4
	1133	75	12.77	694	1.627	71000	2.17	-12.6	46.63	muddy / gray	0=3.0
20 N	1213	95	15.18	6.34	1.629	71000	1-81	-15 2	46.95	muddy large	D=3.0
p .	1295	110	13.74	7.11	1.645	71000	3.12	-143.8	38.11	Renove strye	block, Q=5.0 A
	1306	130	14.04	6.93	1.700	948	4.14	-29.4	58.32	stime clum	The second secon
	1320	140	14.90	6.56	1.678	659	2-43	-15.9	42.72	cloudy	Ø=2.5
	1335	150	15.70	6-54	1.668	614	3.08	-34.7	39.34	cloudy '	Q=3.0
	1355	167	15.17	6.46	1.662	790	1-12	-16.4	45.19	Cloudy	0-3.6
	1415	186	15.06	6.84	1.686	836	1-75		49.52	Clouly	0-30
	1435	205	13.41	6.83	1.740	71200		-39.4	50.11	cladylgray	Q= 4.0
	1525	230	19.60	6.52	1.725	71000		11.7	31.19	aloudy grad	0.3.0
	1540				1.711			42.4	42 52	cloudy / Ratty	Q=3.0
	1555	260		6.61	1.730	71000	1.13	-21 0	47.02	cloudy/gray	1 0=3.0
	1610	280	13.45	0.31	1.614	71000	1.13	41/8	17.67	pause pur	46
	1042	-		-			-			Piss por	}
		1		1	The second secon		Marie Control				

Project No.: 153-1406.0004

Project	Ref: A	meren GW	/ Monito	oring			Project No.: 153-1406.0004				
Locat		BWM-	10	Date	4/15/16		Time	5820]	
Well F	Piezom	eter Data	a								
Depth of	Well (from	top of PVC or	ground)		62.90			feet		,	
Depth of	Water (fror	n top of PVC	or ground)		24.74			feet			
Radius of	f Casing				λ			inches feet			
Casing V	olume							cubic feet gallons			
Devel	opmen	t / Purgiı	ng Dis	charge	e Data						
Purging N	Method				Water	80		- 1			
Start Pur	ging			Date	4114/14		Time	0838			
Stop Purg	ging			Date			Time				
Monitorin	9								. 70.		
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Commer	
4/11/16	0840	5	15.87	6.52	1.493	71000	1.98	159.3	34.15	middy	
	0850	20	16.36	6.95	1.504	71000	0.90	17.3	43.90	muddy	
	OOPO	37	16.45	6.97	1,504	71000	0.97	-28.0	47.10	muddy	
	0910	46	14.53	6.97	1.503	71006	1.30	-46.8	48.79	muddy	
	0920	60	16.57	6.94	1.513	71000	1.05	-55.1		muddy	
	6930	80	16.51	6.92	1.528	7/000	1,80	- 20- 6	55.41	muddy	

130

2.01

- 44.9 37.10 cloudy



Project	Ref: A	Ameren GV	V Monite	oring	_		Project I	No.: 153-	1406.000	04
Locati	ion	BMW-	10			<u> </u>				
Monitore	ed By:	22		Date	4/13/16		Time	1421		
Well F	Piezom	eter Data	a		47 34 5					
Depth of	Well (from	(circle one) top of PVC or	ground)		377			feet		1
Depth of	Water (fro	m top of PVC	or ground)	1	177 N 2 7			feet	10	ce page 1
Radius of	Casing							inches	3 26	
Casing Vo	olume							feet cubic feet gallons	/	
Devel	opmer	ıt / Purgiı	ng Dis	charg	e Data			-		
Purging M	-	J	•	Ŭ	Waterva					1
Start Purg				Date	4 13 16		Time	083	7	1
Stop Purg				Date	11,5110		Time	1603		- CA-
Stop Fulg	jiiig			Date] time	160		
Monitoring	g									
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
4/13/16	1448	320	17.07	6,96	1.705	126	1,66	-57.6	37-15	clardy
	1508	325		6.95	1.701	115	1.43	-57.3	36.75	cloudy
	1528	330	17.00	6.91	1.701	150	1.31		36.92	dovdy
	1548	335	17,00	6-89	1-698	151	1.41	- 56.8	36.81	cloudy
				 						
	Marie Collins	11 -c.								
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APPENDIX I CCR MDNR WELL CERTIFICATION FORMS

MISSOURI DEPARTMEN	_	REF NO		DATE RECEIVED				
NATURAL RESOURCES			0304699	OUTOKNO		03/14/201	6	
DIVISION OF		CR NO		CHECK NO.		170083		
🛮 🧸 🛞 🛮 GEOLOGY AND LAND S	URVEY	STATE WELL NO)		REVENUE NO.			
(573) 368-2165		A206420 0	03/15/2016				031416	
MONITORING WELL		ENTERED NRBA	ASSM	APPROVED B	Y	F	ROUTE	
CERTIFICATION RECORD			PH3					
			1/2016 03/14/2016					
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS		DRILLING CC	ONTRACTOR					
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOUI	RI C/O BILL KUTO	SKY				VARIANCE GRANTED BY DNR	
OWNER ADDRESS 3750 S LINDEBERGH BLVD			STATE MO			NUMBER		
SITE NAME MERAMEC ENERGY CENTER			WELL NUMBER MW1			COUNTY ST LOUIS CITY		
SITE ADDRESS 8200 FINE ROAD			CITY ST LOUIS			STATIC WATER LEVEL 4.6 FT		
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND DI SURFACE COMPL PLACED	ETION WAS				N OF WELL		
X ABOVE GROUND LENGTH 5.0 FT. FLUSH MOUNT DIAMETER 4.0 IN.	DIAMETER 12.0 LENGTH 2.5 FT.	IN.	X CONCRET OTHER	E		38° 24 90° 20		
TEOGRAMOGIVI PRAMETER 4.0 IV.	LLNO111 _2.511.		OTTLEK			LEST	LARGEST	
							1/4 1/4	
LOCKING CAP			SURFACE COMPL	ETTION				
WEEP HOLE	Te	- T	STEEL X AL	LUMINUM PLASTIC			WN NORTH	
	- 11				RANGE	RING FOR:	Direction <u>E</u>	
					RADIONL	ICLIDES	PETROLEUM PRODUCTS ONLY	
			RISER		EXPLOSI*	_	METALS VOC PESTICIDES/HERBICIDESS	
ELEVATION FT.	r '	1'		TER 2.0IN.	3vocs	Ш	FESTICIDES/HERBICIDESS	
			RISER PIPE LENGT	<u> </u>	PROPOS	ED USE OF	WELL	
ANNULAR SEAL			HOLE DIAMETER		GAS MI	GRATION WELL	X OBSERVATION	
LENGTH <u>0.0</u> FT.		+	WEIGHT OR SDR#	SCH40	_	CTION WELL	OPEN HOLE	
SLURRY CHIPS					PIEZOM DIRECT			
PELLETS GRANULAR CEMENT/SLURRY	-		MATERIAL					
IF CEMENT/BENTONITE MIX:			STEEL OTHER	X THERMOPLASTIC (PVC)	DEF FROM	TO	FORMATION DESCRIPTION	
BAGS OF CEMENT USED:								
%OF BENTONITE USED:			Name .		0.0 10.0		SLT CLY SLT	
WATER USED/BAG: GAL.					15.0		BILT	
	L	_	BENTONITE SEAL		21.4		SLT	
			LENGTH:27.5		32.7	36.2	SLT SND	
			CHIPS PELL	ETS GRANULAR	36.2	40.0	SDY GRVL	
			SLURRY SATURATED ZONE	HYDRATED				
SECONDARY FILTER PACK			OATONATED ZONE	HIDRATED				
LENGTH: 0.5FT.	-							
			SCREEN					
	-		SCREEN DIAMETE					
			SCREEN LENGTH: DIAMETER OF DRI					
DEPTH TO TOP OF PRIMARY FILTER PACK:32.4FT.			DEPTH TO TOP					
11L1LIX 1 AON	1 1000000000000000000000000000000000000		1					

TOTAL DEPTH: _40.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 01/23/2016 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _______7.6FT.

SCREEN MATERIAL

X THERMOPLASTIC (PVC)

STEEL

OTHER

/ \	OURI DEPARTMEN		REF NO		DATE RECEIVED				
	RAL RESOURCES			00304700	OUEOU NO		03/14/20	016	
	ION OF		CR NO CHECK NO.				170083		
	OGY AND LAND S	URVEY	STATE WELL N	IO		REVEN			
` ,	368-2165		A206421	03/15/2016			031416		
MONITORING WE			ENTERED NRE	ASSM	APPROVE	D BY		ROUTE	
CERTIFICATION	RECORD		PH1 PH2	PH3					
INFORMATION OURD	LIED DV DDIMADV OOL	ITD A OTOD OD		4/2016 03/14/2016					
NOTE: THIS FORM IS NOT TO BE USED FO	LIED BY PRIMARY CON	NIRACTOR OR	DRILLING C	ONTRACTOR					
OWNER NAME AMEREN MISSOURI C/O BILL	_ KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUTO		VARIANCE DNR				
OWNER ADDRESS 3750 S LINDEBERGH BLVD		CITY ST LOUIS			STATE MO	ZIF 63		NUMBER	
SITE NAME MERAMEC ENERGY CENTER			WELL NUMBER MW2			COUNTY ST LOUIS CITY			
SITE ADDRESS 8200 FINE ROAD				CITY ST LOUIS			STATIC WATER LEV 15.1 FT		
	ENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D SURFACE COMPL		DLE SURFACE CO	MPLETION GROU	T LOCATI	ON OF WEL	L	
X ABOVE GROUND L	ENGTH <u>5.0</u> FT.	PLACED DIAMETER 12.0	IN.	X CONCRET	TE	LAT.	38°	<u>24</u> ' <u>27.77</u> "	
FLUSH MOUNT [LENGTH <u>2.5</u> FT.	OTHER			LONG.	90°	20' 38.95"		
				-		ALLEST	LARGEST		
LOCKING CAP				SURFACE COMPL	LETTION	_	1/4	1/4	_ 1/4
WEEP HOLE		-	ㅡ _	STEEL X A	ALUMINUM PLAST	SEC. I	_G003051	TWN NORT	Н
		ΙΓ				RANGE		Direction <u>E</u>	
							RING FOR:		
						EXPLO	NUCLIDES SIVES X	PETROLEUM PRODUCTS ONLY METALS VOC	
		_		RISER		svocs		PESTICIDES/HERBICIDESS	
ELEVATION	FT.			RISER PIPE DIAME	•	•			
ANNULAR SEAL				RISER PIPE LENGT			SED USE O MIGRATION WELL		
LENGTH0.0	DFT.			WEIGHT OR SDR#			ACTION WELL	OPEN HOLE	
							METERS		
SLURRY CHIPS PELLETS GRAN		- 11		MATERIAL		DIREC	CT PUSH		
CEMENT/SLURRY	TE MIV			STEEL	X THERMOPLASTIC (PV	C) DE	PTH	FORMATION	
IF CEMENT/BENTONI	I E IWIX:			OTHER		FROM	ТО	DESCRIPTION	
BAGS OF CEMENT US	SED:			L		0.0	12.4	SLT	
%OF BENTONITE USE						12.4	30.0	STY CLY	
WATER USED/BAG:	GAL.			→ BENTONITE SEAL		30.0 31.2	31.2 34.2	SND STY CLY	
				LENGTH:23.5		34.2	34.6	STY GRVL	
				CHIPS PELI		34.6	45.0	STY CLY	
				SLURRY	HYDRATE				
SECONDARY FILTER	PACK			SATURATED ZONE	L HYDRATE	U			
LENGTH:1.0		-							
<u></u>	=			SCREEN					
		F		SCREEN DIAMETI SCREEN LENGTH					
				DIAMETER OF DR					
DEPTH TO TOP OF PE FILTER PACK:				DEPTH TO TOP _					
		1 1800 1911	** ** ** ** ** ** ** ** ** ** ** ** **	1		1	1		

FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED.

