



40 CFR PART 257 GROUNDWATER MONITORING PLAN

SCPB, Sioux Energy Center

St. Charles County, Missouri, USA



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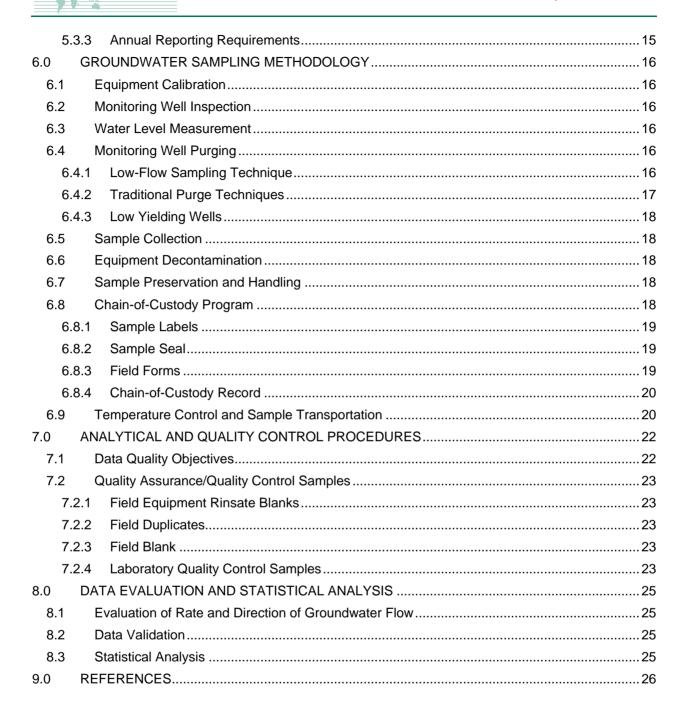
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1.0 INTRODUCTION

This Groundwater Monitoring Plan (GMP) presents information on the design of the groundwater monitoring system, groundwater sampling and analysis procedures, and groundwater statistical analysis methods for the Fly Ash Surface Impoundment (SCPB) at Ameren Missouri's (Ameren) Sioux Energy Center (Facility) in St. Charles County, Missouri (see location on **Figure 1**). The SCPB is an on-site surface impoundment and manages Coal Combustion Residuals (CCR) from the Facility. The SCPB is approximately 60 acres in size and is located to the west/southwest of the generating plant.

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This GMP was developed to meet the requirements of United States Environmental Protection Agency (USEPA) 40 CFR Part 257 "Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities; Final Rule" (the CCR Rule). The CCR Rule requires owners or operators of an existing CCR Surface Impoundment to install a groundwater monitoring system and develop a sampling and analysis program (§§ 257.90 - 257.94). Ameren Missouri has determined that the SCPB is subject to the requirements of the CCR Rule. For this GMP, the Sioux Energy Center generating plant is referred to as the SEC and the SEC and its surrounding facilities, including the Surface Impoundment, are referred to as the Facility or Site.



2.0 SITE SETTING

Ameren owns and operates the Facility in St. Charles County, Missouri located approximately 12 miles west-northwest of the confluence of the Mississippi and Missouri Rivers. **Figure 1** depicts the location of the Facility and property boundaries referenced to local topographic features. **Figure 2** depicts Facility structures relative to the site boundaries, as well as the Mississippi and Missouri rivers. The Facility encompasses approximately 1,025 acres and is located within the floodplain between the Mississippi and Missouri Rivers. The Facility is bounded to the north by wooded areas associated with the Mississippi River. The property is bounded to the south by a railroad. The Facility is bounded to the east and west by agricultural fields.

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The SCPB is located to the south of the SEC. The northern boundary of SCPB extends adjacent to the southern portion of the SEC, and is approximately 60 acres in size as shown in **Figures 1** and **2**. A generalized cross section through the Bottom Ash Surface Impoundment (SCPA) and surrounding area is shown as **Figure 3**. Directly to the west of the SCPB is the SCPA. To the south of SCPB is Highway 94 followed by the Utility Waste Landfill (UWL) and eventually the Missouri River. Northeast of SCPB lies the active coal pile and side channels from the adjacent Mississippi River. North of the SCPB is the SEC, followed by the Mississippi River. East of the CCR Unit lies higher plant facility property followed by the railroad tracks and low lying agricultural land.

2.1 Coal Combustion Residuals (CCR) SCPB Surface Impoundment

The SCPB is located in the floodplain between the Mississippi and Missouri rivers and is constructed with perimeter berms at an elevation of approximately 446 feet MSL. Fly ash has been historically managed and stored in this lined Surface Impoundment, which was constructed in 1993 with a high density polyethylene liner. The bottom of this surface impoundment ranges from approximately 422 to 431 feet above mean sea level (MSL), or approximately 19 to 28 feet below ground surface (BGS).

2.2 Geology

Much of the following information was derived from previous studies completed onsite which are described in the following paragraph. In 2005-2006, a Detailed Site Investigation (DSI) report was conducted by GREDELL Engineering Resources, Inc. (GREDELL, August 2006) in which 114 borings and piezometers were installed in order to characterize the geology and hydrogeology of the proposed UWL located just south of the SEC and the SCPB (Figure 1). Since 2008, a monitoring well network used for monitoring the UWL south of Highway 94 provides hydrogeological information from its 16 monitoring wells. In 2015 and 2016, 24 monitoring wells were installed for CCR groundwater monitoring for the different CCR Units as required by the CCR Rule. These wells provided hydrogeological and geological information about the site. Additional site specific information on the sites hydrogeology and geology is provided in EPRI, 1998.





2.2.1 Physiographic Setting and Regional Geology

The Facility is located in the extreme southeastern corner of the Central Lowland Physiographic Province and the Dissected Till Plains (DSI). However, because the Facility lies between two major river systems in an area that has been mostly deposited by flow and deposition of river deposits, the regional physiographic setting is not representative of local Site geology.

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2.2.2 Local Geology

Based on the site specific borings (Appendix A) alluvial deposits associated with the Missouri and Mississippi Rivers overlie older sedimentary bedrock. These alluvial deposits comprise the surficial alluvial aquifer, which lies unconformably on top of bedrock and is typically 100 to 120 feet thick. Overall, this aquifer is described as a fining upwards sequence of stratified sands and gravels with varying amounts of silts and clays. Drilling in the alluvial aguifer identified different sub-units, including flood basin deposits, floodplain deposits, natural levee deposits, and channel deposits along with volumetrically less important loess deposits. Grain sizes of the alluvial deposits are highly variable.

According to the DSI, bedrock below the alluvial aquifer includes Mississippian-aged rocks of the Meramecian Series. Formations include primarily limestone, dolomite, and shale and are comprised of the Salem Formation, Warsaw Formation, and the Osagean aged Burlington-Keokuk Formation.

2.3 Site Hydrogeology

Uppermost Aquifer

The CCR Rule requires that a groundwater monitoring system be completed in the uppermost aquifer around each CCR Surface Impoundment (§257.91(a)). As shown on Figure 3, the uppermost aquifer beneath all of the CCR impoundments and landfills is the alluvial deposits consisting primarily of alluvial sands with some silt, clay, and gravel associated with the Missouri and Mississippi River Valley alluvium. This alluvium overlies Mississippian-aged sedimentary bedrock formations. These alluvial deposits typically contain a fining upward sequence with some silts and clays present within the shallow zone and mostly coarse sands and gravels present at depth. The thickness of the alluvial aguifer typically ranges from approximately 100 to 120 feet BGS with base elevations of approximately 300 to 330 feet MSL.

2.3.2 Groundwater Elevations

CCR Surface Impoundment Pore-Water 2.3.2.1

The SCPB is a lined CCR Unit that typically has a ponded water level approximately 10 feet or more above the surrounding natural groundwater level. Water in the unit is not interconnected with the surrounding alluvial aquifer due to the liner system used in this surface impoundment to contain sluiced ash. To the west of the SCPB lies the SCPA, which is an unlined surface impoundment.



2.3.2.2 Alluvial Aguifer

During the DSI investigation in the area around the UWL, groundwater in the shallow alluvial aquifer had a relatively flat hydraulic gradient. Maximum groundwater elevation variation at any piezometer location was approximately three feet (3'). Over the year-long groundwater monitoring period, the maximum and minimum groundwater elevation at any well was approximately 417 feet MSL and 411 feet MSL, respectively. Groundwater potentiometric surface maps from the DSI are included in **Appendix B**.

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Golder obtained groundwater elevation measurements from March 2016 through June 2017 within the alluvial aquifer for the CCR monitoring wells. For each of the 8 background sampling events, groundwater elevations were measured at monitoring wells within a 24-hour timeframe and a potentiometric map was generated from these data (**Appendix C** and **Table 1**). Groundwater elevations throughout the alluvial aquifer ranged from approximately 414 to 424 feet MSL. However during any specific sampling event, groundwater elevations within the shallow alluvial aquifer ranged from approximately 1 to 4 feet.

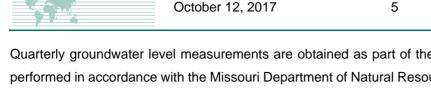
2.3.3 Groundwater Flow Directions

Site groundwater conditions are directly controlled by river stages of the Mississippi and Missouri Rivers, since the alluvial aquifer is hydraulically connected to these water bodies. River Levels display large seasonal changes in the elevations of the Mississippi and Missouri Rivers. Under normal aquifer conditions outside of the influence of the nearby SCPA Surface Impoundment, groundwater flow in the alluvial aquifer would be expected to have a flow direction component parallel to the river and a flow component from the higher of the two rivers towards the lower of the two rivers.

Although the movement of groundwater within the alluvial aquifer at the Facility is complex, the movement has been characterized by frequent groundwater elevation measurements and the generation of potentiometric surface maps generated by GREDELL and Golder (**Appendix B**, **Appendix C** and **Table 1**). The potentiometric surface maps display some variability in the groundwater flow direction. These changes in flow direction appear to be related to the water levels within the adjacent Missouri and Mississippi Rivers.

Beginning in August 2005, DSI groundwater measurements were taken every month to determine the changes in groundwater flow (**Appendix B**). During the year-long monitoring period, the direction of groundwater flow was always southward from the Mississippi River toward the Missouri River. The groundwater level is mostly controlled by the elevation of the Mississippi River with minor fluctuations in gradients caused by changes in elevation of the Missouri River. The majority of the time, the elevation of the Mississippi River to the north of the Facility was a higher water elevation than the Missouri River to the south of the Facility. The DSI reports that the Missouri River elevation exceeded the Mississippi River elevation less than 5% of the time.





Quarterly groundwater level measurements are obtained as part of the groundwater monitoring program performed in accordance with the Missouri Department of Natural Resources (MDNR) UWL permit. These data indicate similar trends in groundwater gradients and flow directions to DSI results and support the predominant flow direction towards the Missouri River. However, temporary reverse gradients and near flat gradient conditions have been rarely observed due to high water conditions in the Missouri River. According to this study, the Missouri River elevation exceeded the Mississippi River elevation 1 of the 4 sampling events (Appendix B).

Potentiometric surface maps generated as a part of the initial baseline sampling events for this GMP do not always display the same results as those completed for the UWL (Appendix C). These maps display larger variations in groundwater flow direction. Of the 8 baseline samples, the Missouri River level was higher than the Mississippi River level for 4 of the events, the Mississippi River was higher for 3 of the events, and during 1 event both rivers were at the same elevation. Additionally, localized flow directions are apparent near Poeling Lake and the Mississippi and Missouri Rivers.

Groundwater flow direction and hydraulic gradient were estimated for the CCR wells using the EPA's Online Tool for Site Assessment (USEPA, 2016). Estimated results from this analysis are provided in Table 2. These results indicate that while groundwater flow direction is variable, overall net groundwater flow during the baseline sampling period was generally towards the east but ranged from northeast to south.

2.3.3.1 **Horizontal Gradients**

Horizontal groundwater gradients in the alluvial aquifer are typically low and flat. The gradients are very dependent on river water levels (bank recharge and bank discharge conditions described earlier). Horizontal flow gradients calculated for the UWL DSI ranged from 0.0004 to 0.0013 feet/foot near the UWL. Gradients calculated as a part of the UWL sampling display similar results to the DSI, with flow gradients ranging from 0.0001 to 0.0008 feet/foot.

Site wide horizontal gradients were also calculated for each of the CCR groundwater background sampling events and the results of these are displayed on Table 2. The calculated horizontal gradients are low, ranging from 0.0001 to 0.0007 feet/foot throughout the shallow alluvial aquifer and in the compliance wells surrounding the SCPB.

A review of the potentiometric surface maps confirms the gradient estimates for a larger scale, but also demonstrates that localized horizontal gradients can be higher especially in areas near the interchange between the Mississippi River and the alluvial aquifer.



2.3.3.2 Vertical Gradients

A review of downward gradients observed in piezometers was completed by comparing groundwater elevations obtained by Golder's initial baseline sampling events. This analysis was completed between shallow and intermediate/deep zone piezometers locations where the piezometers are nested (two or more piezometers in close proximity, screened at different elevations). From the review of these data, areas away from the SCPA show relatively variable vertical gradients that fluctuate between upward and downward with no consistent vertical gradient present between shallow and deeper zones of the alluvial aquifer. Areas of the SCPB adjacent to the SCPA demonstrate a downward gradient.

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2.3.4 Hydraulic Conductivities

In-situ hydraulic conductivity tests (slug tests) were conducted as part of the DSI within the shallow portion of the alluvial aquifer to the south of the existing Surface Impoundments in the area of the UWL. The measured hydraulic conductivity in the area is highly dependent of the geology present within the screening interval of the piezometer. Estimates of the hydraulic conductivity within the aquifer were made using data acquired from slug tests from the DSI piezometers. The calculated average hydraulic conductivity of the fluvial channel sediments was 4.2 x 10⁻² centimeters per second, Natural levee deposits was 1.8 x 10⁻² cm/sec, and floodplain deposits were 7.0 x 10⁻³ cm/sec. Generally, there is a tendency toward higher hydraulic conductivity values where the screened interval intersects with relatively coarse-grained sands interpreted as channel deposits. For relatively homogenous flood plain/levee sequences containing fine-grained sediments, calculated values are demonstrably lower. Similarly, in piezometers where the screen interval intersects finer-grained, clayey backswamp/cut-off deposits, lower hydraulic conductivity values were measured.