SIGNATURE (PRIMARY COUNTRACTOR)
x JOHN SUOZZI

DETAIL THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI
DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS

SIGNATURE (WELL DRILLER)
x JASON DRABEK

DATE WELL DRILLING WAS COMPLETED
01/23/2016

DIPUMP INSTALLED

PUMP INSTALLED

APPRENTICE PERMIT NUMBER
004484

APPRENTICE PERMIT NUMBER

LENGTH OF PRIMARY FILTER

PACK: _______7.3FT.

SCREEN MATERIAL

OTHER

X THERMOPLASTIC (PVC)

TOTAL DEPTH:

45.0 FEET

MISSOURI DEPARTMEN	_	REF NO		DATE RECEIVED				
NATURAL RESOURCES			00304701	011501/110		03/14/20	16	
DIVISION OF		CR NO		CHECK NO.	170083			
🛮 🧸 🛞 🛮 GEOLOGY AND LAND S	URVEY	STATE WELL I	NO		REVENUE NO.			
(573) 368-2165		A206422	03/15/2016		0314			
MONITORING WELL		ENTERED NR	BASSM	APPROVED B	Y		ROUTE	
CERTIFICATION RECORD		PH1 PH2	PH3					
		03/14/2016 03/	14/2016 03/14/2016					
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NTRACTOR OR	R DRILLING C	CONTRACTOR					
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUT	OSKY			VARIANCE GRANTED BY DNR		
OWNER ADDRESS 3750 S LINDEBERGH BLVD	CITY ST LOUIS			STATE MO			NUMBER	
SITE NAME MERAMEC ENERGY CENTER			WELL NUMBER MW3			COUNTY ST LOUIS CITY		
SITE ADDRESS 8200 FINE ROAD			CITY ST LOUIS			STATIC WATER LEVEL 13.6 FT		
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D		OLE SURFACE COI	MPLETION GROUT	LOCATIO	N OF WELI	<u></u>	
X ABOVE GROUND LENGTH _5.0 FT.	PLACED DIAMETER 12.0	IIN	X CONCRET	-	ΙΔΤ	38° 2	Λ' 7.2"	
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH _2.5 FT.				90° 2			
'			-			LLEST	LARGEST	
						1/4	1/4 1/4	
LOCKING CAP			SURFACE COMPL					
WEEP HOLE	-		STEEL X AI	LUMINUM PLASTIC		G003052	TWN NORTH	
	11	Ш			RANGE	RING FOR:	Direction	
					RADIONI	JCLIDES	PETROLEUM PRODUCTS ONLY	
			Гыст		EXPLOS SVOCS	ves X	METALS VOC PESTICIDES/HERBICIDESS	
ELEVATION FT.	_ ' 	11	RISER PIPE DIAME	TER 2.0IN.	3,003		FESTICIDES/HERBICIDESS	
II.			RISER PIPE LENGT	·	PROPOS	ED USE OF	WELL	
ANNULAR SEAL			HOLE DIAMETER			GRATION WELL	X OBSERVATION	
LENGTH0.0FT.			WEIGHT OR SDR#	SCH40	EXTRA	CTION WELL	OPEN HOLE	
SLURRY CHIPS					DIRECT			
PELLETS GRANULAR	- $ $ $ $		MATERIAL					
CEMENT/SLURRY IF CEMENT/BENTONITE MIX:			STEEL OTHER	X THERMOPLASTIC (PVC)	DEI		FORMATION	
			U OTHER		FROM	ТО	DESCRIPTION	
BAGS OF CEMENT USED:			L		0.0		SLT	
%OF BENTONITE USED:					5.0		CLY SLT	
WATER USED/BAG: GAL.			BENTONITE SEAL		6.4 11.1		STY SND CLY SLT	
			LENGTH:20.0		13.5		STY CLY	
			CHIPS PELL	ETS GRANULAR	22.2		CLY SLT	
			SLURRY		25.0		SND	
		-	SATURATED ZONE	HYDRATED	25.2		STY CLY	
SECONDARY FILTER PACK	_				26.1		SDY GRVL	
LENGTH: <u>0.5</u> FT.			SCREEN		30.0	55.0	STY CLY	
	<u> </u>		SCREEN DIAMETE	ER: <u>2.0</u> IN.				
			SCREEN LENGTH:					
DEPTH TO TOP OF PRIMARY			DIAMETER OF DR DEPTH TO TOP					
FILTER PACK: 47.4FT.		2000	I DELIGION -	<u> </u>				

TOTAL DEPTH: _55.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 01/22/2016 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _______7.6FT.

SCREEN MATERIAL

OTHER

X THERMOPLASTIC (PVC)

MISSOURI DEPARTMEN	_	REF NO		DATE RECEIVED				
NATURAL RESOURCES			0304702	OUTOKNO		03/14/2016	1	
DIVISION OF		CR NO		CHECK NO.		170083		
🛮 🧸 🛞 🛮 GEOLOGY AND LAND S	URVEY	STATE WELL NO)		REVENUE			
(573) 368-2165		A206423	03/15/2016				031416	
MONITORING WELL		ENTERED NRBA		APPROVED B	Y	RO	OUTE	
CERTIFICATION RECORD			PH3 I/2016 03/14/2016					
INFORMATION CUIDDUIFD BY DDIMARY CON	ITD A CTOD OD							
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS		DRILLING CC	DNIRACIOR					
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOUI	RI C/O BILL KUTO	SKY				VARIANCE GRANTED BY DNR	
OWNER ADDRESS 3750 S LINDEBERGH BLVD			STATE MO			NUMBER		
SITE NAME MERAMEC ENERGY CENTER			WELL NUMBER MW4			COUNTY ST LOUIS CITY		
SITE ADDRESS 8200 FINE ROAD			CITY ST LOUIS			STATIC WATER LEVEL 20.25 FT		
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION X ABOVE GROUND LENGTH 5.0 FT.	DIAMETER AND DI SURFACE COMPL PLACED DIAMETER 12.0	ETION WAS	LE SURFACE COI		LOCATION	38° 24'	10.9"	
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH <u>2.5</u> FT.		OTHER		LONG	90 ° 20'	41.94"	
				-	SMALI		LARGEST	
LOCKING CAP			SURFACE COMPL	ETTION	-	1/4 _	1/41/4	
WEEP HOLE	Ч —	— —	STEEL X A	LUMINUM PLASTIC	SEC. LG	003051 TW	VN NORTH	
	IT				RANGE		Direction <u>E</u>	
	- 11				MONITOR			
			_		EXPLOSIV	3.7	ETROLEUM PRODUCTS ONLY ETALS VOC	
	_		RISER		svocs	PE	ESTICIDES/HERBICIDESS	
ELEVATIONFT.			1	TER <u>2.0</u> IN.	2000000		ve.	
ANNULAR SEAL			RISER PIPE LENGT HOLE DIAMETER			D USE OF W	VELL X OBSERVATION	
LENGTH0.0FT.			WEIGHT OR SDR#		EXTRACT	TION WELL	OPEN HOLE	
]		PIEZOME			
SLURRY CHIPS PELLETS GRANULAR	\dashv \mid \mid		MATERIAL	_	DIRECT	USH		
CEMENT/SLURRY IF CEMENT/BENTONITE MIX:			I H	X THERMOPLASTIC (PVC)	DEP.	ТН	FORMATION	
			OTHER		FROM	ТО	DESCRIPTION	
BAGS OF CEMENT USED:			L		0.0	12.4 CL	LY SLT	
%OF BENTONITE USED: WATER USED/BAG: GAL.					12.4		LY SLT	
WATER USED/BAG: GAL.	L		BENTONITE SEAL		15.0 20.0		TY CLY LY SLT	
			LENGTH: <u>31.5</u>		40.0		RVL	
			CHIPS PELL	ETS GRANULAR	41.3	60.0 ST	TY CLY	
			SLURRY		60.0	65.0 SL	.T	
SECONDARY FILTER PACK			SATURATED ZONE	HYDRATED				
LENGTH:1.7FT.	-							
<u></u>			SCREEN					
	F		SCREEN DIAMETE					
DEDTIL TO TOP OF PERMANA		_ -	SCREEN LENGTH: DIAMETER OF DR					
DEPTH TO TOP OF PRIMARY FILTER PACK:57.6FT.			DEPTH TO TOP					
	1 1800 181	CONTRACT OF THE PARTY OF THE PA	1		1	1		

TOTAL DEPTH: _65.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 01/22/2016 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: ______7.4FT.

SCREEN MATERIAL

X THERMOPLASTIC (PVC)

STEEL

OTHER

MISSOURI DEPARTMEN		REF NO		DATE RECEIVED			
NATURAL RESOURCES		CR NO	0304703	CHECK NO.		03/14/2016	
DIVISION OF		CK NO		CHECK NO.		170083	
GEOLOGY AND LAND S	URVEY	STATE WELL NO)		REVENUE	NO.	
(573) 368-2165		A206424 C	3/15/2016				031416
MONITORING WELL		ENTERED NRBA		APPROVED B	Y	RC	UTE
CERTIFICATION RECORD		PH1 PH2 03/14/2016 03/14	PH3 /2016 03/14/2016				
INFORMATION SUPPLIED BY PRIMARY CON	NTRACTOR OR						
NOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	CONTACT NAME						VARIANCE ORANITED BY
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOUR	RI C/O BILL KUTOS	SKY				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDEBERGH BLVD			STATE ZIP 63127		7	NUMBER	
SITE NAME MERAMEC ENERGY CENTER			WELL NUMBER MW5			COUNTY ST LOUIS CITY	
SITE ADDRESS 8200 FINE ROAD				CITY ST LOUIS			STATIC WATER LEVEL 18.4 FT
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND DI		E SURFACE COM	MPLETION GROUT	LOCATION	I OF WELL	
X ABOVE GROUND LENGTH 5.0 FT.	PLACED DIAMETER 12.0	IN.	X CONCRET	E	LAT.	38° 24'	3.54"
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH 2.5 FT.		OTHER			90 ° 20'	
					SMALL	EST	LARGEST
LOCKING CAP			SURFACE COMPL	FTTION		1/4	1/4 1/4
WEEP HOLE	Ļ —		Г	UMINUM PLASTIC	SEC LG	003051 TW	N NORTH
WEET HOLE	Ir	\neg			RANGE _		rection <u>E</u>
	- 11	- 11			MONITORI	NG FOR:	
			_		RADIONUC EXPLOSIVE	1/	TROLEUM PRODUCTS ONLY TALS VOC
	_		RISER		svocs		STICIDES/HERBICIDESS
ELEVATIONFT.			RISER PIPE DIAME				
ANNUL AD CEAL			RISER PIPE LENGT			D USE OF W RATION WELL	ELL X OBSERVATION
ANNULAR SEAL LENGTH0,0FT.			HOLE DIAMETER WEIGHT OR SDR#		EXTRACT		OPEN HOLE
			WEIGHT GICODIC		PIEZOME		_
SLURRY CHIPS PELLETS GRANULAR	_		MATERIAL		DIRECT P	USH	
CEMENT/SLURRY			STEEL	X THERMOPLASTIC (PVC)	DEPT	ГН	FORMATION
IF CEMENT/BENTONITE MIX:			OTHER		FROM	ТО	DESCRIPTION
BAGS OF CEMENT USED:			L.		0.0	10.0 ST	Y CLY
%OF BENTONITE USED:					10.0		Y SLT
WATER USED/BAG: GAL.			DENTONITE OF AL		20.0		Y CLY
			BENTONITE SEAL LENGTH: 43.5		30.0 31.9	31.9 SN 35.0 CL	Y SND
			CHIPS PELLI	ETS GRANULAR	35.0		Y CLY
			SLURRY		46.0	60.0 SN	D
0500NDADY 511 550 5 1 511			SATURATED ZONE	HYDRATED			
SECONDARY FILTER PACK LENGTH:1.5FT.	_						
			SCREEN				
	- 		SCREEN DIAMETE				
			SCREEN LENGTH: DIAMETER OF DRI				
DEPTH TO TOP OF PRIMARY FILTER PACK: 46.9FT.			DEPTH TO TOP				
1 LILIX 1 AON	1 1000000000000000000000000000000000000	0.000	_			l	

TOTAL DEPTH: _60.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 01/22/2016 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____13.1FT.

SCREEN MATERIAL

OTHER

X THERMOPLASTIC (PVC)

MISSOURI DEPARTMEN	_	REF NO		DATE RECEIVED				
NATURAL RESOURCES			0304704	OUEOK NO		03/14/2016	3	
DIVISION OF		CR NO	CHECK NO.		170083			
🛮 🧸 🛞 🛮 GEOLOGY AND LAND S	URVEY	STATE WELL NO)		REVENUE NO.			
(573) 368-2165		A206425 (03/15/2016				031416	
MONITORING WELL		ENTERED NRBA	ASSM	APPROVED B	Y	R	OUTE	
CERTIFICATION RECORD			PH3					
			1/2016 03/14/2016					
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS		DRILLING CO	DNIRACIOR					
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOUI	RI C/O BILL KUTO	SKY				VARIANCE GRANTED BY DNR	
OWNER ADDRESS 3750 S LINDEBERGH BLVD			STATE MO			NUMBER		
SITE NAME MERAMEC ENERGY CENTER			WELL NUMBER MW6			COUNTY ST LOUIS CITY		
SITE ADDRESS 8200 FINE ROAD			CITY ST LOUIS			STATIC WATER LEVEL 33.6 FT		
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION X ABOVE GROUND LENGTH 5.0 FT.	DIAMETER AND DI SURFACE COMPL PLACED DIAMETER 12.0	ETION WAS	LE SURFACE CON			N OF WELL	52.06"	
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH _2.5 FT.	IV.	OTHER					
						LEST	LARGEST	
						1/4	1/4 1/4	
LOCKING CAP			SURFACE COMPL					
WEEP HOLE		_	STEEL X AL	UMINUM PLASTIC			VN NORTH	
	- 11		_		RANGE	RING FOR:	Direction <u>E</u>	
					RADIONU	ICLIDES P	ETROLEUM PRODUCTS ONLY	
	111		RISER		EXPLOSIV SVOCS		IETALS VOC ESTICIDES/HERBICIDESS	
ELEVATIONFT.		1.1	RISER PIPE DIAME	TER2.0IN.				
			RISER PIPE LENGT	H <u>44.7</u> FT.	PROPOSI	ED USE OF V	VELL	
ANNULAR SEAL			HOLE DIAMETER	<u>6.0</u> IN.		GRATION WELL	X OBSERVATION	
LENGTH0.0FT.		+	WEIGHT OR SDR#	SCH40	PIEZOM	CTION WELL	OPEN HOLE	
SLURRY CHIPS					DIRECT			
PELLETS GRANULAR CEMENT/SLURRY			MATERIAL STEEL	X THERMOPLASTIC (PVC)	DEP)TU	FORMATION	
IF CEMENT/BENTONITE MIX:			OTHER		FROM	ТО	DESCRIPTION	
BAGS OF CEMENT USED:			L U					
%OF BENTONITE USED:					0.0 12.9		DY SLT TY CLY	
WATER USED/BAG: GAL.					30.0		DY SLT	
	L		BENTONITE SEAL		42.2	52.0 St	ND	
			LENGTH:39.2		52.0	55.0 SI	ND	
			CHIPS PELL	ETS GRANULAR				
			SATURATED ZONE	HYDRATED				
SECONDARY FILTER PACK								
LENGTH: 0.7FT.	-							
			SCREEN					
			SCREEN DIAMETE SCREEN LENGTH:					
DERTH TO TOR OF REMARK		- 1	DIAMETER OF DRI					
DEPTH TO TOP OF PRIMARY FILTER PACK: 42.0FT.			DEPTH TO TOP					
	1 1000 100	000000 E-000000				- 1		

TOTAL DEPTH: _55.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 01/21/2016 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____13.0FT.

SCREEN MATERIAL

X THERMOPLASTIC (PVC)

STEEL

OTHER

MISSOURI DEPARTMEN		REF NO		DATE RECEIVED			
NATURAL RESOURCES		CR NO	00304705	CHECK NO.		03/14/20	116
DIVISION OF	LIDVEV	OKTO		170083			
GEOLOGY AND LAND S (573) 368-2165	URVEY	STATE WELL		1	REVENUE NO.		
MONITORING WELL		A206426	03/15/2016	ADDDOVED D	V		031416 POLITE
CERTIFICATION RECORD		PH1 PH2		APPROVED B	Ť		ROUTE
OLK III IOATION KLOOKS			/14/2016 03/14/2016				
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NTRACTOR OR	DRILLING	CONTRACTOR				
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUT	rosky				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDEBERGH BLVD	CITY ST LOUIS			STATE ZIP 63127		NUMBER	
SITE NAME MERAMEC ENERGY CENTER			WELL NUMBER MW7			COUNTY ST LOUIS CITY	
SITE ADDRESS 8200 FINE ROAD				CITY ST LOUIS			STATIC WATER LEVEL 33.3 FT
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D SURFACE COMPL PLACED DIAMETER 12.0	ETION WAS	SURFACE CON			ON OF WEL	
X ABOVE GROUND LENGTH 5.0 FT. FLUSH MOUNT DIAMETER 4.0 IN.	IIN.	OTHER	E		38 °2 90 °:		
	LENGTH <u>2.5</u> FT.		T			LLEST	LARGEST
L OOKING OAR			OUDEAGE COMPI	ETTION	_	1/4	1/4 1/4
LOCKING CAP WEEP HOLE	<u></u>	\Box	SURFACE COMPL	UMINUM PLASTIC	SEC. I	0000054	TWA NODTH
WEEF HOLE	١r	\neg			RANGE	3003031	TWN NORTH Direction E
	- 11					RING FOR:	1
					EXPLOS	1/	PETROLEUM PRODUCTS ONLY METALS VOC
	_		RISER		svocs		PESTICIDES/HERBICIDESS
ELEVATIONFT.			RISER PIPE DIAME	TER2.0IN.	PPOPOS	ED USE O	= \\/E
ANNULAR SEAL			HOLE DIAMETER			GRATION WELL	X OBSERVATION
LENGTH0.0FT.			WEIGHT OR SDR#	SCH40	1 =	CTION WELL	OPEN HOLE
SLURRY CHIPS					DIRECT		
PELLETS GRANULAR CEMENT/SLURRY	-		MATERIAL STEEL	X THERMOPLASTIC (PVC)	DEI	PTH	FORMATION
IF CEMENT/BENTONITE MIX:			OTHER	A	FROM	ТО	DESCRIPTION
BAGS OF CEMENT USED:			L U		0.0	6.3	SLT
%OF BENTONITE USED:					6.3		STY GRVL
WATER USED/BAG: GAL.					7.4		CLY SLT
			BENTONITE SEAL		11.2		SDY SLT
			LENGTH:34.5	ETS GRANULAR	21.9 23.6	23.6 40.0	STY CLY SND SLT
			SLURRY	_	40.0	52.0	SND
			SATURATED ZONE	HYDRATED			
SECONDARY FILTER PACK LENGTH:1.5FT.	_						
LENGIN: <u>1.5</u> F1.			SCREEN				
	-		SCREEN DIAMETE				
			SCREEN LENGTH: DIAMETER OF DRI				
DEPTH TO TOP OF PRIMARY			DEPTH TO TOP				

TOTAL DEPTH: _52.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 01/24/2016 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____14.2FT.

SCREEN MATERIAL

OTHER

X THERMOPLASTIC (PVC)

MISSOURI DEPARTMENT OF			REF NO DATE RECEIV		DATE RECEIVED	ED			
NATURAL RESOURCES			00304706		03/14/2016				
DIVISION OF			CR NO	CR NO CHECK NO.					
🛕 │ 🏝 │ GEO				T = =- · · = · · · ·	170083	3			
(3/2)	368-2165	011121	STATE WELL NO			REVENU	E NO.	004440	
MONITORING W				3/15/2016	ADDROVED B	031416			
CERTIFICATION			PH1 PH2	PH3	APPROVED B	Ť		ROUTE	
CENTILICATION	INLCOND		03/14/2016 03/14						
INIEODMATION SLID	PLIED BY PRIMARY CON	NTDACTOR OR							
NOTE: THIS FORM IS NOT TO BE USED		VIRACTOR OR	DRILLING CC	MIRACION					
OWNER NAME AMEREN MISSOURI C/O B	ILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUTOS	SKY				VARIANCE GRANTED BY DNR	
OWNER ADDRESS 3750 S LINDEBERGH BLVE)	CITY ST LOUIS			STATE ZIP 63127		NUMBER		
SITE NAME MERAMEC ENERGY CENT	ER		WELL NUMBER					COUNTY ST LOUIS CITY	
SITE ADDRESS 8200 FINE ROAD			CITY ST LOUIS					STATIC WATER LEVEL 38.2 FT	
SURFACE COMPLETION TYPE	LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D		E SURFACE COM	PLETION GROUT	LOCATIO	N OF WELL	-	
ABOVE GROUND	LENGTH FT.	PLACED DIAMETER	IN.	CONCRETE		LAT.	38° 2	4' 7.75"	
FLUSH MOUNT DIAMETER IN. LENGTH FT						LONG. 90° 20' 14.71"			
						SMAI	LEST	LARGEST	
							1/4	1/4 1/4	
LOCKING CAP				SURFACE COMPLE					
WEEP HOLE				STEEL ALUI	MINUM PLASTIC	_	3000050	TWN NORTH	
						RANGE	RING FOR:	Direction <u>E</u>	
						RADIONI		PETROLEUM PRODUCTS ONLY	
				_		EXPLOSI		METALS VOC	
		_		RISER		svocs		PESTICIDES/HERBICIDESS	
ELEVATION	FT.			RISER PIPE DIAMETE		PD 0 D 0 0		- 14/51	
ANNIII AD SEAL				RISER PIPE LENGTH0.0FT. HOLE DIAMETER0.0IN.			PROPOSED USE OF WELL GAS MIGRATION WELL OBSERVATION		
ANNULAR SEAL LENGTH FT.			WEIGHT OR SDR# 0.0			EXTRACTION WELL OPEN HOLE			
LENGTHFT.					<u> </u>	PIEZON	IETERS	_	
H H .	HIPS			MATERIAL		DIRECT	PUSH		
PELLETS GRANULAR CEMENT/SLURRY				STEEL	THERMOPLASTIC (PVC)	DEF	PTH	FORMATION	
IF CEMENT/BENTO	NITE MIX:			OTHER		FROM	TO	DESCRIPTION	
BAGS OF CEMENT	USED:			L U ——		0.0	0.9	GRVL	
%OF BENTONITE U	SED:					0.9		SND	
WATER USED/BAG:						1.2		SDY SLT	
				BENTONITE SEAL		7.1	10.0	CLY SLT	
				LENGTH:		10.0	20.0	STY CLY	
				CHIPS PELLET	'S GRANULAR	20.0		CLY SND	
				SLURRY	1000.75	21.7		STY CLY	
SECONDARY ETT	'D DACK	Г		SATURATED ZONE	HYDRATED	30.0		SDY SLT	
SECONDARY FILTE		_				32.8 50.0		STY CLY SDY SLT	
LENGTH:	<u>v.v</u> i i.			SCREEN		68.0		SDY SLI STY SND	
				SCREEN DIAMETER	:: <u>0.0</u> IN.	75.5		SND	
				SCREEN LENGTH: _		75.9		STY CLY	
DEPTH TO TOP OF	PRIMARY			DIAMETER OF DRIL					
FILTER PACK:	<u>80.0</u> FT.			DEPTH TO TOP	<u>80.0</u> FT.				

FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED.

SIGNATURE (PRIMARY COUNTRACTOR)

SIGNATURE (PRIMARY COUNTRACTOR)

PERMIT NUMBER

006284

I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI
DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS

SIGNATURE (WELL DRILLER)

X JASON DRABEK

TOTAL DEPTH: ____80.0 FEET

DATE WELL CASING, HOLE DIAMETER AND GROUT USED.

DATE WELL DRILLING WAS COMPLETED
01/24/2016

10/24/2016

10/24/2016

PUMP INSTALLED

PUMP INSTALLED

APPRENTICE PERMIT NUMBER
004484

APPRENTICE PERMIT NUMBER

LENGTH OF PRIMARY FILTER

PACK: _____0.0FT.

SCREEN MATERIAL

OTHER

THERMOPLASTIC (PVC)

MISSOURI DEPARTMENT OF		REF NO		DATE RECEIVED					
NATURAL RESOURCES		00305960		05/26/2016					
DIVISION OF			CR NO		CHECK NO.			_	
			OTATE MELL NO	\		DEVENUE	17009	9	
(573) 368-2165			A206734 (REVENU	E NO.	052616	
MONITORING W			ENTERED NRBA	05/31/2016 .SSM	APPROVED B	052616 3Y ROUTE			
CERTIFICATION			PH1 PH2	PH3	ALLIKOVEDE			ROOTE	
OLKIII IOAIIOK	INLOGNE			/2016 05/26/2016					
INFORMATION SUPI	PLIED BY PRIMARY CON	NTRACTOR OR	DRILLING CO	ONTRACTOR			<u> </u>		
OWNER NAME AMEREN MISSOURI C/O BI	ILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUTO:	SKY				VARIANCE GRANTED BY DNR	
OWNER ADDRESS		CITY			STATE	ZIP		NUMBER	
370 S LINDBERGH BLVD		ST LOUIS			MO 631				
SITE NAME MERAMEC ENERGY CENT	ER		WELL NUMBER BMW1			COUNTY ST LOUIS CIT		COUNTY ST LOUIS CITY	
SITE ADDRESS 8200 FINE RD				CITY ST LOUIS				STATIC WATER LEVEL 25.42 FT	
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF DIAMETER AND DEPTH OF THE HOLE SURFACE COMPLETION GROUT LOC							LOCATION OF WELL		
X ABOVE GROUND	LENGTH 5.0 FT.	PLACED DIAMETER 12.0	IN				LAT. <u>38</u> ° <u>24</u> ' <u>6.91</u> "		
FLUSH MOUNT	DIAMETER _4.0 IN.	LENGTH _2.5 FT.		OTHER		LONG. 90° 19' 59.74"			
							LEST	LARGEST	
								1/4 1/4	
LOCKING CAP				SURFACE COMPLE	ETTION				
WEEP HOLE				STEEL X ALUMINUM PLASTIC SE			SEC. <u>LG000050</u> TWN NORTH		
				L.		RANGE		Direction	
							RING FOR:	1	
				_		RADIONU EXPLOSI		PETROLEUM PRODUCTS ONLY METALS VOC	
		_	RISER			svocs		PESTICIDES/HERBICIDESS	
ELEVATION	FT.		RISER PIPE DIAMETER2.0IN.						
			RISER PIPE LENGTH52.7FT.			PROPOSED USE OF WELL			
ANNULAR SEAL			HOLE DIAMETER6.0IN.			GAS MIGRATION WELL X OBSERVATION EXTRACTION WELL OPEN HOLE			
LENGTH37.5FT.			+	WEIGHT OR SDR#	SCH40	PIEZON		OPEN HOLE	
SLURRY CHIPS			DIRE			DIRECT			
PELLETS GRANULAR CEMENT/SLURRY				MATERIAL STEEL	(THERMOPLASTIC (PVC)	DEF	OTI I	FORMATION	
IF CEMENT/BENTOI	NITE MIX:			OTHER	THERMOTERATIO (1 VO)	FROM	TO	DESCRIPTION	
DAGO OF OFMENT	LICED.					TROW	10	DESCRIPTION	
BAGS OF CEMENT				han.		0.0		CON	
%OF BENTONITE U						1.1		STY CLY	
WATER USED/BAG:	GAL.			BENTONITE SEAL		27.8 28.6		STY CLY STY CLY	
				LENGTH:5.0		37.1		CLY SLT	
				CHIPS PELLE	TS GRANULAR	40.0		CLY SND	
				SLURRY	_	48.1		SND	
		_		SATURATED ZONE	HYDRATED	50.0	51.1	STY CLY	
SECONDARY FILTER PACK					51.1	51.3	CLY SND		
LENGTH: 0.0FT.		7 11		SCREEN		51.3		CLY SND	
				SCREEN DIAMETER	R∙ 2.0INI	53.8		SND	
				SCREEN LENGTH:		60.0		STY CLY	
DEPTH TO TOP OF	PRIMARY			DIAMETER OF DRIL		64.0 66.2		CLY SLT STY CLY	
FILTER PACK:				DEPTH TO TOP		00.2	70.0	OTT OLI	

TOTAL DEPTH: _70.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x <u>JEFFREY INGRAM</u> 006124 04/08/2016 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____14.1FT.

SCREEN MATERIAL

OTHER

X THERMOPLASTIC (PVC)

MISSOURI DEPARTMENT OF		REF NO		DATE RECEIVED			
NATURAL RESOURCES		00304708 CR NO		03/14/2016 CHECK NO.			
DIVISION OF	OKTIO	CR NO.			17008	3	
GEOLOGY AND LAND S (573) 368-2165	STATE WELL		1	REVENU	E NO.		
MONITORING WELL		A206429	03/15/2016	ADDDOVED D	031416		
CERTIFICATION RECORD		PH1 PH2		APPROVED B	Ť		ROUTE
OLKIII IOATION KLOOKD			/15/2016 03/15/2016				
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NTRACTOR OR	RDRILLING	CONTRACTOR				
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOU	IRI C/O BILL KU	TOSKY				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDEBERGH BLVD	CITY ST LOUIS			STATE MO	ZIP 63127		NUMBER
SITE NAME MERAMEC ENERGY CENTER				WELL NUMBER BMW2		COUNTY ST LOUIS CITY	
SITE ADDRESS 8200 FINE ROAD		CITY ST LOUIS					STATIC WATER LEVEL 14.11 FT
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION X ABOVE GROUND LENGTH 5.0 FT.	DIAMETER AND D SURFACE COMPL PLACED DIAMETER 12.0	LETION WAS	HOLE SURFACE CON			ON OF WEL	
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH 2.5 FT.	1	OTHER		LONG	90°	20' 20.37"
						LLEST	LARGEST
LOCKING CAP			SURFACE COMPL	ETTION		1/4	1/4 1/4
WEEP HOLE	ү —	ㅡ	STEEL X AL	LUMINUM PLASTIC	SEC. L	3000050	TWN NORTH
	1 [RANGE		Direction <u>E</u>
	- 11					RING FOR:	
					EXPLOS	3.7	
ELEVATION ET	_		RISER	TED COIN	SVOCS	L	PESTICIDES/HERBICIDESS
ELEVATIONFT.			1	TER <u>2.0</u> IN. 'H 39.7FT	PROPOS	ED USE OF	F WELL
ANNULAR SEAL		RISER PIPE LENGTH39.7FT. HOLE DIAMETER6.0IN.			GAS MIGRATION WELL X OBSERVATION		
LENGTH0.0FT.			WEIGHT OR SDR#	SCH40		CTION WELL	OPEN HOLE
SLURRY CHIPS				DIRECT			
PELLETS GRANULAR CEMENT/SLURRY	- 11		MATERIAL STEEL	X THERMOPLASTIC (PVC)	DEI)TII	FORMATION
IF CEMENT/BENTONITE MIX:			OTHER		FROM	ТО	FORMATION DESCRIPTION
BAGS OF CEMENT USED:			L U		0.0		CLY SLT
%OF BENTONITE USED:					6.9		STY CLY
WATER USED/BAG: GAL.					35.6	38.8	CLY SLT
	L		BENTONITE SEAL		38.8		STY GRVL
			LENGTH: 31.5	ETS GRANULAR	41.4	50.0	STY CLY
			SLURRY				
			SATURATED ZONE	HYDRATED			
SECONDARY FILTER PACK							
LENGTH: <u>0.7</u> FT.			SCREEN				
	<u> </u>		SCREEN DIAMETE				
			SCREEN LENGTH:				
DEPTH TO TOP OF PRIMARY			DIAMETER OF DRI				

TOTAL DEPTH: _50.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 01/25/2016 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____8.0FT.

SCREEN MATERIAL

OTHER

X THERMOPLASTIC (PVC)

APPENDIX J STATISTICAL ANALYSIS PLAN





STATISTICAL ANALYSIS PLAN

Prepared in accordance with the United States Environmental Protection Agencies Coal Combustion Rule, part 40 CFR 257.93 for Ameren Missouri's Surface Impoundment at the Meramec Energy Center, St. Louis County, Missouri



Submitted To: Ameren Missouri

1901 Chouteau Avenue St. Louis, Missouri 63103

Submitted By: Golder Associates Inc.

820 S. Main Street, Suite 100 St. Charles, MO 63301 USA

Date: October 16, 2017

Project No.153-1406





EXECUTIVE SUMMARY

This Statistical Analysis Plan (SAP) was developed to meet the requirements of United States Environmental Protection Agency (USEPA) 40 CFR Part 257 "Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities; Final Rule" (the Rule or CCR Rule). The Rule requires owners or operators of an existing Coal Combustion Residuals (CCR) Surface Impoundment to install a groundwater monitoring system and develop a sampling and analysis program (§§ 257.90 - 257.94). Ameren Missouri has determined that the Surface Impoundments at the Meramec Energy Center in St. Louis County, Missouri is subject to the requirements of the CCR Rule.

As a part of the groundwater sampling and analysis requirements of the Rule, statistical methods as described in Section §257.93(f) of the Rule need to be implemented to statistically evaluate groundwater quality. The selected statistical method must then be certified by a qualified professional engineer stating that the statistical method is appropriate for evaluating the groundwater monitoring data for the CCR Unit. Detailed descriptions of the acceptable statistical data methods are provided in the USEPA's *Statistical Analysis of Groundwater Data at RCRA Facilities, Unified Guidance* (USEPA, 2009) (Unified Guidance). The Unified Guidance is also recommended in the CCR Rule to be used for guidance in the selection of the appropriate statistical evaluation method.

This SAP details the statistical procedures to be used to establish background conditions, to implement detection monitoring, and to implement assessment monitoring (if needed) for Ameren Missouri at the above mentioned CCR Unit. Detailed information on collection, sampling techniques, preservation, etc. are provided in the Groundwater Monitoring Plan (GMP) for the CCR Unit specified above. This SAP is a companion documents to the GMP and assumes that data analyzed by the procedures described in this SAP are from samples that were collected in accordance with the GMP.