Groundwater flow velocities were calculated as a part of the DSI using these hydraulic conductivity values, hydraulic gradients, and an estimated value for effective porosity (Figure 33 of the DSI). The DSI suggests a representative range of prevailing groundwater movement at the Site is between 14 to 188 feet per year, depending on hydraulic conductivity and effective porosity.

Golder also performed rising head hydraulic conductivity tests on the 15 newly installed CCR monitoring wells within the alluvial aquifer in order to estimate the hydraulic conductivities in February and November, 2016. The tests were conducted using a pneumatic slug (Hi-K slug) and a downhole pressure transducer. The results of Golder's hydraulic conductivity testing estimated an average hydraulic conductivity of approximately 2 x 10⁻² cm/sec for the wells screened in the shallow alluvial aquifer. Golder's findings for hydraulic conductivity values are summarized below in **Table 3** and are consistent with the conductivities calculated in the DSI.



Estimated groundwater flow velocities were calculated using the CCR monitoring well hydraulic conductivity, hydraulic gradients and an estimated value for effective porosity (**Table 2**). Using these values, flow velocities were estimated to range between 0.02 and 0.09 feet per day at the SCPB.

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Table 3: CCR Monitoring Well Hydraulic Conductivities

				Estimated Hydraulic						
	Total Depth	Well Screen Interval	Well Screen interval	Conductivity	Estimated Hydraulic					
Well ID	(feet BTOC)	(feet BTOC)	(feet MSL)	(feet/day)	Conductivity (cm/sec)					
Background	d Monitoring W	/ells								
BMW-1S	26.0	15.8 - 25.6	402.2 - 412.0	16	5.5E-03					
BMW-3S	26.7	16.5 - 26.3	400.4 - 410.2	53	1.9E-02					
SCPB Fly As	SCPB Fly Ash Surface Impoundment Monitoring Wells									
LMW-1S	42.5	32.3 - 42.1	405.0 - 414.8	31	1.1E-02					
LMW-2S	42.7	32.5 - 42.3	404.9 - 414.7	56	2.0E-02					
LMW-3S	26.2	16.0 - 25.8	404.4 - 414.2	35	1.2E-02					
LMW-4S	27.2	17.0 - 26.8	402.6 - 412.4	28	9.9E-03					
LMW-5S	47.5	37.3 - 47.1	400.3 - 410.1	56	2.0E-02					
LMW-6S	42.1	31.9 - 41.7	404.3 - 414.1	56	2.0E-02					
LMW-7S	42.2	32.0 - 41.8	402.5 - 412.3	45	1.6E-02					
LMW-8S	47.2	37.0 - 46.8	400.0 - 409.8	75	2.6E-02					
LMW-9S	41.6	31.4 - 41.2	404.4 - 414.2	22	7.9E-03					
SCL4A Utili	ty Waste Landf	ill Monitoring Wells								
UG-3*	30.0	19.8 - 30.0	399.7 - 410.0	51	1.8E-02					
TMW-1	28.9	18.7 - 28.5	399.6 - 409.4	75	2.6E-02					
TMW-2	30.4	20.2 - 30.0	398.2 - 408.0	45	1.6E-02					
TMW-3	30.1	19.9 - 29.7	398.2 - 408.0	56	2.0E-02					
SCPC Utility	y Waste Landfil	l Monitoring Wells								
UG-1A*	28.5	18.3 - 28.5	399.2 - 409.5	51	1.8E-02					
UG-2*	30.0	19.8 - 30.0	399.3 - 409.5	51	1.8E-02					
DG-1*	35.0	24.7 - 35.0	396.8 - 407.1	51	1.8E-02					
DG-2*	34.5	24.3 - 34.5	397.3 - 407.5	51	1.8E-02					
DG-3*	35.0	24.7 - 35.0	398.9 - 409.1	51	1.8E-02					
DG-4*	34.7	24.4 - 34.7	398.1 - 408.4	51	1.8E-02					

Notes

- 1. feet BTOC feet below top of casing
- 2. feet MSL feet above mean sea level.
- 3. cm/sec centimeters per second.
- 4. Rising head tests were completed by Golder Associates using a Pneumatic Hi-K Slug®.
- 5. * Hydraulic conductivity values based on results from the UWL DSI.

2.3.5 Porosity and Effective Porosity

Porosities were estimated based on the grain size distributions of an aquifer soil sample collected during monitoring well drilling. Representative grain size distribution were collected from the screen intervals at LMW-3S and LMW-8S using the ASTM D6912 Method B and the results are provided in **Appendix D**. The results show that the materials in the screen intervals of the wells are mostly comprised of sand (at least





90%) with lesser amounts of gravel, silt and clay. Also, the typical grain size of the sand ranges from fine to coarse sand. Textbook values of porosities for sands and sand/gravel mixes range from 25-50% (Fetter, 2000 and Freeze and Cherry, 1979) and fine sands typically range from 29-46%, whereas coarse sands typically range from 26-43% (Das, 2008). An average porosity of 35% is estimated for the alluvial aquifer based on the site specific grain size data.

Effective porosity is the porosity that is available for fluid flow. Studies completed in unconsolidated sediments have determined that water molecules pass through all pores and the effective porosity is approximately equal to the total porosity (Fetter, 2000). Therefore, the effective porosity of the alluvial aquifer is estimated to be 0.35.



3.0 GROUNDWATER MONITORING NETWORK

3.1 Monitoring Network Design Criteria

§257.91 of the CCR Rule sets out the requirements for development of a groundwater monitoring system for both new and existing CCR landfills and Surface Impoundments. The performance standard in the CCR Rule (§257.91(a)) states that the groundwater monitoring system must consist of a sufficient number of wells at appropriate locations to yield groundwater samples in the uppermost aquifer that accurately represent:

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- The quality of background groundwater
- The quality of groundwater passing the waste boundary of the CCR unit

3.2 Design of the Groundwater Monitoring System

The detection monitoring well network for the Facility is depicted on **Figure 2**. The network consists of 11 monitoring wells screened in the uppermost aquifer for the purpose of monitoring the SCPB Surface Impoundment. The monitoring well network includes 2 background groundwater monitoring wells (BMW-1S and BMW-3S) that are located approximately 2,500 to 3,500 feet west of the SCPB in areas unaffected by CCR disposal. Nine (9) of the groundwater monitoring wells are placed ringing the SCPB and are considered to be the compliance wells. The groundwater monitoring well locations were selected based on site-specific technical information presented in section 2.0 of this document, as well as the preferential migration pathway analysis below.

3.2.1 Preferential Migration Pathway Analysis

After detailed review of the information outlined in section 2.0 of this document, a preferential migration pathway for potential groundwater impacts coming from the SCPB was determined. The SCPB has a bottom elevation between 422-431 feet MSL. In the unlikely event of a liner failure, potential constituent migration pathways are likely to be downward then laterally in the direction of groundwater flow in the shallow alluvial aquifer. Groundwater flow within the alluvial aquifer can also be variable depending on levels within the Missouri River and can flow in a variety of directions. Groundwater monitoring wells were placed around the unit in order to capture flow in variable directions. Based on water level readings, the groundwater in the alluvial aquifer can range from approximately 414 to 424 feet MSL. In order to place monitoring well screens within the migration pathway from the unit, monitoring wells were installed with screen interval elevations that range below the seasonal low groundwater levels so that the well screen is submerged below the water table surface to allow for groundwater sampling.





3.2.2 Background/Upgradient Monitoring Well Locations

As described above, the flow of groundwater in the alluvial aquifer is generally from either the Mississippi River towards the Missouri River or from the Missouri River towards the Mississippi River. Alluvial aquifer flow is also locally influenced by water levels in the SCPA and the Mississippi and Missouri River levels. The CCR Rule (§257.91(a)(1)) requires that background groundwater samples from the uppermost aquifer;

"Accurately represent the quality of background groundwater that has not been affected by leakage from a CCR unit."

The CCR Rule also allows for sampling of background monitoring wells that are not hydraulically upgradient where hydrogeological conditions do not allow wells that are hydraulically upgradient and/or where sampling at other monitoring wells will provide an indication of background groundwater quality that is as representative as, or more representative than, that provided by upgradient monitoring wells. At this facility, groundwater flows both north and south towards the Mississippi and Missouri Rivers, complicating the location of upgradient wells. As a result, two background monitoring well locations were placed to the west of the SCPB, in side-gradient locations across from Poeling Lake.

As shown in **Figure 2**, the background monitoring wells BMW-1S and BMW-3S are west of the SCPB at a location approximately the same distance from the Mississippi River. These wells, located cross gradient to the SCPB provide background groundwater quality for SCPB monitoring.

3.2.3 Downgradient Monitoring Well Locations

Downgradient monitoring wells are located ringing the SCPB to monitor potential migration pathways. **Figure 2** shows that the downgradient well network consists of nine groundwater monitoring wells (LMW-1S, LMW-2S, LMW-3S, LMW-4S, LMW-5S, LMW-6S, LMW-7S, LMW-8S, and LMW-9S) around the SCPB at locations that are located as close to the waste boundary as practical.

3.2.1 Groundwater Monitoring Well Screen Intervals

The system of monitoring wells ringing the SCPB are screened in the shallow alluvial aquifer zone. Details on the construction of the groundwater monitoring wells are provided in **Table 4** and **Appendix E**.

Screen intervals were installed with a target elevation of 405-415 feet MSL and in sandy geological environments. Final screening intervals range from approximately 400 to 415 feet MSL.





4.0 INSTALLATION OF THE GROUNDWATER MONITORING SYSTEM

The CCR Rule Groundwater Monitoring System for the SCPB was installed in December 2015 and November 2016 as described in the following subsections.

4.1 Drilling Methods and Monitoring Well Constructions

Cascade Drilling LP installed the monitoring wells using a rotosonic drill rig (Mini Sonic CDD 1415 and Geoprobe 8040) under direct supervision of a Golder Geologist or Engineer. Continuous soil core samples were obtained at each well borehole location and were logged in the field by Golder. Soils were classified according to the Unified Soil Classification System. Boring logs and well construction diagrams are provided in **Appendix A**, and **Appendix E**, respectively.

Groundwater monitoring wells were installed in accordance with Missouri Department of Natural Resources (MDNR) Well Construction Rules (10 CSR 23-4.060 Construction Standards for Monitoring Wells). All groundwater monitoring wells were installed using 2-inch diameter PVC well riser pipe and 10-foot long, 0.010-inch machine slotted well screens. Wells were installed with a sand filter pack, bentonite seal, and annular space in accordance with MDNR Well Construction Rules. Details on the construction of the groundwater monitoring wells are provided in **Table 4** and **Appendix E**.

Monitoring wells were completed with an aluminum protective cover with a locking lid that extends approximately 2 to 3 feet above ground surface and a small concrete pad. Three yellow protective posts (concrete filled steel bollards) have been installed around each monitoring well surface completion.

4.2 Groundwater Monitoring Well Development

After well construction, a Golder geologist or engineer developed groundwater monitoring wells using surging and purging techniques. During development, field parameters (pH, conductivity, temperature, and turbidity) were recorded and development was complete once a minimum of three well-bore volumes of water were purged, turbidity was typically less than 20 nephelometric turbidity units (NTU) or \pm 10% and consecutive measurements of field parameter values were within 10 percent difference. Groundwater monitoring wells were developed using an inertial pump with a surge block ring attached to a foot valve to surge and purge the well. Well development forms are attached in **Appendix F**.

4.3 Dedicated Pump Installation

A dedicated pump was installed in each groundwater monitoring well after development and hydraulic conductivity testing. The dedicated pumps provide a consistent, repeatable sampling method to reduce likelihood of cross contamination, reduce water sample turbidity, and expedite sampling. For the purposes of this groundwater monitoring network, low-flow QED brand PVC MicroPurge bladder pumps with Dura-Flex Teflon bladders were installed in each well.



4.4 **Surveying and Well Registration**

Zahner and Associates, Inc., a Professional Land Surveyor licensed in Missouri, surveyed the location and top of casing elevation of the monitoring wells. A drawing showing the location of the groundwater monitoring wells is shown in Figure 2 and a summary of survey information is provided in Table 4. Upon completion of monitoring well installation and surveying, MDNR Well Construction Registration Forms were prepared for each well and submitted to MDNR. Copies of these forms are provided in Appendix G.

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5.0 GROUNDWATER MONITORING PROGRAM

The groundwater monitoring program for the SCPB Surface Impoundment is described in the following sections.

5.1 Baseline Sampling Events

In accordance with section 257.94(b) of the CCR Rule, before starting detection monitoring, eight baseline (or background) samples were collected for all Appendix III and Appendix IV parameters at all downgradient and upgradient/background monitoring wells prior to October 17, 2017. These samples establish initial baseline datasets that are used for the statistical evaluation of groundwater results.

5.2 Detection Monitoring

The Detection Monitoring Program is defined in the CCR Rule in section 257.94 and the following sections outline the procedures for the detection monitoring program.

5.2.1 Sampling Constituents and Monitoring Frequency

Detection monitoring should be completed at a minimum of semi-annually (approximately every 6 months) for all Appendix III constituents (**Table 5**), unless a demonstration that the need for an alternative monitoring schedule is required. **Table 6** lists the analytical methods and practical quantitation limits used for the monitoring program.

5.2.2 Data Evaluation and Response

As required in the CCR Rule, a statistical evaluation of the groundwater data must be completed within 90 days of receiving data from the laboratory. The data will be analyzed using the methods and procedures outlined in the statistical analysis plan (**Appendix H.**).