This SAP was prepared by Golder Associates, Inc. (Golder) on behalf of Ameren in order to document appropriate method of groundwater data evaluation in compliance with CCR Rules. The methods and groundwater data evaluation techniques used in this SAP are appropriate for evaluation of the groundwater monitoring data for the above mentioned CCR Unit and are in compliance with performance standards outlined in Section §257.93(g) of the CCR Rule.



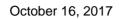


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Table 1

Physical Independence Confidence Interval Method Selection Table 2



1.0 BASELINE STATISTICS

This section discusses the procedures, methods, and processes that will be implemented as part of the Detection Monitoring statistical evaluation. Detection Monitoring will begin after eight rounds of sampling are completed at each monitoring well for each of the Appendix III and Appendix IV parameters. This background monitoring period provides baseline data for each monitoring well which can be used as the basis of the statistical evaluation. Detection monitoring will be completed on a semiannual basis unless adequate groundwater flow is not available for semiannual sampling and proper documentation as outlined in §257.94(d) is completed. Detection monitoring will analyze for Appendix III analytes as outlined in the Groundwater Monitoring Plan for this CCR Unit.

1

1.1 STATISTICAL DATA PREPARATION AND INITIAL REVIEW

Many of the statistical comparison tests used in detection, and assessment monitoring require various analyses to be completed prior to the data being used for the calculation of statistical limits. This section discusses the methods and procedures for completing this initial review of the data. The analyses required include testing for statistical independence, physical independence, and procedures to evaluate potential outliers.

1.1.1 Physical and Statistical Independence of Groundwater Samples

Detection, and Assessment Monitoring statistical evaluations assume that background and downgradient sampling results are statistically independent. The Unified Guidance states that "Physical independence of samples does not guarantee statistical independence, but it increases the likelihood of statistical independence." (Section 14.1, Unified Guidance). Physical independence is most likely achieved when consecutive groundwater samples are collected from independent volumes of water within a given aquifer zone. Using the Darcy Equation, minimum time intervals between sampling events can be calculated in order to confirm the minimum time interval for groundwater to travel through the borehole is less than the time between sampling events (**Table 1, Physical Independence**). This minimum time can be calculated as displayed in Section 14.3.2 of the Unified Guidance.



	Hydraulic	Average Hydraulic			
Well ID	, Conductivity	Gradient	Effective Porosity	Well Bore Volume	Minimum Time
Symbol	К	I	n	D	T _{min}
Units	Feet/Day	Feet/Foot	%	Feet	Days
MW-1	85.14	0.0023	0.35	0.5	0.9
MW-2	92.34	0.0023	0.35	0.5	0.8
MW-3	184.68	0.0023	0.35	0.5	0.4
MW-4	46.17	0.0023	0.35	0.5	1.6
MW-5	56.15	0.0023	0.35	0.5	1.4
MW-6	37.44	0.0023	0.35	0.5	2.0
MW-7	49.40	0.0023	0.35	0.5	1.5
MW-8	5.35	0.0023	0.35	0.5	14.2
MW-B1	2.81	0.0023	0.35	0.5	27.1
MW-B2	106.19	0.0023	0.35	0.5	0.7

Table 1: Physical Independence

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Notes:

- Average hydraulic gradient and effective porosity taken from table 2 in the Groundwater Monitoring Plan (GMP)
- 2. Hydraulic Conductivity taken from table 3 of the Groundwater Monitoring Plan (GMP)
- 3. Calculation completed using the Darcy Equation as outlined in section 14.3.2 of the Unified Guidance.

1.1.2 Data Review – Testing For Outliers

Careful review of the data is critical for verifying that there is an accurate representation of the groundwater conditions. Early identification of anomalous data (outliers) helps play a key role in a successful SAP. Possible causes for outliers include:

- Sampling error or field contamination;
- Analytical errors or laboratory contamination;
- Recording or transcription errors;
- Faulty sample preparation, preservation, or shelf-life exceedance; or
- Extreme, but accurately detected environmental conditions (e.g., spills, migration from the facility).

The following sections outline a few graphical and statistical tests that should be completed prior to the data being used to calculate statistical limits.

1.1.2.1 Time Series Plots

Time Series plots are a quick and simple method to check for possible outliers. Time series plots should be generated with the concentration of the analyte on the Y-axis and the sample date (time) on the X-axis. If any data points look to be potential outliers, the data should be flagged and further evaluated as described in Section 1.1.2.2 below.



1.1.2.2 Dixon's and Rosner's Tests

If graphical methods demonstrate that potential outliers exist, further investigation of these data points can be completed using Dixon's test for datasets with fewer than 25 samples and Rosner's test with datasets greater than 20 samples. Formal testing should only be performed if an observation seems particularly high compared to the rest of the dataset. If statistical testing is to be completed to whether an outlier exists, it should be cautioned that these outlier tests assume that the rest of the data (other than the outlier) are normally distributed. Additionally, because log-normally distributed data often contain one or more values that appear high relative to the rest, it is recommended that the outlier test be run on the transformed values instead of their original observations. This way, one can avoid classifying a high log-normal measurement as an outlier just because the test assumptions were violated. Most groundwater statistical packages can complete Dixon's and Rosner's tests and more information about Dixon's and Rosner's tests is provided in Sections 12.3 and 12.4 of the Unified Guidance. If the test designates an observation as a statistical outlier, the source of the abnormal measurement should be investigated. In general, if a data point is found to be a statistical outlier, it should not be used for statistical evaluation. However, outlier removal should be performed carefully, and typically only when a specific cause for the outlier can be identified.

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In some cases where a specific cause for an outlier cannot be identified, professional judgment can be used to determine whether the outlier significantly affects the statistical results to the extent that removal is deemed necessary. If an outlier value with much higher concentration than other background observations is not removed from background prior to statistical testing, it will tend to increase both the background sample mean and standard deviation. In turn, this may substantially raise the magnitude of the prediction limit or control limit calculated from that data set. Thus, experience shows that it is a good practice to remove obvious outliers from the database even when independent evidence of the source of the outlier does not exist. The removal of outliers tends to normalize the data and therefore produce a more robust statistical limit. Outlier removal also tends to produces a more conservative statistical limit, since the data variability is decreased, thereby decreasing the standard deviation.

1.2 Upgradient Monitoring Wells

Following the identification and removal of outliers, the upgradient data are further reviewed to determine appropriate methods for statistical evaluation to maintain adequate statistical power while minimizing the chance of false positives. The following sections describe the procedures and methods that should be used, based on the background dataset, to compare the background datasets, to calculate the data distribution, to handle non-detect (ND) data, and to select appropriate statistical evaluation methods (interwell vs intrawell).

1.2.1 Calculate for Mean and Standard Deviation

Following outlier removal, initial summary statistics including mean and standard deviation should be calculated for the background monitoring well datasets. While these summary statistics are easily



completed in many groundwater statistical software packages, it is important to account for values that have low or zero values as described below.

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1.2.1.1 Reporting of Low and Zero Values

1.2.1.1.1 Estimated Values (J Flag)

Estimated values are values that have a concentration between the method detection limit (MDL¹) and the practical quantitation limit (PQL²) for any given compound. These values are typically displayed with a J flag in laboratory report packages and are often referred to as "J-values". In most cases, The Unified Guidance recommends using the estimated value provided for statistical evaluation. Estimated values are typically used because the accuracy and power of most statistical evaluations lose power as the percentage of non-detects increases. While they are below the PQL, estimated values are considered detectable concentrations for statistical calculations, which has the effect of lowering the percentage of non-detects.

This "rule" should be applied with care, as there is an exception. Estimated values are not considered detectable concentrations if all values for a single constituent are less than the PQL. This is discussed in more detail in Section 1.3.5 of this document.

1.2.1.1.2 Non-Detects Values (ND)

Non-Detect Values (ND) are concentrations that were not detected at a concentration above the MDL. ND values are typically displayed with a "U" or "ND" flag in laboratory data report packages. The following approaches for managing ND values are based on recommendations in the Unified Guidance and are applicable for use with the statistical evaluation procedures that will be further discussed and used in this SAP (prediction intervals, confidence intervals, and tolerance intervals):

- If <15% ND, substitute ½ the PQL;
- If between 15% to 50% ND, use the Kaplan-Meier or robust regression on ordered statistics to estimate the mean and standard deviation;
- If >50% but less than 100% ND, use a non-parametric test; or
- If 100% of values are less than the PQL, use the Double Quantification Rule.

1.2.2 Data Distribution

Statistical evaluations of groundwater data require an understanding of the data distribution for each analyte in each monitoring well. Data typically fall into one of the following distributions:

² PQL = minimum concentration of an analyte (substance) that can be measured with a high degree of confidence that the analyte is present at or above that concentration (typically 5-10x higher than the MDL).



¹ MDL = lowest level of an analyte (substance) that the laboratory can reliably detect with calibrated instrumentation; generally based on results of an annual "MDL study" performed in accordance with 40 CFR Part 136, Appendix B; MDLs are generally set using laboratory grade deionized water spiked with a known concentration and thus do not account for effects of matrix interference inherent in typical groundwaters.

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- Normal distribution Sometimes referred to as Gaussian distribution, a normal distribution is a common continuous distribution where data form a symmetrical bellshaped curve around a mean. Normally distributed data are tested using parametric methods.
- Transformed-normal distribution Similar to a normal distribution, however, data are asymmetrical until transformation is applied to all data which then causes it to form a bell-curve. Transformed-normal data distributions are also tested use parametric methods.
- Non-Normal Distribution When the data are not or cannot be transformed into a symmetrical distribution. Non-normal data distributions are tested using Nonparametric methods.

Testing for data distributions can be completed in several different ways including the skewness coefficient, probability plots with Filliben's test, or the Shapiro-Wilk/Shapiro-Francia Test. All of these methods may be employed, however, the Shapiro-Wilk and Shapiro-Francia tests are generally considered the best method according to the Unified Guidance. The Shapiro-Wilk test is best for sample sizes under 50 while the Shapiro-Francia test is best with larger datasets of 50 or more observations. Most groundwater statistical software packages can complete both Shapiro-Wilk and Shapiro-Francia tests and a detailed discussion of the testing procedures is provided in Section 10.5.1 of the Unified Guidance.

Based on the outcome of the data distribution testing, data will use either Parametric or Non-parametric tests. It is important to note that non-parametric testing usually requires larger datasets in order to minimize the Site Wide False Positive Rate (SWFPR) therefore when the raw data are not normally distributed, a transformed-normal distribution is preferred when possible.

1.2.3 Temporal Trend

Most statistical tests assume that the sample data are statistically independent and identically distributed. Therefore, samples collected over a period of time should not exhibit a time dependence. A time dependence could include the presence of trends or cyclical patterns when observations are graphed on a time series plot. Trend analysis methodologies test to see whether the dataset displays an increasing, decreasing, or seasonal trend. A statistically significant increasing or decreasing trend could indicate a release from the CCR unit (or alternative source) and further investigation of the cause of the trend may be necessary.

If a trend is suspected, a Theil-Sen trend line should be used to estimate slope and the Mann-Kendall Trend Test should be used to evaluate the slope significance (Chapter 14, Unified Guidance). If a statistically significant trend is reported, based on a Sen's slope/Mann-Kendall trend test, the source of the trend should be investigated. If the trend can be shown to be a result of an upgradient or off-site source, the data can be de-trended and used to calculated statistical limits. De-trending can be accomplished by computing a linear regression on the data (see Section 17.3.1 of the Unified Guidance) and then using the regression residuals instead of the original measurements in subsequent statistical analysis.



1.2.4 Comparing Background Datasets (Spatial Variation)

After physical independence, outlier, trend, and summary statistical testing is completed, the datasets from the background monitoring wells should be compared to one another for each individual constituent. The comparison of these background datasets is useful for determining whether spatial variability exists in the background dataset, and can also be used to decide whether an interwell or intrawell approach is more appropriate for statistical evaluation.

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Box and whisker plots can be used to perform side by side comparison for each well and can be completed for each individual analyte to determine if the variance is equal across the background datasets. If the box plots appear to be staggered and do not appear to be from the same population (same variance) then a Lavene's test using an α of 0.01 should be used as a check to determine if the background datasets have spatial variation. Testing methods and procedures are provided in Section 11.2 of the Unified Guidance.

The preferred method for comparing background datasets is a Mann-Whitney (or Wilcoxon Rank Sum) Test, which evaluates the ranked medians of both the historical and new dataset populations. An α of 0.05 should be used for this evaluation. After calculation, if the Mann-Whitney statistic does not exceed the critical point, the test assumes that the two data populations have equal medians, and therefore are likely from the same statistical distribution. The testing methods and procedures for this analysis are provided in Section 16.2 of the Unified Guidance.

If spatial variability is identified within the background dataset, an additional investigation may be needed in order to confirm that the variability is not caused by impacts from the CCR unit. If there is spatial variability and it is not caused by impacts from the CCR unit, then an intrawell approach to statistical evaluation may be appropriate.

1.3 Compliance Monitoring Wells and Statistically Significant Increases

After completing the previously described analyses of the background data, a statistical evaluation of the compliance monitoring data should be completed to determine if there are any Statistically Significant Increases³ (SSIs) that could trigger assessment monitoring. Section §257.93(F) of the CCR Rule specifies the list of methods that can be used for statistical evaluation. These specific methods to be used for statistical evaluation of data from the RMSGS are detailed below. Further, the Unified Guidance is recommended in the CCR Rule to be used for guidance in the selection of the appropriate statistical evaluation method. This section provides a guide to choosing the correct statistical evaluation to analyze the compliance wells for SSIs, the basic principles of each method, and response activities for identified SSIs.

³ SSI = a verified statistical exceedance; under compliance monitoring programs, the first time an exceedance is reported it is an initial statistical exceedance and is only considered an SSI if a confirmatory result verifies the initial exceedance.



1.3.1 Interwell vs Intrawell Statistical Analysis

1.3.1.1 Interwell Statistical Analysis

An interwell statistical evaluation compares the groundwater results from the compliance (downgradient) monitoring wells to a pool of background (typically upgradient) monitoring well results. If results from the downgradient wells are statistically higher (or significant) than the background dataset then an exceedance is triggered. This upgradient verses downgradient method typically assumes that:

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- Naturally, un-impacted groundwater characteristics in the compliance monitoring wells is comparable and equal on average to the background monitoring wells.
- Upgradient and downgradient monitoring well samples are drawn from the same aquifer and are screened in essentially the same hydrostratigraphic position.
- The aquifer unit is homogeneous and isotropic.
- Groundwater flow is in a definable pathway from upgradient to downgradient wells beneath the CCR Unit.

An interwell approach is preferable for statistical evaluation because it compares data to a background dataset that is not influenced by the CCR Unit. Interwell methods should be used with two exceptions: (1) there are significant differences in the datasets of the background wells (as indicated by methods described in Section 1.2.4) or (2) it can be demonstrated that groundwater geochemistry at all wells (background and compliance) is not impacted by the CCR Unit.

1.3.1.2 Intrawell Statistical Analysis

An intrawell statistical evaluation compares the groundwater results from a compliance monitoring well to historical data collected from that same compliance monitoring well. This method can be used for CCR monitoring when groundwater data from the background monitoring wells is statistically different than that of the compliance monitoring wells or when it can be shown that there is no impact from the CCR Unit in either upgradient or downgradient/compliance wells.

1.3.2 Statistical Power

As discussed above, one of the primary goals of the selection of a proper statistical evaluation method is to limit the potential for results to falsely trigger a SSI while also maintaining sufficient statistical power to detect a true SSI. Falsely triggering a SSI when no release from the CCR unit has occurred is referred to as a false positive. The False Positive Rate (FPR), typically denoted by the Greek letter α , is also known as the "significance level". The FPR is the probability that a future compliance observation will be declared to be from a different statistical distribution than the background data. If the FPR is set too high, it can lead to the conclusion that there is evidence of impact when none exists. Conversely, if the FPR is set too low, it can lead to a false conclusion that no contamination exists, when it actually does exist (also known as a "false negative"). Ultimately, the ability to accurately identify SSIs depends on the selection of an appropriate FPR, which is referred to as the statistical power. FPRs are set for each parameter (or for each





parameter in each well for intrawell analysis). However, statistical analysis programs and the resulting decision making do not depend on each individual measurement/comparison error rates, but are dependent on the collective error rate from all of the individual comparisons. When the individual FPRs are integrated over the entire statistical monitoring program, it is referred to as the site-wide false positive rate (SWFPR), which is a better measure of the ability of the entire statistical program to detect false positive observations.

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1.3.2.1 <u>Site-Wide False Positive Rate</u>

For CCR monitoring, detection monitoring events are based on multiple comparisons, which include the seven (7) Appendix III parameters, at each compliance monitoring well. The SWFPR can be calculated based on several input parameters, including the assumed FPR, the number of downgradient monitoring wells (n), the number of parameters, and the number of statistical comparisons events in a given year for the CCR Unit. The Unified Guidance recommends that a statistical evaluation program be designed with an annual, cumulative SWFPR of approximately 10%.

The Unified Guidance recommends measuring statistical power using power curves which display the probability that an individual comparison will detect a concentration increase relative to background results. After determining the statistical method based on the background data, a power curve can be generated in order to determine the statistical power of the compliance monitoring program. The methods and procedures for calculating the SWFPR are described in Section 6.2.2 of the Unified Guidance.

1.3.2.2 Verification Sampling

Verification Sampling is an important aspect of the SAP as it improves statistical power while maintaining the SWFPR. Most statistical evaluations incorporate verification sampling mathematically into their determination of the SWFPR. Verification sampling is typically completed at a 1 of 2 pass strategy. As described above if an initial statistical exceedance is reported, then verification sampling will be performed to confirm the initial exceedance. Verification samples should be collected on a schedule that allows for physical independence of the samples. In a 1 of 2 pass strategy, if the concentration of the verification sample is less than the calculated compliance limit, then no SSI is triggered. If the initial and subsequent verification observation are above the calculated compliance limit, a SSI is triggered.

Due to the time constraints for reporting put forth in the CCR rule, it is suggested that verification sampling not be completed at the next regularly scheduled sampling event, but instead be collected prior to the next sampling event. Verification sampling within 90 days (assuming a 1 of 2 pass verification sampling strategy) will typically allow sufficient time to complete laboratory and statistical analysis in accordance with the timeframes set forth in the CCR Rules.



1.3.3 Statistical Evaluation Methods

As outlined above, the CCR rule list 5 possible methods for statistical evaluation. The different methods that can be employed for CCR monitoring as outlined in §257.93(F) are:

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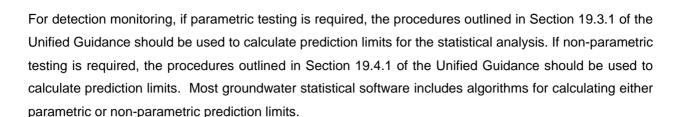
- §257.93(F)(1) "A parametric analysis of variance followed by multiple comparison procedures to identify statistically significant evidence of contamination. The method must include estimation and testing of the contrasts between each compliance well's mean and the background mean levels for each constituent."
- §257.93(F)(2) "An analysis of variance based on ranks followed by multiple comparison procedures to identify statistically significant evidence of contamination. The method must include estimation and testing of the contrasts between each compliance well's median and the background median levels for each constituent."
- §257.93(F)(3) "A tolerance or prediction interval procedure, in which an interval for each constituent is established from the distribution of the background data and the level of each constituent in each compliance well is compared to the upper tolerance or prediction limit."
- §257.93(F)(4) "A control chart approach that gives control limits for each constituent."
- **§257.93(F)(5)** "Another statistical test method that meets the performance standards of paragraph (g) of this section."

1.3.4 Prediction Intervals

Section §257.93(F)(3) outlines using prediction intervals or tolerance intervals for statistical evaluation. Based on recommendation from the Unified Guidance, prediction limits are the preferred method for calculating detection monitoring compliance limits and will be used to calculate compliance limits for the seven Appendix III constituents. In addition, the Unified Guidance suggests using prediction limits with verification sampling (Chapter 19 of the Unified Guidance), because prediction limits help to maintain low SWFPR while still providing high statistical power. Tolerance intervals, which are a backward looking procedure, should not be used for detection monitoring, but will likely be used in assessment monitoring, as further described in Section 2.0 below. If, at any point in the future, a different statistical method becomes more applicable to the site conditions, this document may be modified to include that method as recommended by the Unified Guidance.

Prediction interval methods can be used for parametric and non-parametric datasets as well as for intrawell or interwell statistical analysis. Prediction limits use background data from either background monitoring wells for interwell analysis or from historical data for intrawell analysis calculate a concentration that represents an upper limit of expected future concentrations for a particular population. In contrast to tolerance limits, prediction intervals are a forward looking, predictive analysis, which incorporate uncertainty in future measurements, and are thus the most appropriate method for detection monitoring programs. Typically, a one-sided upper prediction limit is used to evaluate detection monitoring observations. Observations must be lower than the prediction limit (or within the upper and lower prediction limits for pH) to be considered "in control". Parametric methods are generally preferred over non-parametric methods, because they result in lower SWFPRs and higher statistical power.





1.3.5 Double Quantification Rule

In situations where the entire background dataset is reported as ND or Estimated (J-flag), the Double Quantification Rule (DQR) will be used to supplement the prediction limit analyses. Generally, the Appendix III constituents occur at detectable concentrations in natural groundwater; however, if ND results are encountered for a given constituent, the DQR can be implemented. A demonstration that this statistical evaluation is as least as effective as any other test and results as described in §257.93(f)(5) can be made. The DQR is recommended by the Unified Guidance as a supplement to prediction limits because it reduces the number of non-detects used for statistical analysis and provides a lower SWFPR while maintaining statistical power.

Under the DQR, a SSI is triggered if a compliance well observation is higher than the reporting limit (RL)/PQL in either (1) both a detection monitoring sample and its verification resample, or (2) two consecutive sampling events in a program were resampling is not utilized.

1.4 Responding to SSIs

If the statistical evaluation for an Appendix III analyte triggers a SSI, the data must be evaluated to determine if the cause of the SSI is due to a release from the CCR Unit or from an alternative source. Possible alternative sources may include laboratory causes, sampling causes, statistical evaluation causes, or natural variation. If the SSI can be attributed to one of these sources and the SSI was not caused by the CCR Unit, an alternate source demonstration (ASD) can be completed. An ASD must be certified by a qualified professional engineer and completed in writing within 90 days of completing the statistical evaluation for a particular sampling event. If the SSI cannot be attributed to an alternative source and is from the CCR Unit, then Assessment Monitoring is triggered.

1.5 Updating Background Values

The Unified Guidance suggests that updating statistical limits should only be completed after a minimum of 4 to 8 new measurements are available (i.e., every 2 to 4 years of semiannual monitoring, assuming no verification sampling). The periodic update of background, during which additional data are incorporated into the background, improves statistical power and accuracy by providing a more conservative estimate of the true background population. Prior to incorporating new data into the background dataset, a test should be performed to demonstrate that the "new data" are from the same statistical population as the existing



background results. Below are three methods that can be used in determining if the "new" data should be included in the background:

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- Time Series Graphs As described in Section 1.1.2.1, time series graphs can be used as a qualitative test to assist with the determination whether a new group of data match the historical data or if there is a concentration trend that could be indicative of a release or evolving groundwater conditions.
- Box-Whisker plots can also be used to determine whether or not the datasets are similar.
- Mann-Whitney (or Wilcoxon Rank) Test Used to evaluate the ranked medians of both the historical and new dataset populations. An α of 0.05 should be used for this evaluation. After calculation, if the Mann-Whitney statistic does not exceed the critical point, the test assumes that the two data populations have equal medians, and therefore are likely similar.