5.3 Assessment Monitoring

Assessment monitoring is outlined in section 257.95 of the CCR Rule and is initiated after a confirmed SSI has been identified and no alternate source demonstration has been completed. In accordance with the CCR Rule, a notification must be prepared and placed within the Facility operating record and on the publically available website stating that an Assessment Monitoring program has been initiated. The purpose of Assessment Monitoring is to determine whether or not groundwater concentrations are at a Statistically Significant Level (SSL) compared to Groundwater Protection Standards (GWPS). Detection Monitoring sampling continues during Assessment Monitoring.

5.3.1 Sampling Constituents and Monitoring Frequency

As outlined in section 257.95 of the CCR rule, Assessment Monitoring groundwater sampling must begin within 90 days of a confirmed SSI determination. Sampling must be completed at all monitoring wells used in the detection monitoring program, for all Appendix IV analytes (**Table 5**). Within 90 days of receiving



data from this initial Assessment Monitoring sampling event, a second sampling event must be completed analyzing the Appendix IV constituents detected in groundwater during the initial sampling event.

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Following this initial phase of the Assessment Monitoring Program, the CCR Rule requires sampling of the full list of Appendix IV constituents on an annual basis (Annual Assessment Event). During the other semiannual Assessment Sampling Event, only those Appendix IV constituents that are detected during the annual sampling event are to be analyzed and reported. Additionally, verification resampling will be performed within 90 days of receiving data from the laboratory for all detected Appendix IV constituents for each event.

5.3.2 Data Evaluation and Response

As required in the CCR Rule, a statistical evaluation of the groundwater data must be completed within 90 days of receiving data from the laboratory. The data will be analyzed using the methods and procedures outlined in the Statistical Analysis Plan (Appendix H).

A GWPS is required for each Appendix IV constituent and must be included in the annual report. The GWPS will be either the MCL or a value based on background data, whichever is higher. The generation of the GWPS is discussed in more detail in the Statistical Analysis Plan (Appendix H). Statistical analysis must be completed within 90 days of receiving data from the laboratory. The statistical analysis will determine if any constituents are SSLs greater than the GWPS.

In order to discontinue Assessment Monitoring and return to Detection Monitoring, the concentration of all Appendix III and Appendix IV constituents for all compliance wells must be at levels statistically lower than background levels for two consecutive sampling events (257.95(e)). If any constituent is present at a statistical level above background levels, but below the GWPS, then Assessment Monitoring continues.

Responding to a SSL 5.3.2.1

If the Assessment Monitoring statistical evaluations demonstrate that a SSL has been triggered, then the owner/operator of the CCR unit must complete the following four actions as described in 257.95(g):

- 1. Prepare a notification identifying the constituents in Appendix IV that have exceeded a CCR Unit specific GWPS. This notification must be placed in the facility operating record within 30 days of identifying the SSL (257.95(g)) and 257.105(h)). Additionally, within 30 days of placing the notification in the operating record, the notification must be posted to the internet site (257.107(h)).
- 2. Define the character and extent of the release and any relevant site conditions that may affect the corrective action remedy that is ultimately selected. The characterization must be sufficient to support a complete and accurate assessment of the corrective measures necessary to effectively clean up releases from the CCR Unit and must include at least the following: (No timeframe is specified in the CCR Rule for this action)





- A. Installation of additional monitoring wells that are necessary to define the contaminant plume
- B. Collect data on the nature and estimated quantity of the material released
- C. Install and sample at least one additional monitoring well at the facility boundary in the direction of the contaminant plume migration
- 3. Notify off-site property owners if the contamination plume has migrated offsite on to their property within 30 days of this determination.
- 4. If possible, provide an alternate source demonstration that determines that the SSL is not caused by a release at the facility within 90 days of completing the statistical evaluation. If no alternate source demonstration can be made and the plume is determined to have originated from the CCR Unit, then proceed to corrective action steps in the CCR Rule.
 - D. If no alternate source demonstration is made, and the CCR Unit is an unlined surface impoundment, the closure or retrofit must be initiated.

Actions 1-3 must be completed regardless of whether or not an alternate source demonstration can be made.

5.3.3 Annual Reporting Requirements

In addition to the periodical reporting listed above, an annual groundwater monitoring report will be prepared according to the requirements of 40 CFR §257.90(e). At a minimum, the annual groundwater monitoring report will contain the following information:

- The current status of the groundwater monitoring program
- A projection of key activities planned for the upcoming year
- A map showing the CCR unit and all background (or upgradient) and downgradient monitoring wells included in this monitoring plan
- A discussion of any monitoring wells that were installed or decommissioned during the preceding year or any other changes made to the groundwater monitoring system
- Analytical results from groundwater sampling
- The monitoring data obtained under §§ 257.90 through 257.98, including a summary of the number of groundwater samples that were collected for analysis for each background and downgradient well, the dates the samples were collected, and whether the sample was required by the detection monitoring or assessment monitoring programs
- A narrative discussion of any transition between monitoring programs (e.g., the date and circumstances for transitioning from detection monitoring to assessment monitoring in addition to identifying the constituent(s) detected at a statistically significant increase over background levels)
- If required, an alternate source demonstration that is certified by a professional engineer
- If required, a demonstration that an alternate sampling frequency is needed
- If assessment monitoring is required, a listing of GWPS for each Appendix IV constituent



6.0 GROUNDWATER SAMPLING METHODOLOGY

Sampling will be performed in accordance with accepted practices within the industry and with the provisions of Missouri regulations. The following sections provide details regarding procedures that will be used to collect groundwater samples. Although this section provides reference to specific forms, the use of other equivalent forms to record the necessary data is permissible.

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6.1 Equipment Calibration

Equipment used to record field water quality parameters will be calibrated each day prior to use following manufacturers' recommendations. Calibration solutions for standardization materials will be freshly prepared or from non-expired stock. In the absence of manufacturer or regulatory guidance, field equipment should be calibrated to within +/- 10 percent of the standard (or 0.1 standard units for pH meters). Equipment that fails calibration may not be used. Calibration records will be maintained. A sample field Instrument Calibration Form is included in **Appendix I**.

6.2 Monitoring Well Inspection

Prior to performing any water purging or sampling, each monitoring well will be inspected to assess its integrity. The condition of each monitoring well will be evaluated for any physical damage or other breach of integrity. The security of each monitoring well will be assessed in order to confirm that no outside source constituents have been introduced to the monitoring well.

6.3 Water Level Measurement

To meet the requirements of §257.93(c), water level measurements will be taken at all monitoring wells and prior to the start of any groundwater purging. These measurements will be taken within a 24 hour period and will be recorded on the Record of Water Level Readings form or Groundwater Sample Collection Form (included in **Appendix I**). Static water levels will be measured in each monitoring well prior to purging using an electric meter accurate to 0.01 foot. The measuring probe will be rinsed with distilled or deionized water before and after use at each well.

6.4 Monitoring Well Purging

Prior to collecting samples, each monitoring well will be purged. Purging will be accomplished using either:

- Low-flow (a.k.a., minimal drawdown, or Micropurge) techniques
- Traditional purging techniques where at least three well volumes are evacuated before samples are collected

6.4.1 Low-Flow Sampling Technique

Low-flow groundwater sampling procedures will be used for purging and sampling monitoring wells that are equipped with dedicated pumps and will sustain a pumping rate of at least 100 milliliters per minute (ml/min).





Water will be purged from these wells at low rates in order to minimize drawdown in the well during purging and sampling. Depth to water measurements and field water quality parameters (temperature, pH, turbidity, and conductivity) recorded during purging will be used as criteria to determine when purging has been completed. Sample collection will be initiated immediately after purging at each well.

During water purging, wells will be pumped at rates that minimize drawdown in the well. Purging rates in the range of 100-500 ml/min typically will be used; however, higher rates may be used if sustained by the well. Stabilization of the water column will be considered achieved when three consecutive water level measurements vary by 0.3 foot or less at a pumping rate of no less than 100 ml/min.

At a minimum, field water quality parameter measurements of temperature, pH, turbidity, and conductivity, will be measured during purging at each well. Prior to collecting the initial set of field water quality parameters, the water in the sampling pump and discharge tubing (i.e., pump system volume) remaining from the previous sampling event will be removed.

After evacuating the water in the pump system, collecting field measurements will begin. Depth to water measurements and field water quality parameter measurements will be made during purging. If a field meter equipped with a flow cell is used, an amount of water equal to the volume of the flow cell should be allowed to pass through the flow cell between individual field stabilization measurements. Stabilization will be attained and purging considered complete when three consecutive measurements of each field parameter vary within the following limits:

- ± 0.2 for pH
- ± 3% for Conductivity
- ± 10% for Temperature
- Less than 10 nephelometric turbidity units (NTU) or ± 10% for Turbidity

All data gathered during monitoring well purging will be recorded on a form, an example of which is included in **Appendix I**.

6.4.2 Traditional Purge Techniques

If low-flow sampling is not performed, wells will be purged a minimum of 3 well volumes before collecting a sample. Purging procedures will generally follow those for low-flow sampling including measurement of the field parameters listed above with two exceptions:

- Higher flow rate may be used during purging
- Purging is completed after a minimum of 3 well volumes have been removed (see below)

Even where low-flow sampling is not performed, the sampling goals are to:



- Stabilize field parameters (listed in previous section) prior to collecting samples
- Minimize drawdown in the well

When traditional purge techniques are used, field stabilization measurements will be collected at the beginning of purging and between each well volume purged. The stability criteria will be those described above for low-flow sampling.

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6.4.3 Low Yielding Wells

If a monitoring well purges dry, it will be allowed to recover up to 24 hours before samples are collected. No additional purging will be performed after initially purging the monitoring well dry. If recharge is insufficient to fill all necessary sample bottles, samplers will note this on the field form, and fill as many sample bottles as possible.

6.5 Sample Collection

Sampling should take place immediately after purging is complete. Samples will be transferred directly from field sampling equipment into containers supplied by the analytical laboratory appropriate for the constituents being monitored as listed in **Table 6**. Sample containers will be kept closed until the time each set of sample containers is filled.

6.6 Equipment Decontamination

All non-dedicated field equipment that is used for purging or sample collection shall be cleaned with a phosphate-free detergent and triple-rinsed, inside and out, with deionized or distilled water prior to use and between each monitoring well. Decontamination water shall be disposed of at an Ameren approved location. Any disposable tubing used with non-dedicated pumps should be discarded after use at each monitoring well. Clean latex gloves will be worn by sampling personnel during monitoring well purging and sample collection.

6.7 Sample Preservation and Handling

In accordance with §257.93 of the CCR Rule, groundwater samples collected as part of the monitoring program will not be filtered prior to analysis. Once groundwater samples have been collected and preserved in laboratory supplied containers, they will be packed into insulated, ice-filled coolers to be maintained at a temperature as close as possible to 4 degrees Celsius. Groundwater samples will be collected in the designated size and type of containers required for specific parameters. Sample containers will be filled in such a manner as not to lose preservatives by spilling or overfilling. Samples will be delivered to the laboratory or sent via overnight courier following chain-of-custody procedures.

6.8 Chain-of-Custody Program

The chain-of-custody (COC) program will allow for tracing sample possession and handling from the time of field collection through laboratory analysis. The COC program includes sample labels, sample seals,



field Groundwater Sample Collection Forms, and COC record. A sample Chain-of-Custody (COC) form is provided in **Appendix I**.

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Each sample will be assigned a unique sample identification number to be recorded on the sample label. The sample identification number for all samples will be designated differently based on the nature of the samples. Each sample identification number and description will be recorded on the field Groundwater Sample Collection Form and on the COC document.

6.8.1 Sample Labels

Sample labels will be sufficiently durable to remain legible when wet and will contain the following information, written with indelible ink:

- Site and sample identification number
- Monitoring well number or other location
- Date and time of collection
- Name of collector
- Parameters to be analyzed
- Preservative, if applicable

6.8.2 Sample Seal

The shipping container will be sealed to prevent the samples from being disturbed during transport to the laboratory.

6.8.3 Field Forms

All field information must be completely and accurately documented to become part of the final report for the groundwater monitoring event. Example field forms are included in **Appendix I**. The field forms will document the following information:

- Identification of the monitoring well
- Sample identification number
- Field meter calibration information
- Static water level depth
- Purge volume
- Time monitoring well was purged
- Date and time of collection
- Parameters requested for analysis
- Preservative used
- Field water quality parameter measurements



- Field observations on sampling event
- Name of collector(s)
- Weather conditions including air temperature and precipitation

6.8.4 Chain-of-Custody Record

The COC record is required for tracing sample possession from time of collection to time of receipt at the laboratory. The National Enforcement Investigations Center (NEIC) of USEPA considers a sample to be in custody under any of the following conditions:

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- It is in the individual's possession
- It is in the individual's view after being in his possession
- It was in the individual's possession and he locked it up
- It is in a designated secure area

All environmental samples will be handled under strict COC procedures beginning in the field. The field team leader will be the field sample custodian and will be responsible for ensuring that COC procedures are followed. A COC record will accompany each individual shipment. The record will contain the following information:

- Sample destination and transporter
- Sample identification numbers
- Signature of collector
- Date and time of collection
- Sample type
- Identification of monitoring well
- Number of sample containers in shipping container
- Parameters requested for analysis
- Signature of person(s) involved in the chain of possession
- Inclusive dates of possession

A copy of the completed COC form will be placed in a water resistant bag and accompany the shipment and will be returned to the shipper after the shipping container reaches its destination. The COC record will also be used as the analysis request sheet. When shipping by courier, the courier does not sign the COC record: copies of shipping forms are retained to document custody.

6.9 Temperature Control and Sample Transportation

After collection, sample preservation, and labeling, sample containers will be placed in coolers containing water-ice with the goal of reducing the groundwater samples to a temperature of approximately 4°C or less.