Ultimately, the Mann-Whitney (Wilcoxon Rank Sum) Test is the statistical test that is used to determine whether new observations should be included in the background dataset. It is important to note that a difference in background datasets does not automatically prevent the new data from being used; however, if differences are noted, a review of the new data will be conducted to determine if the noted difference is a result of a change in the natural conditions of the groundwater or if it is the result of a potential release from the CCR Unit. If the new data are included in the background dataset, the prediction limits will be recalculated, as described in Section 1.3.4 above.





2.0 ASSESSMENT MONITORING STATISTICAL EVALUATION

This section discusses the procedures, methods, and processes that will be implemented as part of the assessment monitoring statistical evaluation, if required. Assessment monitoring will be initiated if a SSI is triggered during detection monitoring. As per the CCR Rule in Section §257.95(b), assessment monitoring must be initiated within 90 days of identifying an SSI (not the sample event which provided the data that resulted in the SSI). This 90-day period includes sampling the groundwater monitoring network for the Appendix IV constituents. Following the initial sampling event for all Appendix IV constituents, the monitoring network is then sampled again within 90 days of receiving the results from the initial Appendix IV sampling event. Following these initial assessment monitoring events, assessment monitoring is performed on a semiannual basis. During one of the two semiannual events, the full list of Appendix IV constituents must be tested. During the second assessment monitoring event of each year, only the Appendix IV constituents that are detected during the previous semiannual event are required to be Assessment monitoring is terminated if concentrations for all Appendix III and Appendix IV monitored. constituents in all compliance wells are statistically lower than background for two consecutive sampling events (§257.95(e)). The following sections discuss the procedures, methods, and processes that will be implemented as part of the assessment monitoring statistical evaluation. As discussed in Section 1.1 of this document, many of the statistical comparisons used in assessment monitoring require various analyses to be completed prior to the data being accepted into the statistical evaluation. Before using the results from assessment monitoring, the steps outlined in Sections 1.1 and 1.2 will be completed. Please refer to those sections for descriptions on the methods and techniques required to complete these analyses.

2.1 Establishing a Ground Water Protection Standard (GWPS)

Following the removal of outliers and the performance of general statistics described in Sections 1.1 and 1.2, GWPS will be developed for use in the assessment monitoring program. The GWPS is a key element to the assessment monitoring process. GWPS must be generated for each of the detected Appendix IV analytes. If interwell methods are utilized (preferred method), a site-wide GWPS will be generated for each analyte based on Appendix IV results reported for background/hydraulically upgradient wells. If intrawell methods are utilized, a well specific GWPS will be generated for each analyte.

For Appendix IV parameters that have a maximum contaminant level (MCL), as established by the United States Environmental Protection Agency, the GWPS is set equal to the MCL. For those constituents whose background concentration are greater than the MCL, the GWPS will be calculated from the background data. Finally, for those constituents that do not have an established MCL, the GWPS will be calculated. Several analytes (cobalt, lead, lithium, and molybdenum) do not have MCLs established and therefore the GWPS must be calculated based on their background concentrations.





2.1.1 Maximum Contaminant Level (MCL) Based GWPS

Many of the Appendix IV analytes have USEPA MCL levels. As specified in the CCR Rule in Section §257.95(b), the GWPS must either be the MCL, or a limit based on background data, whichever is greater. This section describes the methods to be used for statistical analysis when the MCL is to be used as the GWPS.

For Assessment Monitoring, the Unified Guidance recommends the confidence interval method to evaluate for potential exceedances, which are referred to as "statistically significant levels" (SSLs) (Chapter 21, Unified Guidance). Using confidence intervals, SSLs are identified by comparing the calculated confidence interval against the GWPS. A confidence interval statistically defines the upper and lower bounds of a specified population within a stipulated level of significance. Confidence intervals are required to be calculated based on a minimum of 4 independent observations, but a more representative confidence interval can be developed when all of the available data are utilized.

The specific type of confidence interval should be based the attributes of the data being analyzed, including: (1) the data distribution, (2) the detection frequency, and (3) potential trends in the data. Table 1 below is based on Table 4-4 from the Electric Power Research Institute's *Groundwater Monitoring Guidance for the Coal Combustion Residual Rule* (2015), which displays the criteria for selecting an appropriate confidence interval. The method and procedure for calculating the Upper Confidence Limit (UCL) and Lower Confidence Limit (LCL) is provided in the section reference from the Unified Guidance, which is listed in the last column of Table 1, below.



Table 2- Confidence Interval Method Selection

Data Distribution	Non-detect Frequency	Data Trend	Confidence Interval Method
Normal	Low	Stable	Confidence Interval Around Normal Mean (Section 21.1.1)
Transformed Normal (Log-Normal)	Low	Stable	Confidence Interval Around Lognormal Arithmetic Mean (Section 21.1.3)
Non-normal	N/A	Stable	Nonparametric Confidence Interval Around Median (Section 21.2)
Cannot Be Determined	High	Stable	Nonparametric Confidence Interval Around Median (Section 21.2)
Residuals After Subtracting Trend are Normal (with equal variance)	Low	Trend	Confidence Band Around Linear Regression (Section 21.3.1)
Residuals after Subtracting Trend are Non-Normal	Low	Trend	Confidence Band Around Theil-Sen Line (Section 21.3.2)

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In an assessment monitoring program the LCL is of prime interest. If the LCL exceeds the GWPS, there is statistical evidence that a SSL has been triggered. An initial SSL should be confirmed by verification sampling. If only the UCL exceeds the GWPS while the LCL is below the GWPS, the test is considered inconclusive and the Unified Guidance recommends that this situation be interpreted as "in compliance". If both the UCL and the LCL are below the GPWS, the data are also "in compliance" with the GWPS.

It is important to note that a slightly different set of criteria are used to determine whether assessment monitoring can be terminated. Additional discussion of the criteria used for exiting assessment monitoring and returning to detection monitoring is provided below in Section 2.2.

During Assessment Monitoring, a per test FPR (α) of 0.05 will be used as an initial error level for calculating the two-tailed confidence intervals for the compliance wells (which actually means 2.5% FPR per tail). In some cases based on recommendations from the Unified Guidance, it is appropriate to adjust the FPR of the confidence interval based on the number of data points available as well as the distribution of the data being evaluated. If deemed necessary based on recommendations from the Unified Guidance, an approach is provided in Section 22 of the Unified Guidance for determining an appropriate per test FPR based on the data characteristics.



When performing assessment monitoring statistical evaluations, it is important to evaluate the compliance data for shifts. If no shifts have occurred, then all of the available Appendix IV data for a particular constituent can be used in the statistical evaluation. If shifts are noted (typically based on qualitative evaluation of a time series plot), only the data collected after the shift should be used in the statistical evaluation.

2.1.2 Non-MCL Based GWPS

Background or historical concentration limits should be assessed using the following techniques for all Appendix IV analytes. These concentration limits should then be compared with the MCL, if available, and the higher of these two values will be used as the GWPS.

The Unified Guidance provides two acceptable approaches for establishing a non-MCL based GWPS (unless all values are ND, in which case the Double Quantification Rule as described above in Section 1.3.5 should be used). The two methods include the tolerance interval approach or the prediction interval approach.

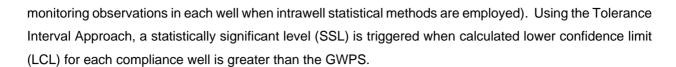
2.1.2.1 Tolerance Interval Approach

If the background dataset is normally or transformed normally distributed, the Unified Guidance recommends Tolerance Intervals over the Prediction Intervals for establishing a GWPS. The GWPS should be based on a 95 percent coverage/95 percent confidence tolerance interval. If the background data are non-normal (even after transformation), then a large number of background observations are required to calculate a non-parametric tolerance interval (typically a minimum of 60 background observations are required to meet these requirements). If there is an insufficient number of background observations to calculate a non-parametric tolerance interval, then a non-parametric Prediction Interval approach should be used, as described in Section 2.1.2.2 below.

The Upper Tolerance Limit (UTL) is calculated for each detected Appendix VI constituent. Tolerance Limits, as outlined in the Unified Guidance (Section 17.2), are a concentration limit that is designed to contain a pre-specified percentage of the dataset population. Two coefficients associated tolerance intervals are (1) the specified population proportion and (2) the statistical confidence. The coverage coefficient (γ), which is used to contain the population portion, and the tolerance coefficient (or confidence level (1- α)), which is used to set the confidence of the test. Typically, the UTL is calculated to have a coverage and confidence of 95%. When an MCL does not exist or the background concentrations are greater than the MCL, the calculated UTL for each constituent is used as the GWPS. The confidence interval for each compliance well is then compared with the GWPS.

In order to calculate a valid confidence interval, a minimum of four data points are necessary for each of the detected Appendix IV constituents in each compliance monitoring well (or four "new" assessment





Tolerance limits can be completed using both parametric (Section 17.2.1 of Unified Guidance) or non-parametric methods (Section 17.2.2 of Unified Guidance). However, as described above, the non-parametric method requires at least 60 background (or historical) measurements in order to achieve 95% confidence with 95% coverage. Tolerance Intervals can be calculated using most groundwater statistical software packages.

2.1.2.2 <u>Prediction Interval Approach</u>

If Tolerance Intervals cannot be used to calculate the GWPS (based on recommendation from the Unified Guidance, such as non-parametric datasets, ect.), then a Prediction Interval method should be used. This method is very similar to Section 1.3.4 of this document, however, for assessment monitoring, the Unified Guidance suggests using a prediction interval about a future mean for normally/transfomred-normally distributed datasets or a prediction interval about a future median for datasets with a high percent of ND or non-normally distributed data.

When using prediction intervals to calculate for a GWPS, a one-sided prediction interval is calculated using background (or historical) datasets based on a specified number of future comparisons - four future comparisons is typical. The Upper Prediction Limit that is calculated as a product of this method then becomes the GWPS, and is compared against the confidence interval for the compliance data, as described in Section 2.1.2.1, above. As also described above, if the LCL is greater than the calculated prediction limit then an SSL is triggered.

2.2 Returning to Background Detection Monitoring

As specified in 257.95(e) of the CCR Rule, in order to return to detection monitoring, the concentration of all constituents listed in Appendix III and Appendix IV must be shown to be at or below calculated "background (or historical) values" for two consecutive semiannual sampling events. This determination of background values is based on the statistical evaluation procedure established for detection monitoring. Therefore, if prediction limits (with the double quantification rule for analytes with all non-detects) are used for detection monitoring, prediction limits should be calculated and used for all Appendix III and IV analytes to determine when the monitoring program can return to Detection Monitoring. It is important to remember that Appendix IV constituents are only required to be sampled annually with only those Appendix IV constituents that are detected during the previous semiannual event being required to be analyzed during the second semiannual event of a given year. If statistical results demonstrate that concentrations for all constituents are below background levels for a particular event, all Appendix IV constituents should be sampled during the next event in order to achieve this goal of returning to Detection Monitoring. If this



statistical evaluation demonstrates that any of the Appendix III or Appendix IV are at a concentration above background levels, but no SSLs have been triggered, then the CCR unit will remain in assessment monitoring (257.95(f)).