All samples included in the shipping container will be packed in such a manner to minimize the potential for container breakage. Samples will be either hand-delivered or shipped via commercial carrier to the certified analytical laboratory. Custody seals will be placed on the shipping containers if a third party courier is used.



7.0 ANALYTICAL AND QUALITY CONTROL PROCEDURES

7.1 Data Quality Objectives

As part of the evaluation component of the Quality Assurance (QA) program, analytical results will be evaluated for precision, accuracy, representativeness, completeness, and comparability (PARCC). These are defined as follows:

■ Precision is the agreement or reproducibility among individual measurements of the same property, usually made under the same conditions

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- Accuracy is the degree of agreement of a measurement with the true or accepted value
- Representativeness is the degree to which a measurement accurately and precisely represents a characteristic of a population, parameter, or variations at a sampling point, a process condition, or an environmental condition
- Completeness is a measure of the amount of valid data obtained from a measurement system compared with the amount that was expected to be obtained under correct normal conditions
- Comparability is an expression of the confidence with which one data set can be compared with another data set in regard to the same property

The accuracy, precision and representativeness of data will be functions of the sample origin, analytical procedures and the specific sample matrices. Quality Control (QC) practices for the evaluation of these data quality indicators include the use of accepted analytical procedures, adherence to hold time, and analysis of QC samples (e.g., blanks, replicates, spikes, calibration standards and reference standards).

Quantitative QA objectives for precision and accuracy, along with sensitivity (detection limits) are established in accordance with the specific analytical methodologies, historical data, laboratory method validation studies, and laboratory experience with similar samples. The Representativeness of the analytical data is a function of the procedures used to process the samples.

Completeness is a qualitative characteristic which is defined as the fraction of valid data obtained from a measurement system (e.g., sampling and analysis) compared to that which was planned. Completeness can be less than 100 percent due to poor sample recovery, sample damage, or disqualification of results which are outside of control limits due to laboratory error or matrix-specific interferences. Completeness is documented by including sufficient information in the laboratory reports to allow the data user to assess the quality of the results. The overall completeness goal for each task is difficult to determine prior to data acquisition. For this project, all reasonable attempts will be made to attain 90% completeness or better (laboratory).

Comparability is a qualitative characteristic which allows for comparison of analytical results with those obtained by other laboratories. This may be accomplished through the use of standard accepted methodologies, traceability of standards to the National Bureau of Standards (NBS) or USEPA sources,



use of appropriate levels of quality control, reporting results in consistent, standard units of measure, and participation in inter-laboratory studies designed to evaluate laboratory performance.

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Data quality and the standard commercial report package will be evaluated with respect to PARCC criteria using the laboratory's QA practices, use of standard analytical methods, certifications, participation in interlaboratory studies, temperature control, adherence to hold times, and COC documentation (also called Data Validation).

7.2 Quality Assurance/Quality Control Samples

This section describes the various Quality Assurance/Quality Control (QA/QC) samples that will be collected in the field and analyzed in the laboratory and the frequency at which they will be performed.

7.2.1 Field Equipment Rinsate Blanks

In cases where sampling equipment is not dedicated or disposable, an equipment rinsate blank will be collected. The equipment rinsate blanks are prepared in the field using laboratory-supplied analyte-free water. The water is poured over and through each type of sampling equipment following decontamination and submitted to the laboratory for analysis of target constituents. **One rinsate blank will be collected for every 10 samples.**

7.2.2 Field Duplicates

Field duplicates are collected by sampling the same location twice, but the field duplicate is assigned a unique sample identification number. Samplers will document which location is used for the duplicate sample. One field duplicate will be collected for every 10 samples.

7.2.3 Field Blank

Field blanks are collected in the field using laboratory-supplied analyte-free water. The water is poured directly into the supplied sample containers in the field and submitted to the laboratory for analysis of target constituents. One field blank will be collected for every 10 samples.

7.2.4 Laboratory Quality Control Samples

The laboratory will have an established QC check program using procedural (method) blanks, laboratory control spikes, matrix spikes, and duplicates. Details of the internal QC checks used by the laboratory will be found in the laboratory QAP and the published analytical methods. These QC samples will be used to determine if results may have been affected by field activities or procedures used in sample transportation or if matrix interferences are an issue. One (1) Matrix Spike (MS)/ Matrix Spike Duplicate (MSD) set (i.e. one sample plus one MS, and one MSD sample at one location) will be collected per 20 samples. MS/MSD samples will have a naming convention as follows:



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Sample: S-LMW-1SMS: S-LMW-1S-MSMSD: S-LMW-1S-MSD

8.0 DATA EVALUATION AND STATISTICAL ANALYSIS

The following sections describe the evaluation and analysis procedures that are followed upon receipt of the analytical report.

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8.1 Evaluation of Rate and Direction of Groundwater Flow

Groundwater elevations will be determined for each sampling event and will be used to develop a groundwater elevation contour map that will be submitted with reports. The direction of groundwater flow will be determined from up-and downgradient relationships as depicted on the water level map. Based on these maps, groundwater flow velocities will be estimated for each event.

8.2 Data Validation

Before the data are used for statistical analysis, they will be evaluated by examining the quality control data accompanying the data report from the laboratory. Relevant quality control data could include measures of accuracy (percent recovery), precision (relative percent difference, RPD), and sample contamination (blank determinations). Data that fail any of these checks will be flagged for further evaluation. A Data Quality Review (DQR) may be initiated with the laboratory for any anomalous data.

8.3 Statistical Analysis

Upon completion of the data validation, the data will be submitted for statistical analysis in compliance with 40 CFR §257.93. The detailed statistical analysis plan for the Facility will be included in **Appendix H**.



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TABLES

Groundwater Level Data SCPB Surface Impoundment

Sioux Energy Center, St. Charles County, MO

	Loca	tion ⁶	Top of Casing ⁷	Ground Surface ⁷		nd Event 1 '2016	Backgrour 5/9/2		Backgroun 7/5/2		Backgrour 9/14/		Backgrour 11/7/		Backgroun		Backgrour 3/8/2		Backgrour 6/5/2	
Well ID	Northing	Easting	Feet MSL ⁵	Feet MSL ⁵	DTW ³	GWE ⁴	DTW ³	GWE ⁴	DTW ³	GWE ⁴	DTW ³	GWE ⁴	DTW ³	GWE ⁴	DTW³	GWE ⁴	DTW ³	GWE⁴	DTW ³	GWE ⁴
LMW-1S	1121320.4	879427.2	447.10	445.4	27.53	419.57	28.05	419.05	28.25	418.85	28.81	418.29	28.55	418.55	28.76	418.34	29.56	417.54	23.86	423.24
LMW-2S	1120332.8	879283.7	447.16	445.2	27.81	419.35	27.92	419.24	28.21	418.95	28.90	418.26	28.83	418.33	29.62	417.54	30.28	416.88	24.00	423.16
LMW-3S	1119348.8	878856.4	430.17	428.4	11.45	418.72	10.91	419.26	11.47	418.70	12.18	417.99	12.45	417.72	13.75	416.42	14.20	415.97	7.17	423.00
LMW-4S	1119226.6	879561.5	429.40	427.3	10.68	418.72	10.21	419.19	10.77	418.63	11.45	417.95	11.69	417.71	12.93	416.47	13.46	415.94	6.24	423.16
LMW-5S	1119250.6	880348.6	447.36	445.5	28.55	418.81	28.26	419.10	28.78	418.58	29.42	417.94	29.64	417.72	30.81	416.55	31.34	416.02	24.09	423.27
LMW-6S	1119782.0	880867.8	446.00	444.1	26.98	419.02	27.10	418.90	27.51	418.49	28.12	417.88	28.14	417.86	29.01	416.99	29.63	416.37	24.89	421.11
LMW-7S	1120261.0	880650.0	444.26	442.2	25.11	419.15	25.38	418.88	25.72	418.54	26.34	417.92	26.23	418.03	26.93	417.33	27.61	416.65	21.21	423.05
LMW-8S	1121024.3	880328.8	446.80	444.8	27.60	419.20	28.08	418.72	28.30	418.50	28.92	417.88	28.64	418.16	29.05	417.75	29.80	417.00	23.86	422.94
LMW-9S	1121905.9	879849.3	445.57	443.7	26.64	418.93	27.30	418.27	27.38	418.19	28.03	417.54	27.51	418.06	27.45	418.12	28.39	417.18	24.23	421.34
BMW-1S	1121709.2	876755.6	427.77	426.0	8.48	419.29	9.31	418.46	9.62	418.15	10.25	417.52	9.77	418.00	9.98	417.79	10.82	416.95	5.30	422.47
BMW-2S ¹¹	1122772.1	880524.1	437.86	436.1	19.53	418.33	20.52	417.34	20.43	417.43	21.19	416.67	20.33	417.53	19.90	417.96	21.07	416.79	16.00	421.86
BMW-3S	1121792.9	875809.5	426.69	424.1	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	8.65	418.04	9.76	416.93	4.17	422.52
Mississippi River	1124029 ²	879444 ²	NA	NA	NA	416.60	NA	416.80	NA	417.30	NA	416.50	NA	417.80	NA	418.50	NA	416.90	NA	422.00
Missouri River	1112870 ²	878170 ²	NA	NA	NA	416.60	NA	420.30	NA	421.19	NA	418.20	NA	415.39	NA	415.39	NA	413.90	NA	422.94

Notes:

- 1.) Groundwater monitoring wells surveyed by Zahner & Associates, Inc. on January 14 and December 8, 2016.
- 2.) * Mississippi and Missouri River gauge locations are estimated.
- 3.) DTW Depth to water measured in feet below top of casing.
- 4.) GWE Groundwater elevation measured in feet above mean sea level.
- 5.) MSL Feet above mean sea level.
- 6.) Horizontal Datum: State Plane Coordinates NAD83 (2000) Missouri East Zone feet.
- 7.) Vertical Datum: NAVD88 feet.
- 8.) River Elevation for the Mississippi River is provided by Ameren
- 9.) River Elevation for the Missouri River are calculated based on nearby USGS (United States Geological Survey) river elevation gauges.
- 10.) NA Not Applicable.
- 11.) BMW-2S is used as a groundwater elevation piezometer only and is not used for CCR groundwater sampling.

Reviewed MNH

Prepared JSI

Check

JS/RJF

Generalized Hydraulic Properties of Uppermost Aquifer SCPB Surface Impoundment Sioux Energy Center, St. Charles, MO

	SCPB Compliance Wells										
	(LMW-1S, LMW-2S, LMW-3S, LMW-4S, LMW-5S, LMW-6S, LMW-7S, LMW-8S, LMW-9S)										
		Average	Estimated	Mean	Mean		Estimated				
Baseline	Baseline	Groundwater	Hydraulic	Hydraulic	Hydraulic	Estimated	Groundwater				
Sampling	Sampling	Flow Direction	Gradient	Conductivity	Conductivity	Effective	Velocity				
Event	Event Date	(Azimuth)	(Feet/Foot)	(Feet/Day)	(cm/sec)	Porosity	(Feet/Day)				
1	3/16/2016	181.6	0.0002	42.10	1.5E-02	0.35	0.02				
2	5/9/2016	38.7	0.0003	42.10	1.5E-02	0.35	0.04				
3	7/5/2016	68.8	0.0002	42.10	1.5E-02	0.35	0.02				
4	9/14/2016	72.1	0.0001	42.10	1.5E-02	0.35	0.02				
5	11/7/2016	162.6	0.0002	42.10	1.5E-02	0.35	0.03				
6	1/3/2017	180.9	0.0007	42.10	1.5E-02	0.35	0.09				
7	3/8/2017	90.0	0.0003	42.10	1.5E-02	0.35	0.04				
8	6/5/2017	62.3	0.0006	42.10	1.5E-02	0.35	0.07				

Estimated Results (USEPA Tool)					
Resultant Groundwater					
Flow Direction	109				
(Azimuth)					
Estimated Annual Net					
Groundwater	8				
Movement (Feet/Year)					

Prepared By: JSI Checked By: RJF Reviewed By: MNH

Notes:

- 1. Azimuth and Hydraulic Gradient calculated using the United States Environmental Protection Agency (USEPA) On-Line Tools for Site Assessment Calculation for Hydraulic Gradient (magnitude and direction) available at https://www3.epa.gov/ceampubl/learn2model/part-two/onsite/gradient4plus-ns.html
- 2. Hydraulic conductivity value is the geometric mean of slug test results for the SCPB monitoring wells.
- 3. An effective porosity of 0.35 was used based on grain size distributions and published values (Fetter 2000, Cohen 1953, and Johnson 1967).
- 4. Azimuth is measured clockwise in degrees from north.
- 5. cm/sec Centimeters per second.

Monitoring Well Construction Details SCPB Surface Impoundment Sioux Energy Center, St. Charles County, MO

		Location ⁴		Top of Casing Elevation	Ground Surface Elevation	Top of Screen	Bottom of Screen	Base of Well	Total Depth
Well ID	Date Installed	Northing	Easting	(FT MSL) ⁵	(FT MSL) ⁵	(FT MSL) ⁵	(FT MSL) ⁵	(FT MSL) ⁵	(FT BGS) ⁵
LMW-1S	12/15/2015	1121320.4	879427.2	447.10	445.4	414.8	405.0	404.6	40.8
LMW-2S	12/16/2015	1120332.8	879283.7	447.16	445.2	414.7	404.9	404.5	40.8
LMW-3S	12/8/2015	1119348.8	878856.4	430.17	428.4	414.2	404.4	404.0	24.4
LMW-4S	12/8/2015	1119226.6	879561.5	429.40	427.3	412.4	402.6	402.2	25.1
LMW-5S	12/14/2015	1119250.6	880348.6	447.36	445.5	410.1	400.3	399.9	45.6
LMW-6S	12/14/2015	1119782.0	880867.8	446.00	444.1	414.1	404.3	403.9	40.2
LMW-7S	12/14/2015	1120261.0	880650.0	444.26	442.2	412.3	402.5	402.1	40.2
LMW-8S	12/15/2015	1121024.3	880328.8	446.80	444.8	409.8	400.0	399.6	45.2
LMW-9S	12/18/2015	1121905.9	879849.3	445.57	443.7	414.2	404.4	404.0	39.7
BMW-1S	12/8/2015	1121709.2	876755.6	427.77	426.0	412.0	402.2	401.8	24.2
BMW-3S	11/8/2016	1121792.9	875809.5	426.69	424.1	410.2	400.4	400.0	24.2

Notes:

- 1.) All elevations and coordinates were surveyed on January 14, 2016 and December 8, 2016 by Zahner and Associates, Inc.
- 2.) FT MSL = Feet Above Mean Sea Level.
- 3.) FT BGS = Feet Below Ground Surface.
- 4.) Horizontal Datum: State Plane Coordinates NAD83 (2000) Missouri East Zone Feet.
- 5.) Vertical Datum: NAVD88 Feet.

Prepared By: JS Checked By: JSI Reviewed By: MNH

Groundwater Quality Monitoring Parameters SCPB Surface Impoundment Sioux Energy Center, St. Charles County, MO

	Monitoring Parameter	Background ²	Detection ³	Assessment ⁴
Field Parameters	Temperature, pH, Conductivity and Dissolved Oxygen	Х	Х	Х
	Boron	X	Χ	Х
	Calcium	X	Х	Х
Calcium Chloride Fluoride Sulfate pH Total Dissolved Solids (T Antimony Arsenic Barium	Chloride	Х	Х	Х
Appendix III ¹	Fluoride	Х	Х	Х
	Sulfate	Х	Х	Х
	рН	Х	Х	Х
	Total Dissolved Solids (TDS)	Х	Х	Х
	Antimony	X		Х
	Arsenic	Х		Х
	Barium	X		Х
	Beryllium	Х		Х
	Cadmium	X		Х
	Chromium	Х		Х
	Cobalt	Х		Х
Appendix IV ¹	Fluoride	Х		Х
	Lead	Х		Х
	Lithium	Х		Х
	Mercury	Х		Х
	Molybdenum	Х		Х
	Selenium	Х		Х
	Thallium	Х		Х
	Radium 226 & 228	Х		Х

Notes:

- 1.) Analyte lists match requirements for monitoring from USEPA Rule 40 CFR parts 257 and 261.
- 2.) Background will be performed through October 2017 until at least 8 samples are collected.
- 3.) Approximately 6 months will separate each semi-annual sampling event.
- 4.) If necessary, assessment monitoring will be performed in accordance with USEPA Rule.

Prepared By: JS

Checked By: MWD Reviewed By: MNH

Analytical Methods and Practical Quantitation Limits SCPB Surface Impoundment Sioux Energy Center, St. Charles County, MO

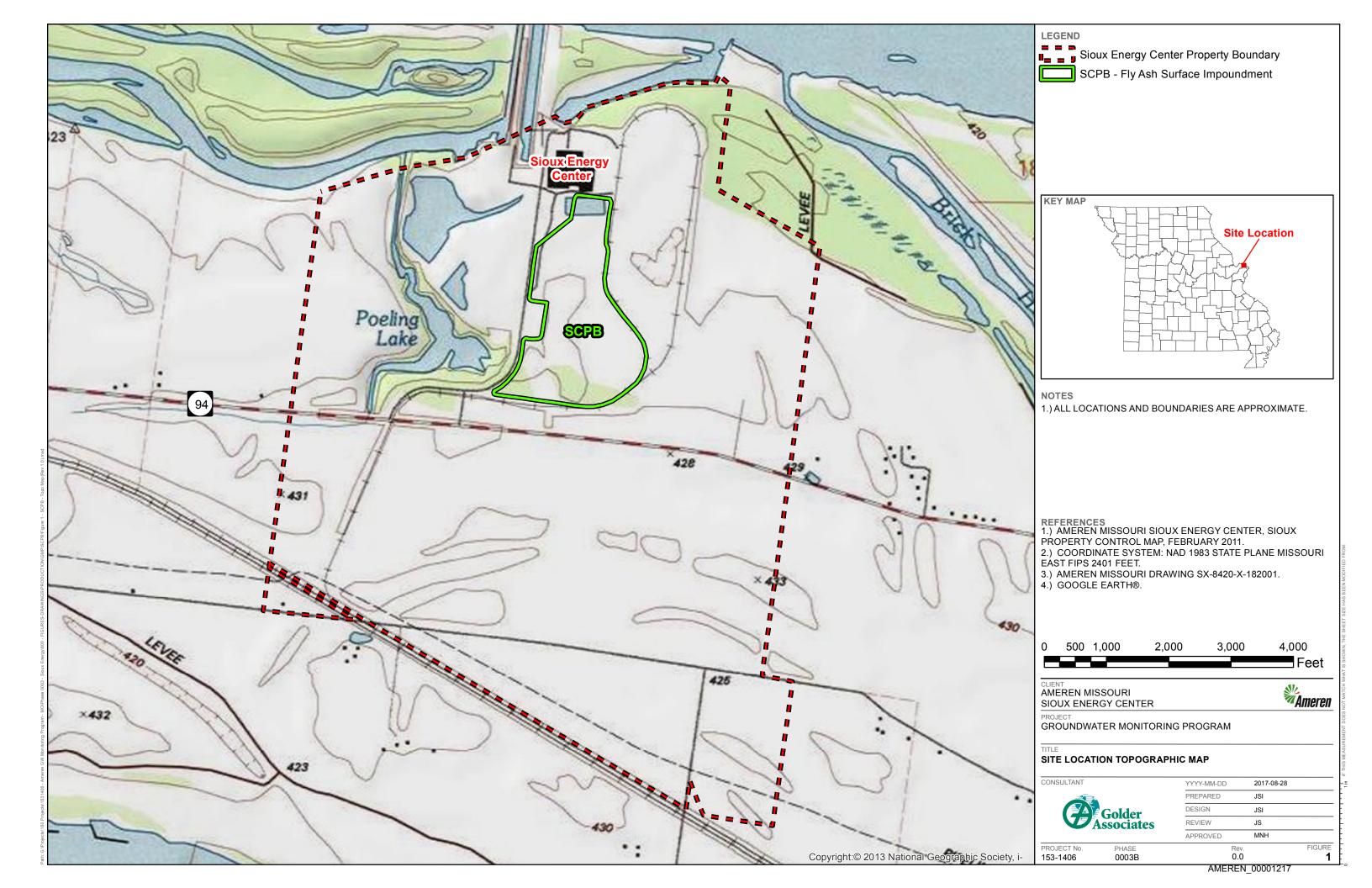
Analyte	Method Reference	Preservative	Hold Times	PQL (μg/L)	MCL (mg/L)
Appendix III - Detection Mon	itoring		_		
Boron	SW-846 6010/MCAWW 200.7	HNO3	6 months	20.0	NA
Calcium	SW-846 6010/MCAWW 200.7	HNO3	6 months	500.0	NA
Chloride	EPA 300.0/325.5/MCAWW 300/SW8463 9251/9056	NA	28 days	500.0	NA
Fluoride	EPA 300.0, 300.1	NA	28 days	-	4
рН	4500 H+B-2000	NA	NA	-	NA
Sulfate	EPA 300.0/SW8463 300	NA	28 days	2000.0	NA
Total Dissolved Solids (TDS)	2540 C-1997/SM18-20 2540 C	NA	7 days	10000.0	NA
Appendix IV - Assessment Mo	onitoring	-		•	
Antimony	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.006
Arsenic	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.01
Barium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	2.0	2
Beryllium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.004
Cadmium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	0.5	0.005
Chromium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.5	0.1
Cobalt	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	4.0	NP
Fluoride	EPA 300.0	N/A	28 days	-	4
Lead	SW-846 6020	HNO3	6 months	0.005	0.015
Lithium	SW-846 6010	HNO3	6 months	-	NA
Mercury	SW-846 7470	HNO3	28 days	-	0.002
Molybdenum	SW-846 6010	HNO3	6 months	-	NP
Selenium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.05
Thallium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	0.2	0.002
Radium 226 & 228	SW-846 903.1/SM 6500 904	-	-	1.0 (pCi/L)	5.0 (pCi/L)

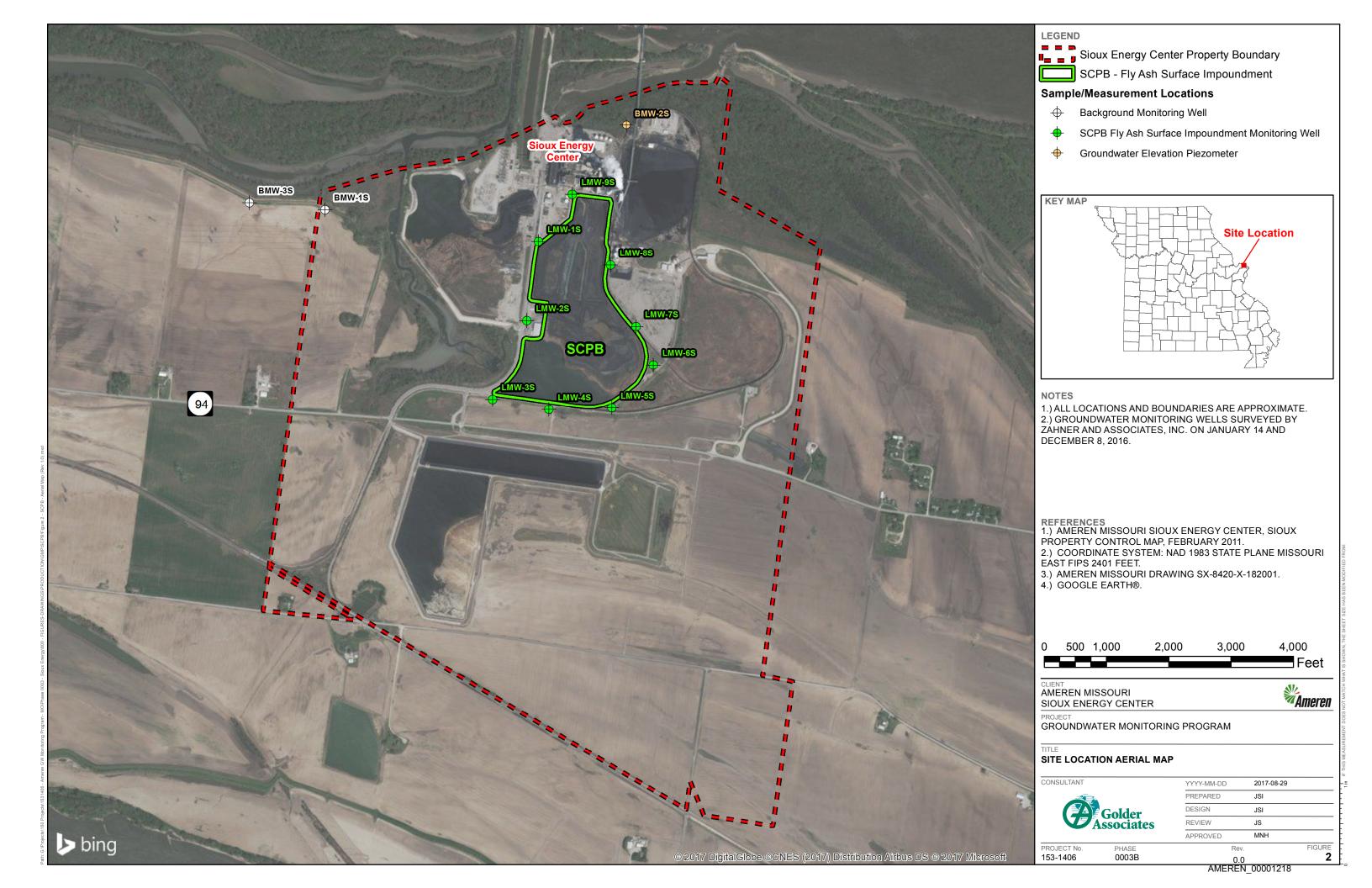
Notes:

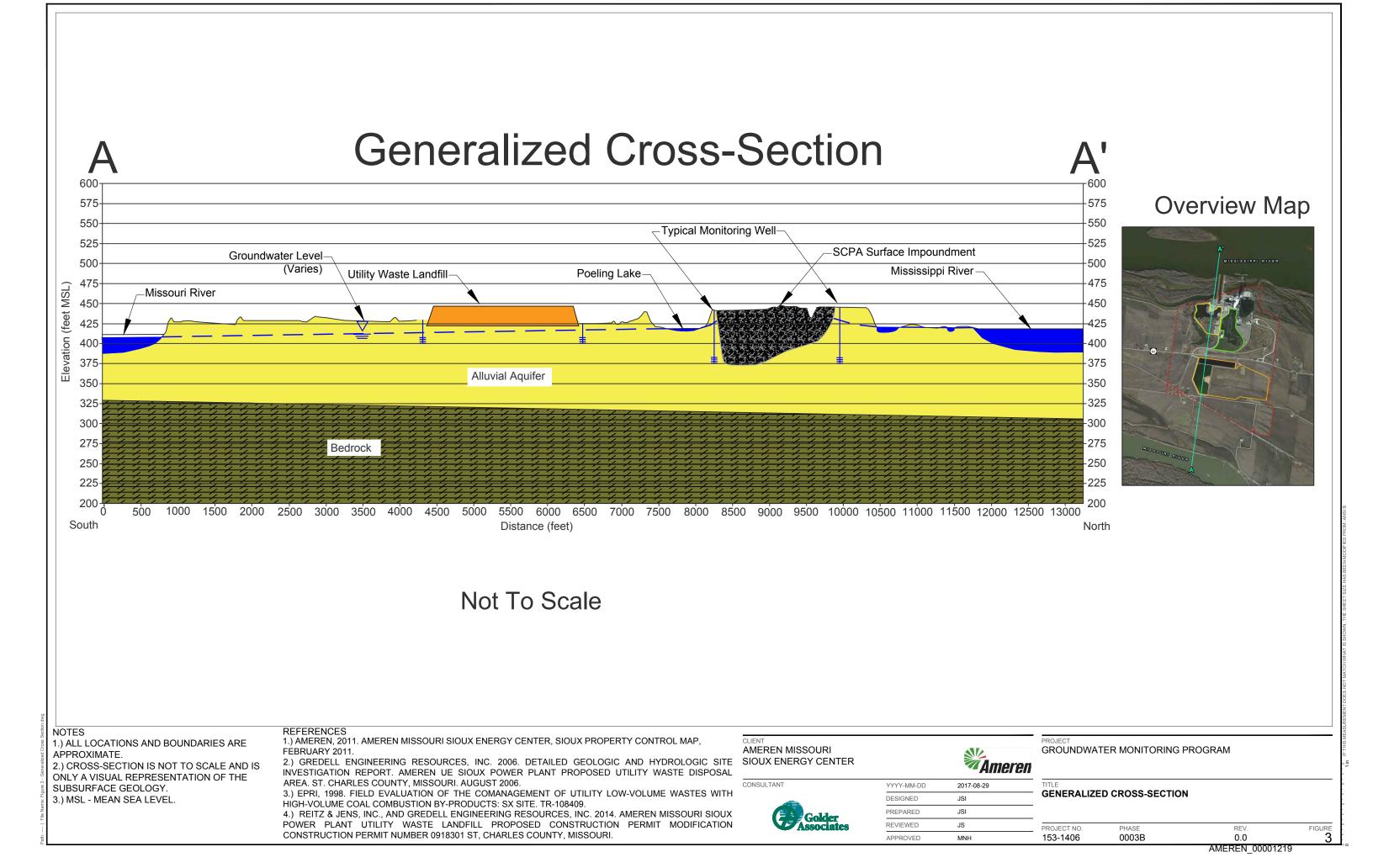
- 1.) NA not applicable.
- 2.) Analyte lists matches requirements for detection and assessment monitoring from United States Environmental Protection Agency (USEPA) Rule 40 CFR parts 257 and 261.
- 3.) SW-846 3rd denotes Test Methods for Evaluating Solid Waste, Physical- Chemical Methods, EPA publication SW-846, 3rd edition, and subsequent updates.
- 4.) MCAWW denotes Methods for the Chemical Analysis of Water and Wastes (MCAWW), United States Environmental Protection Agency (USEPA) published in the 1983.
- 5.) EPA 300 denotes Methods for the Determination of Organic Compounds in Drinking Water Environmental Monitoring Systems Laboratory, Office of Research and Development, USEPA, Cincinnati, Ohio 45268. EPA-300/4-88/039, December 1988 (Revised July 1991).
- 6.) SM18-20 denotes Standard Methods for the Examination of Water and Wastewater, 18th, 19th, and 20th Editions, published by the American Public Health Association, Water Environment Federation, and the American Water Works Association.
- 7.) Other industry-used or agency-approved methods may be used provided that they produce the necessary level of precision and accuracy for data use and reporting.
- 8.) Updates to the methods listed here are approved for use.
- 9.) PQL Practical Quantitation Limit.
- 10.) MCL Maximum Contaminant Level from USEPA 2014 Edition of the Drinking Water Standards and Health Advisories. October 2014. http://water.epa.gov/drink/contaminants/index.cfm.
- 11.) Dash (-) Indicates no information available.
- 12.) μg/L Micrograms per liter.
- 13.) pCi/L Picocuries per liter.
- 14.) NP Not Promulgated.
- 15.) mg/L Milligrams per liter.

Prepared By: JS Checked By: MWD Reviewed By: MNH

FIGURES







APPENDIX A CCR MONITORING WELL BORING LOGS

RECORD OF BOREHOLE LMW-1S SHEET 1 of 2 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 445.39 DRILLING METHOD: 0 Sonic
DRILLING DATE: 12/15/2015
DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 LOCATION: Sioux Energy Center COORDINATES: N: 1,121,320.36 E: 879,427.16 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-1.5) FILL - (GW) GRAVEL, fine to coarse sub-angular gravel, some fine sand, trace non-plastic GW fines; pale yellowish brown (10YR 6/2); non-cohesive, 443.9 1.5 (1.5-12.0) CCR - (ML) sandy SILT, non-plastic fines, fine sand, trace sub-angular gravel; dusky yellowish brown (10YR 2/2), FLY ASH; non-cohesive, dry, compact 3.7 5.0 1 SO 440.4 - 5 (5.0) SAA (Same As Above) except, some sub-angular MI 10 (12.0-15.0) (ML) sandy CLAYEY SILT, low plasticity fines, fine sand; dark yellowish brown (10YR 4/2); cohesive, w<PL, firm SO 3 ML Sonic 430.4 15.0 - 15 (15.0-41.0) (SP) SAND, fine sand, trace non-plastic fines pockets; moderate yellowish brown (10YR 5/4); non-cohesive, moist, compact 6 SO 10/9/17 - 20 GLDR_CO.GDT 423.1 (22.3) SAA except, some low to medium plasticity fines SP 5 SO SEC LOGS.GPJ ft bgs 2/16/2016 - 25 25.0 (25.0) SAA except, no fines RECORD OF BOREHOLE MWD 5.0 5.0 SO 6 415.4 Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE LMW-1S SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 12/15/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOCATION: Sioux Energy Center DATUM: NAVD88 ELEVATION: 445.39 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,121,320.36 E: 879,427.16 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER USCS TYPE DEPTH (ft) - 30 (15.0-41.0) (SP) SAND, fine sand, trace non-plastic fines pockets; moderate yellowish brown (10YR 5/4); non-cohesive, moist, compact (Continued) (30.0) SAA except, wet 30.0 Run #7, Driller pushes sampler down for 11.0 foot run. - 35 Sonic 9.8 11.0 SP 7 SO .9 40 END OF BORING AT 41.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG LMW-1S. - 45 GOLDER STL RECORD OF BOREHOLE MWD SEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 50 - 55 LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE LMW-2S SHEET 1 of 2 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 445.24 DRILLING METHOD: 0 Some DRILLING DATE: 12/16/2015 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,120,332.80 E: 879,283.70 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 0 (0.0-1.0) CCR - (GW) GRAVEL, fine to coarse sub-angular gravel, trace fine sand, trace non-plastic fines; yellowish gray (5Y 7/2), ASH; non-cohesive, dry, (1.0-6.2) CCR - (ML) sandy SILT, non-plastic fines, fine sand, trace sub-angular gravel; dark yellowish brown (10YR 4/2), ASH; non-cohesive, dry, loose 2.8 5.0 1 SO ML - 5 439.0 6.2 (6.2-10.0) (ML) CLAYEY SILT, low plasticity fines, trace fine sand; dusky yellowish brown (10YR 4/2); cohesive, ML 10 (10.0-25.0) (SM) SILTY SAND, fine sand, non-plastic fines; medium dark gray (N4); non-cohesive, moist, SO 3 Sonic 430.2 - 15 (15.0) SAA (Same As Above) except, dark yellowish 6 brown (10YR 4/2) SM 4 SO 10/9/17 - 20 SEC LOGS.GPJ GLDR_CO.GDT 5 SO ft bgs 2/16/2016 - 25 (25.0-30.0) (SP) SAND, fine sand, trace non-plastic fines; dark yellowish brown (10YR 4/2); non-cohesive, moist, compact RECORD OF BOREHOLE MWD 5.0 5.0 SP SO 6 415.2 Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE LMW-2S SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 12/16/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOCATION: Sioux Energy Center DATUM: NAVD88 ELEVATION: 445.24 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,120,332.80 E: 879,283.70 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER USCS TYPE DEPTH (ft) - 30 (30.0-41.0) (SW) SAND, fine to coarse sub-rounded sand; moderate yellowish brown 910YR 5/4); non-cohesive, wet, compact 30.0 Run #7, Driller pushes sampler down for 11.0 foot run. - 35 Sonic 10.0 11.0 SW 7 SO .9 40 END OF BORING AT 41.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG LMW-2S. - 45 GOLDER STL RECORD OF BOREHOLE MWD SEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 50 - 55 LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE LMW-3S SHEET 1 of 1 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 428.36 DRILLING DATE: 12/8/2015 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,119,348.78 E: 878,856.39 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 0 (0.0-10.0) (CL) SILTY CLAY, medium plasticity, some fine sand, some organics (roots); brownish gray (5YR 4/1); cohesive, w~PL, firm 2.8 5.0 1 SO 423.4 5.0 - 5 CL (5.0) SAA (Same As Above) except, low plasticity fines, 421.4 7.0 (7.0) SAA except, medium plasticity fines 4.1 5.0 418.4 10.0 10 (10.0-10.9) (ML) sandy SILT, non-plastic fines, fine sand; brownish gray (5YR 4/1) to light olive gray (5Y 5/2); non-cohiesvie, wet, compact MI 417.5 10.9 (10.9-22.0) (SP) SAND, fine sand, trace non-plastic fines; moderate yellowish brown (10YR 5/4); Sonic non-cohesive, wet, compact SO 3 6 - 15 SP SO - 20 GLDR_CO.GDT 406.4 22.0 (22.0-25.0) (SW) SAND, fine to coarse well graded sub-rounded sand, trace fine sub-rounded gravel; moderate yellowish brown (10YR 4/2) to dark yellowish orange (10YR 6/6); non-cohesive, wet, compact 5 SO SW - 25 END OF BORING AT 25.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION RECORD OF BOREHOLE MWD LOGGED: JSI/JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

10/9/17

SEC LOGS.GPJ

GOLDER STL

RECORD OF BOREHOLE LMW-4S SHEET 1 of 1 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 427.27 DRILLING DATE: 12/8/2015 DRILL RIG: Mini Sonic (CDD1415) INCLINATION: -90 AZIMUTH: N/A LOCATION: Sioux Energy Center COORDINATES: N: 1,119,226.63 E: 879,561.45 SAMPLES SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS BORING NUMBER DESCRIPTION USCS TYPE DEPTH - 0 (0.0-4.5) (CL) SILTY CLAY, medium plasticity fines, some fine sand, trace organics (roots); brownish gray (5YR 4/1); cohesive, w~PL, firm CL 2.0 5.0 1 SO 422.8 4.5 (4.5-7.5) (SM) SILTY SAND, fine sand, non-plastic fines; light brownish gray (5YR 6/1); non-cohesive, moist, - 5 Run #2, Sample appears to be compacted while being extruded into sample bags. Measured field recovery: 2.0/5.0. Estimated actual recovery: 3.5/5.0. SM Water Level 7.14 ft
 bgs 2/16/2016 SO (7.5-11.4) (SP-SM) SAND, fine sand, some non-plastic fines; moderate yellowish brown (10YR 5/4); non-cohiesve, moist, compact SP-SM 10 (10.0) SAA (Same As Above), wet 10.0 (11.4-15.6) (SM) SILTY SAND, fine sand, non-plastic to very low plasticity fines; moderate yellowish brown Sonic (10YR 5/4); non-cohesive, wet, compact SO 3 SM - 15 (15.6-21.7) (SP-SM) SAND, fine sand, non-plastic fines; moderate yellowish brown (10YR 5/4) to light olive gray (5Y 5/2); non-cohesive, wet, compact 4.7 5.0 4 SO SP-SM 10/9/17 - 20 GLDR_CO.GDT (21.7-25.1) (SW) SAND, fine to coarse sub-rounded sand; pale yellowish brown (10YR 6/2) to dark yellowish orange (10YR 6/6); non-cohesive, wet, compact SO 5 SW SEC LOGS.GPJ - 25 END OF BORING AT 25.1 FEET BELOW GROUND SURFACE. FOR WELL DETAILS, SEE WELL CONSTRUCTION BOREHOLE MWD LOG LMW-4S. RECORD OF GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JSI/JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE LMW-5S SHEET 1 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 12/14/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DATUM: NAVD88 ELEVATION: 445.54 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,119,250.56 E: 880,348.58 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 0 (0.0-5.0) (ML) sandy SILT, non-plastic fines, fine sand; grayish brown (5YR 3/2) to moderate brown (5YR 4/4); non-cohesive, dry, loose ML SO 442.3 (3.2) SAA (Same As Above) except, compact - 5 (5.0-20.0) (ML) SILT, non-plastic fines, some fine sand; dark gray (N3); non-cohesive, dry, compact 10 433.5 12.0 (12.0) SAA except, low plasticity fines 3 SO ML Sonic 430.5 - 15 (15.0) SAA except, trace sub-angular gravel; dark 6 yellowish brown (10YR 4/2) 4 SO - 20 (20.0-30.0) (CL) SILTY CLAY, medium plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2); cohesive, w~PL, stiff SEC LOGS.GPJ GLDR_CO.GDT <u>5.7</u> 10.0 SO - 25 CL 5 GOLDER STL RECORD OF BOREHOLE MWD 415.5 Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder

REVIEWED: PJJ/MNH

10/9/17

DRILLER: J. Drabek

Associates

RECORD OF BOREHOLE LMW-5S SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 12/14/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DATUM: NAVD88 ELEVATION: 445.54 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,119,250.56 E: 880,348.58 SOIL/ROCK PROFILE SAMPLES **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 30 (30.0-35.8) (ML) sandy SILT, low plasticity fines, fine sand; moderate yellowish brown (10YR 5/4); cohesive, 30.0 ML 10.0 10.0 - 35 6 SO (35.8-38.0) (CL) SILTY CLAY, low to medium plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2); cohesive, w~PL, firm CL 6" Sonic (38.0-45.6) (SP) SAND, fine to medium sand, trace non-plastic fines; dark yellowish orange (10YR 6/6) to dark yellowish brown (10YR 4/2); non-cohesive, moist, 405.5 40 (40.0) SAA except, wet 40.0 SP 4.2 5.6 7 SO - 45 END OF BORING AT 45.6 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG LMW-5S. 10/9/17 - 50 SEC LOGS.GPJ GLDR_CO.GDT - 55 GOLDER STL RECORD OF BOREHOLE MWD LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE LMW-6S SHEET 1 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 12/14/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DATUM: NAVD88 ELEVATION: 444.10 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,119,782.02 E: 880,867.84 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 0 (0.0-12.7) (ML) SILT, non-plastic fines, some fine sand, some sub-angular gravel; dusky yellowish brown (10YR 2/2); non-cohesive, dry, loose 1 SO 439.1 5.0 - 5 (5.0) SAA (Same As Above) except, compact ML - 10 SO 431.4 12.7 (12.7-14.0) (ML) sandy SILT, non-plastic fines, fine sand; olive gray (5Y 4/1); non-cohesive, dry, compact MI 430.1 14.0 (14.0-20.0) (ML) SILT, non-plastic to low plasticity fines, trace fine sand; brownish black (5YR 2/1); cohesive, Sonic 429.1 w<PL, stiff (15.0) SAA except, some fine sand; moderate yellowish brown (10YR 5/4) - 15 6 ML 4 SO - 20 (20.0-30.0) (SP) SAND, fine sand, trace non-plastic fines; moderate yellowish brown (10YR 5/4); non-cohesive, moist, compact SEC LOGS.GPJ GLDR_CO.GDT SP SO - 25 5 GOLDER STL RECORD OF BOREHOLE MWD 414.1 Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JS

CHECKED: JSI

REVIEWED: PJJ/MNH

10/9/17

DRILLING CONTRACTOR: Cascade

DRILLER: J. Drabek

Golder

Associates

RECORD OF BOREHOLE LMW-6S SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 12/14/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DATUM: NAVD88 ELEVATION: 444.10 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,119,782.02 E: 880,867.84 SAMPLES SOIL/ROCK PROFILE BORING METHOD DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER USCS TYPE DEPTH (ft) - 30 (30.0-40.2) (SW) SAND, fine to coarse sub-rounded sand, some non-plastic fines; moderate yellowish brown (10YR 5/4); non-cohesive, wet, compact 30.0 - 35 7.0 10.2 SW 6 SO 40 403.9 40.2 END OF BORING AT 40.2 FEET BELOW GROUND SURFACE. FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG LMW-6S. - 45 GOLDER STL RECORD OF BOREHOLE MWD SEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 50 - 55 LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE LMW-7S SHEET 1 of 2 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 442.24 DRILLING METHOD: 0 Sonic
DRILLING DATE: 12/14/2015
DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 LOCATION: Sioux Energy Center COORDINATES: N: 1,120,261.02 E: 880,649.98 SAMPLES SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 0 (0.0-1.0) FILL - (GP) GRAVEL, sub-angular to sub-rounded gravel, some fine to coarse sand; yellowish gray (5Y 7/2); non-cohesive, dry, loose °0° GP (1.0-5.0) (ML) SILT, low plasticity fines, some fine sand; dark yellowish brown (10YR 4/2); cohesive, w<PL, firm 1 SO ML - 5 (5.0-6.0) CCR - (SW) SAND, fine to coarse sand, some sub-angular gravel, some non-plastic fines; grayish black (N2), ASH; non-cohesive, moist, loose SW (6.0-10.0) CCR- (ML) SILT, low plasticity fines, some fine sand; dark yellowish brown (10YR 4/2), ASH; cohesive, w<PL, firm ML 10 (10.0-12.5) FILL- (GW) GRAVEL, sub-angular to sub-rounded gravel, some fine to coarse sand, some low plasticity fines; dark yellowish brown (10YR 4/2); non-cohesive, moist, compact GW 429.7 12.5 5.0 5.0 SO (12.5-40.2) (SP) SAND, fine sand, some non-plastic fines; moderate yellowish brown (10YR 5/4); 3 non-cohesive, moist, compact Sonic - 15 6 SO 422.2 10/9/17 - 20 (20.0) SAA (Same As Above) except, no fines GLDR_CO.GDT SP Water Level 21.74 ft bgs 2/16/2016 5 SO SEC LOGS.GPJ - 25 RECORD OF BOREHOLE MWD 5.0 5.0 SO 6 412.2 Log continued on next page GOLDER STL LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE LMW-7S SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 12/14/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DATUM: NAVD88 ELEVATION: 442.24 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,120,261.02 E: 880,649.98 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER USCS TYPE DEPTH (ft) - 30 (12.5-40.2) (SP) SAND, fine sand, some non-plastic fines; moderate yellowish brown (10YR 5/4); non-cohesive, moist, compact *(Continued)* (30.0) SAA except, wet 30.0 Run #7, Poor recovery during run. Driller notes sample may have washed out. - 35 3.0 10.2 SP 7 SO 40 402.0 40.2 END OF BORING AT 40.2 FEET BELOW GROUND SURFACE. FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG LMW-7S. - 45 GOLDER STL RECORD OF BOREHOLE MWD SEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 50 - 55 LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE LMW-8S SHEET 1 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 12/15/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DATUM: NAVD88 ELEVATION: 444.77 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,121,024.26 E: 880,328.85 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-17.8) CCR - (ML) sandy SILT, non-plastic fines, fine sand, some sub-angular gravels; dusky yellowish brown (10YR 2/2), ASH; non-cohesive, dry, loose 1 SO 439.8 5.0 - 5 (5.0) SAA (Same As Above) except, compact ML - 10 SO 3 Sonic - 15 6 SO (17.8-22.0) (ML) sandy CLAYEY SILT, low plasticity fines, fine sand; moderate brown (5YR 4/4); cohesive, w<PL, firm ML - 20 SEC LOGS.GPJ GLDR_CO.GDT 422.8 22.0 (22.0-25.0) (SP) SAND, fine sand, trace non-plastic fines; dark yellowish brown (10YR 4/2); non-cohesive, 5 SO SP ft bgs 2/16/2016 (25.0-30.0) (ML) CLAYEY SILT, low to medium plasticity fines, some fine sand; light olive gray (5Y 5/2); cohesive, w~PL, firm - 25 RECORD OF BOREHOLE MWD 5.0 5.0 ML SO 6 414.8 Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JS

CHECKED: JSI

REVIEWED: PJJ/MNH

10/9/17

GOLDER STL

DRILLING CONTRACTOR: Cascade

DRILLER: J. Drabek

Golder

Associates

RECORD OF BOREHOLE LMW-8S SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 12/15/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DATUM: NAVD88 ELEVATION: 444.77 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,121,024.26 E: 880,328.85 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER USCS TYPE DEPTH (ft) - 30 (30.0-45.2) (SW) SAND, fine to coarse sub-rounded sand; moderate yellowish brown (10YR 5/4); non-cohesive, moist, compact 30.0 9.7 10.0 - 35 7 SO 6" Sonic SW 404.8 40.0 40 (40.0) SAA except, trace sub-rounded gravel; wet <u>4.1</u> 5.2 8 SO - 45 399.6 45.2 END OF BORING AT 45.2 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG LMW-8S. GOLDER STL RECORD OF BOREHOLE MWD SEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 50 - 55 LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

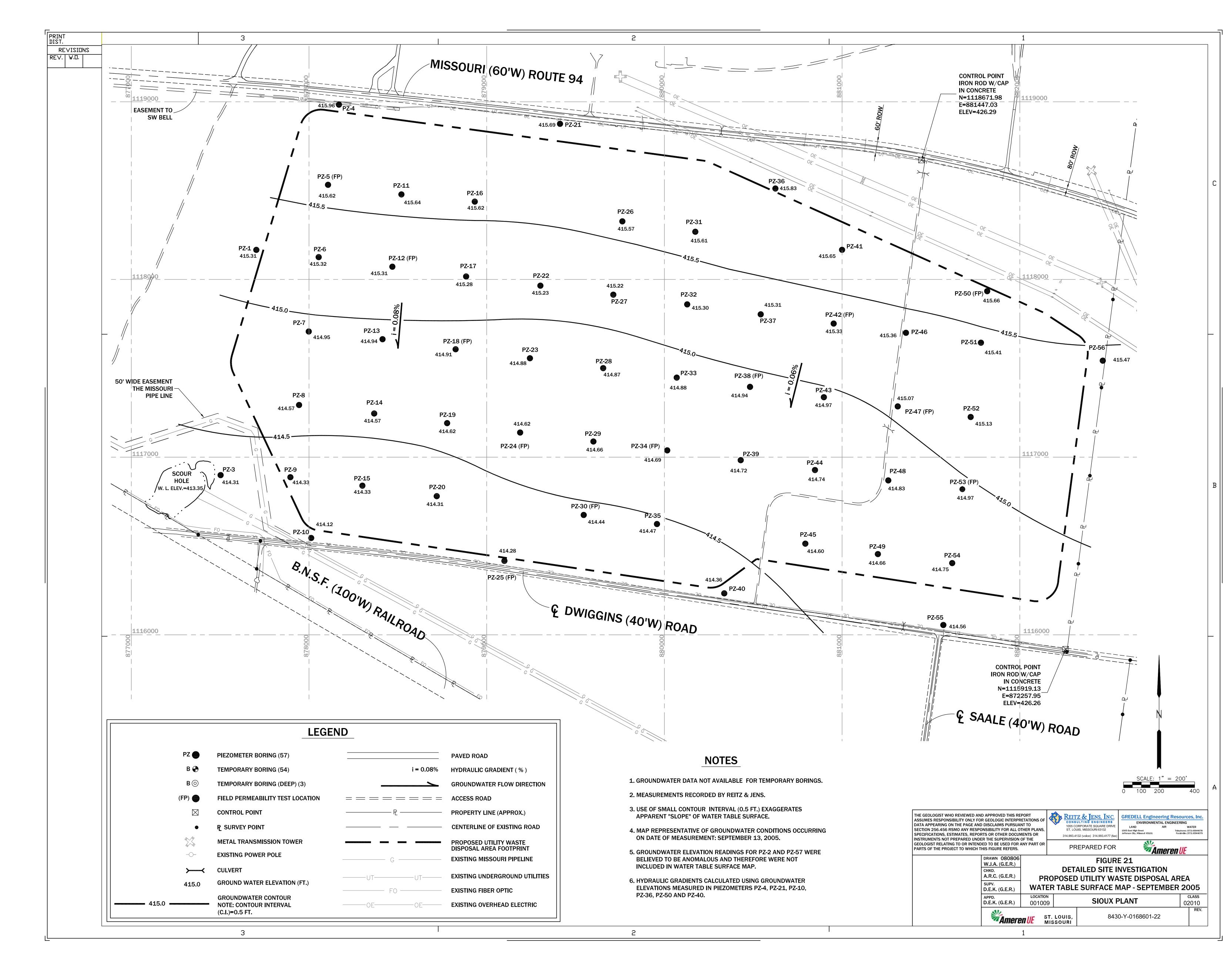
RECORD OF BOREHOLE LMW-9S SHEET 1 of 2 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 443.66 DRILLING METHOD: 0 Some DRILLING DATE: 12/18/2015 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,121,905.88 E: 879,849.27 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 0 Hydrovac was used on the first 8 ft to insure no utility lines would be hit (0.0-8.0) Air knife/hydrovac excavation Hydrovac 0.0 8.0 NA 1 NA - 5 435.7 8.0 (8.0-12.3) CCR - (SP) SAND, fine to medium sub-angular sand, some non-plastic fines; dusky yellowish brown (10YR 2/2), ASH; non-coheisve, dry, loose 2.0 2.0 2 SO 433.7 10.0 10 SP (10.0) SAA (Same As Above) except, trace sub-angular gravel (12.3-15.0) - FILL (GP) sandy GRAVEL, fine to coarse sub-angular gravel, fine to coarse sub-angular sand; very pale orange (10YR 8/2); non-cohesive, dry, 3 SO 0 GP 428.7 15.0 - 15 (15.0-22.0) (ML) CLAYEY SILT, low plasticity fines; grayish black (N2); cohesive, w<PL, firm 4 SO Sonic .0 10/9/17 - 20 SEC LOGS.GPJ GLDR_CO.GDT (22.0-25.0) (SM) SILTY SAND, fine sand, non-plastic fines; dark gray (N3); non-cohesive, wet, compact SM SO - 25 (25.0-40.0) (SP) SAND, fine sands; moderate yellowish brown (10YR 5/4); non-cohesive, wet, compact 5 RECORD OF BOREHOLE MWD SP Log continued on next page GOLDER STL LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