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2.3 Response to a SSL

If the assessment monitoring statistical evaluation demonstrates that a SSL has been triggered, then the owner/operator of the CCR unit must complete the following four actions as described in 257.95(g):

- 1. Prepare a notification identifying the constituents in Appendix IV that have exceeded a CCR Unit specific GWPS. This notification must be placed in the facilities operating record within 30 days of identifying the SSL
- 2. Define the nature and extent of the release and any relevant site conditions that may affect the corrective action remedy that is ultimately selected. The characterization must be sufficient to support a complete and accurate assessment of the corrective measures necessary to effectively clean up releases from the CCR Unit and must include at least the following:
 - A. Installation of additional monitoring wells that are necessary to define the contaminant plume,
 - B. Collect data on the nature and estimated quantity of the material released,
 - C. Install and sample at least one additional monitoring well at the facility boundary in the direction of the contaminant plume migration,
- 3. Notify off-site property owners if the contamination plume has migrated offsite on to their property, and
- 4. If possible, provide an alternative source demonstration that determines that the SSL is not caused by a release at the facility within 90 days of completing the statistical evaluation. If no alternative source demonstration can be made and the plume is determined to have come from the CCR Unit then initiate corrective action.

Actions 1-3 must be completed regardless of whether or not an alternate source demonstration can be made.

2.4 **Updating Background Values**

The background for Assessment Monitoring Parameters should be updated using the same methods and techniques described in Section 1.5 for updating detection monitoring background data.





3.0 REFERENCES

- EPRI. 2015. Groundwater Monitoring Guidance for the Coal Combustion Residual Rule. Electric Power Research Institute. November.
- USEPA. 2009. Statistical Analysis of Groundwater Monitoring Data at RCRA Facilities, Unified Guidance.

 Office of Resource Conservation and Recovery Program Implementation and Information Division.

 March
- USEPA. 2015. Federal Register. Volume 80. No. 74. Friday April 17, 2015. Part II. Environmental Protection Agency. 40 CFR Parts 257 and 261. Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule/ [EPA-HQ-RCRA-2009-0640; FRL-9919-44-OSWER]. RIN-2050-AE81. April.



APPENDIX K EXAMPLE FIELD FORMS

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Project	Ref:				-		Project N	No.:		
Locati	ion									
Monitore	d By:			Date			Time			
Well P	iezom	eter Data	a							
Denth of \	Nell (from	(circle one) top of PVC or	around)					feet		
•	·	n top of PVC o	,					feet		
Radius of		·	,					inches		
								feet		
Casing Vo	olume							cubic feet		
								gallons		
Devel	opmen	t / Purgir	ng Disc	charge	e Data					
Purging M	lethod									
Start Purg	jing			Date			Time			
Stop Purg	ing			Date			Time			
Monitorin	9									
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft TOC)	Appearance of Water and Comments

Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft TOC)	Appearance of Water and Comments
	1									

GROUNDWATER SAMPLE COLLECTION FORM



Project Ref: _						Project No. :	
WEATHER CO	ONDITIONS						
Temperatur	e			_Weather			
SAMPLE INFO	ORMATION						
Sample Loc	cation				_Sample No		
	te			!			
Sample Me	thod				_ Sample Type		· · · · · · · · · · · · · · · · · · ·
	Wate	r Lev	el Before Purging	j:			
	Wate	r Lev	el Before Samplir	ng:			
	Wate	r Lev	el After Sampling	:			
	Appe	aranc	e of Sample:				
FIELD MEASU	JREMENTS						
Para	<u>meter</u> Un	its	Measurement	<u>Measurement</u>	Measurement	<u>Measurement</u>	<u>Sample</u>
	Time hhr	nm					
Volume Disc	harge ga	ıls					
	pH Stan	dard					
•	CondS			<u> </u>	<u> </u>		
	rbidity N7	īU					
Tempe							
Dissolved O Redox Po		g/i mV					
Redux 1 0	teritiai 17-	1110					
LABORATOR	Y CONTAINI	ERS					
Sub-					Type and Size of	Filtered	Type of
Sample		P	Analysis Requeste	d	Sample Container		Type of Preservative
1					Campio Comamo	(100 0.110)	
2							
3							
4							
5							
6							
7							
8							
REMARKS:							
NA = Not appli	cable						
SAMPLING MET							
	Bailer: PVC/F	PΕ.		taltic Pump	Air-Lift Pump		
	Stainle	ess St		nersible Pump	Other		

Hand Pump

Teflon

Golder	ABOVE G	ROUND MONITORING	G WELL CONST	RUCTION LOG
PROJECT NAME:		Р	ROJECT NUMBER	:
SITE NAME:		L	OCATION:	
CLIENT:		S	URFACE ELEVATION	ON:
GEOLOGIST:		NORTHING:		EASTING:
DRILLER:		STATIC WATER LEVEL:		COMPLETION DATE:
DRILLING COMPANY:		D	RILLING METHODS	S:
STICK UP:		PROTECTION OF TYPE OF SCREE SIZE OF AMOUNT	FECTIVE CASING (yes IRAVEL OR SAND HOLE ID SURFACE ELEVATION FER OF RISER PIPE (in.) FER OF BOREHOLE (in.) RETE SEAL DEPTH (ft. b) IND AMOUNT OF ANNUAL FER SAND PACK DEPTH (ft. b) FESCREEN DEPTH (ft. b) OF SCREEN: IN SLOT SIZE (in.): IN SLOT SIZE (in.): IN OF SAND:	DN:
TOTAL DEPTH OF BOREHOLE (ft. bgs):		вотто	M OF WELL DEPTH (ft. M OF FILTER PACK (ft.	bgs):
ADDITIONAL NOTES:				
CHECKED BY:				PREPARED BY:



RECORD OF WATER LEVEL READINGS

Project N	lame:			Location:				Project No).:	
Borehole No.	Date	Time	Measuring Device / Serial No.	Measurement Point (M.P)	Water Level Below M.P.	Correction To Survey Mark	Survey Mark Elevation	Water Level Elevation	Ву	Comments

Sheet ___ of ___



Project Name:			Project No:	
Calibration By:				
Instrument Details				
Instrument Name				
Serial No.				
Model No.				
Calibration Details				
Required Calibration Freque	ency/Last Ca	alibration		
Calibration Standard				
Calibration Standard(s) Exp	iration Date			
				II. d
Calibration:	Date	Time	Calibration Standard Units:	Instrument Reading Units:
				+
Comments:				

Chain of Custody Record >>> Select a Laboratory <<< #N/A #N/A #N/A Regulatory Program: DW NPDES RCRA Other: #N/A COC No: **Client Contact** Project Manager: Site Contact: Date: Tel/Fax: Carrier: COCs Your Company Name here Lab Contact: of Address **Analysis Turnaround Time** Sampler: For Lab Use Only: WORKING DAYS City/State/Zip CALENDAR DAYS Walk-in Client: Phone (xxx) xxx-xxxx TAT if different from Below FAX Lab Sampling: (xxx) xxx-xxxx 2 weeks Project Name: 1 week Site: Job / SDG No.: 2 days P O # 1 day Sample Type Sample Sample # of (C=Comp, Sample Identification Date Time G=Grab) Matrix Cont. Sample Specific Notes: Preservation Used: 1= Ice, 2= HCI; 3= H2SO4; 4=HNO3; 5=NaOH; 6= Other Possible Hazard Identification: Sample Disposal (A fee may be assessed if samples are retained longer than 1 month) Are any samples from a listed EPA Hazardous Waste? Please List any EPA Waste Codes for the sample in the Comments Section if the lab is to dispose of the sample. Unknown Poison B Return to Client Archive for___ Non-Hazard Flammable Disposal by Lab Months Special Instructions/QC Requirements & Comments: **Custody Seals Intact:** Cooler Temp. (°C): Obs'd: Corr'd: Therm ID No.: Custody Seal No .: Yes No. Relinquished by: Date/Time: Received by: Company: Company: Date/Time: Relinguished by: Date/Time: Date/Time: Received by: Company: Company:

Date/Time:

Company:

Received in Laboratory by:

Company:

Relinquished by:

Date/Time:

Golder Associates

Field Boring Log

DEPTH HOLE PROJ. NO DEPTH SOIL DRILL GA INSP DEPTH ROCK CORE WEATHER	PROJECT DRILLING METHOD DRILLING COMPANY		BORING NO OF OF
ABANDONMENT	DRILL RIG	DRILLER	DATUM
DEPTHS / / / / WATER LEVEL CAVE-IN DATE-TIME NOTE DEPTHS / / / (DELAYED) WATER LEVEL CAVE-IN DATE-TIME NOTE	SAMPLER HAMMER TYPE	_WT DROP	STARTED/_ COMPLETED/_ TIMEDATE DATE

	SAMPLE TYPES				ABBREVIATION	<u>s</u>			ORDER OF DESCRIPTION	<u>NC</u>		NON-COHES	IVE S	OILS	COHESIVE S	OILS		
C.S. * D.O. D.S. F.S. P.S.	CHUNK SAMPLE DRIVE OPEN (SPT) DENISON SAMPLE FOIL SAMPLE PITCHER SAMPLE SOIL CORE	ANG BL BR C CIN CO CL CLY	ANGULAR BLACK BROWN COARSE CAVE-IN COHESIVE CLAY CLAYEY DRY	GR HE HO LYD M MIC MOT MST NC	GRAY HETEROGENEOUS HOMOGENEOUS LAYERED MEDIUM MICACEOUS MOTTLED MOIST NON-COHESIVE	RX RND SAT SD SI SIY	RED RESIDUAL ROCK ROUNDED SATURATED SAND SILT SILTY SOME	ENERAL CONSTITUENTS	1) GROUP SYMBOL 2) SOIL GROUP NAME 3) PRIMARY COMPONENTS 4) SECONDARY COMPONENTS; 6) GOLOR 7) WEATHERING 8) STRUCTURE 9) SENSITIVITY	CL/SI: SD: S GL: S		RELATIVE DEN VERY LOOSE LOOSE COMPACT DENSE VERY DENSE	VLS LS CP DN	0-4 $4-10$ $10-30$ $30-50$	VERY SOFT SOFT	VS S FM ST	<0.25	PINGER PRESSURE EXTRUDES 5 MOLDS EASILY MOLDS THUMB INDENTS THUMBNAIL INDENTS RESISTS THUMBNAIL
*	WASH SAMPLE E SIZE	EL F FL FRAG GL	ELONGATED FINE FLAT FRAGMENTS GRAVEL	NP OG ORG	NON-PLASTIC ORANGE ORGANIC POCKET PEN. PLASTIC LIMIT	TR WL WH WR Y	TRACE WATER LEVEL WEIGHT OF HAMMER WEIGHT OF RODS YELLOW	BEHAVIOR GI	10) CONTAMINATION 11) MINEROLOGY 12) ORIGIN; 13) BEHAVIOR (CO/NC) 14) MOISTUREWATER CONTEN 15) DENSITY/CONSISTENCY	"AND"	z" 5 – 12% X "-Y" 12 – 35% 35 – 50%	MOIST FEEL	FLOW S COC	S DL	W~PL CAN	NOT ROLL	OLL 4 mm	THREAD 2 – 4 mm <2 mm

* NOTE SIZ	E GL GRAVEL PL PLA	STIC LIN) MOISTUR) DENSITY/							EE WATER W > PL C		
FLEV				SAMP			\top		STITUE			HAVI						
ELEV. DEPTH	LITHOLOGY	NO.	TYPE I	DEPTH	PT N /	BLOWS REPERSION AT	<u>c</u>	GL	SD	CL/SI	CO or NC	MOIST.	DENS.	uscs	SAMPLE	DESCRIPTION	AND	DRILLING NOTES
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