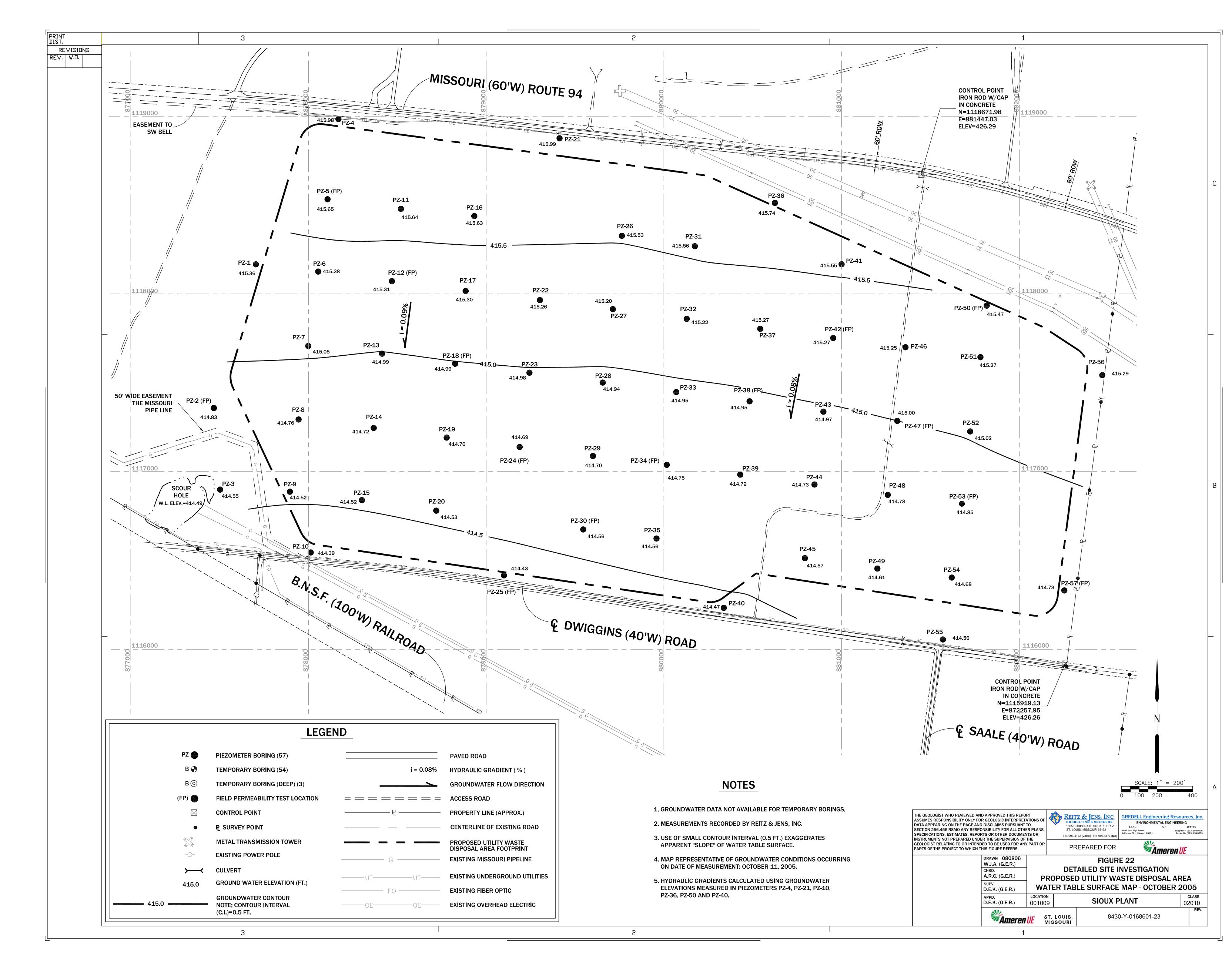
RECORD OF BOREHOLE LMW-9S SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 12/18/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOCATION: Sioux Energy Center DATUM: NAVD88 ELEVATION: 443.66 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 1,121,905.88 E: 879,849.27 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER USCS TYPE DEPTH (ft) (25.0-40.0) (SP) SAND, fine sands; moderate yellowish brown (10YR 5/4); non-cohesive, wet, compact (Continued) - 30 <u>5.0</u> 5.0 6 SO - 35 SP 40 END OF BORING AT 40.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG LMW-9S. - 45 GOLDER STL RECORD OF BOREHOLE MWD SEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 50 - 55 LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

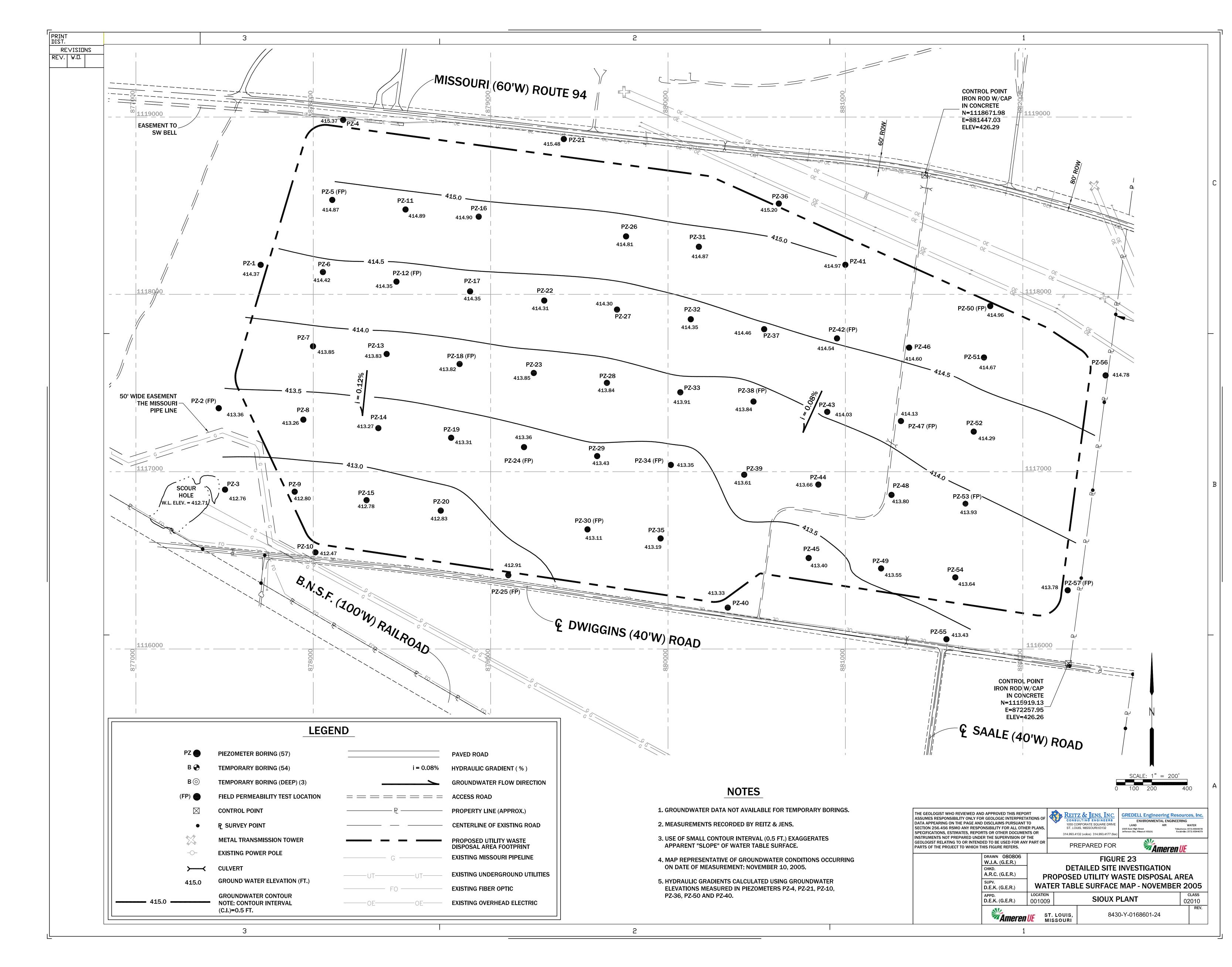
RECORD OF BOREHOLE BMW-1S SHEET 1 of 1 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 425.98 DRILLING DATE: 12/8/2015 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 LOCATION: Sioux Energy Center COORDINATES: N: 1,121,709.18 E: 876,755.57 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT NUMBER DESCRIPTION TYPE USCS DEPTH (ft) - 0 (0.0-8.5) (ML) sandy SILT, non-plastic to very low plasticity fines, fine sand, trace organics (roots); brownish gray (5YR 4/1); non-cohesive, moist, loose 2.4 5.0 1 SO ML 421.0 5.0 - 5 (5.0) SAA (Same As Above), no organics Water Level 6.33 ft
 Water Level 6.35 ft
 bgs 2/16/2016 SO (8.5-15.6) (CL) SILTY CLAY, medium plasticity fines, trace fine sand; light brownish gray (5YR 6/1); cohesive, w~PL, firm 10 Sonic CL 2.8 5.0 SO 3 6 - 15 Run #4, Sample appears to be compacted while being extruded into sample bags. Measured field recovery: 5.2/10.0. Estimated actual recovery: 7.5/10.0. (15.6-17.5) (SP-SM) SAND, fine sand, some non-plastic fines; light brown (5YR 5/6); non-cohesive, wet, compact SP-SM (17.5-18.5) (CL) SILTY CLAY, medium plasticity fines, CL trace fine sand; medium dark gray (N4); cohesive, w~PL, 407.5 18.5 (18.5-25.0) (SP-SM) SAND, fine sand, some non-plastic fines; medium dark gray (N4); non-cohesive, wet, compact 7.5 10.0 10/9/17 - 20 SO SEC LOGS.GPJ GLDR_CO.GDT SP-SM - 25 END OF BORING AT 25.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION RECORD OF BOREHOLE MWD GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JSI/JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

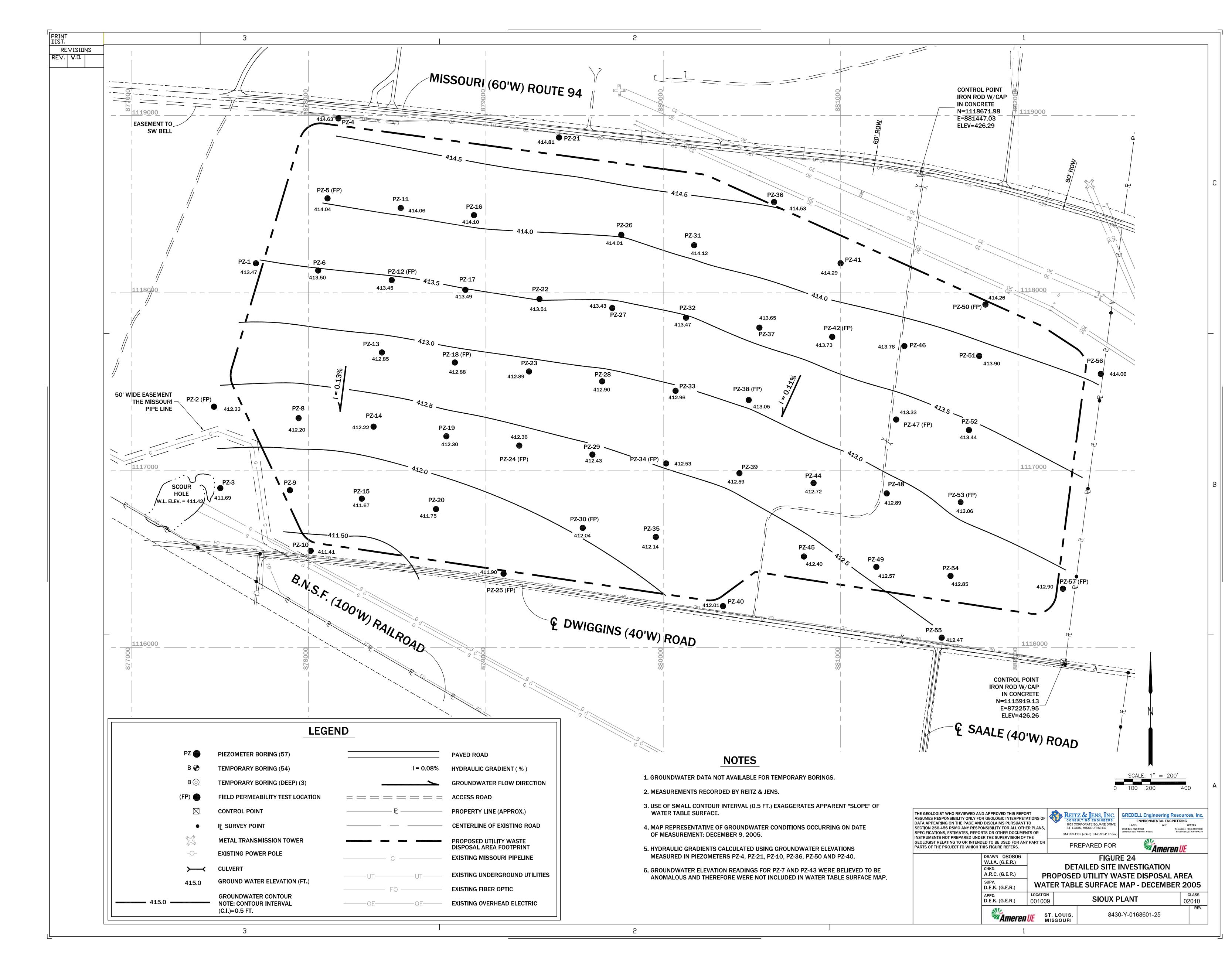
RECORD OF BOREHOLE BMW-3S SHEET 1 of 1 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.003B LOÇATION: Sioux Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 424.12 DRILLING DATE: 11/8/2016 AZIMUTH: N/A INCLINATION: -90 DRILL RIG: Geoprobe (8140CC) COORDINATES: N: 1,121,792.93 E: 875,809.46 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 0 (0.0-1.2) (CH) CLAY, high plasticity fines, some organics; dusky brown (5YR 2/2); cohesive, w~PL, firm СН 422.9 1.2 (1.2-12.0) (CL) SILTY CLAY, medium plasticity fines; pale brown (5YR 5/2); cohesive, w~PL, moist 4.4 5.0 1 SO - 5 CL 10 Sonic (12.0-22.2) (SP) SAND, fine to medium sub-angular sand, trace non-plastic fines; light brown (5YR 6/4); non-cohesive, wet, compact 3 SO 409.1 - 15 (15.0) Same As Above (SAA) excpet color to pale brown (5YR 5/2) SP 3.4 5.0 4 SO 10/9/17 - 20 SEC LOGS.GPJ GLDR_CO.GDT 3.3 4.0 5 SO (22.2-24.0) (SM) SILTY SAND, fine to medium sand, some non-plastic fines; medium gray (N5); non-cohesive, wet, compact SM END OF BORING AT 24.2 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION - 25 LOG BMW-3S. GOLDER STL RECORD OF BOREHOLE MWD LOGGED: MSG SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JS Golder DRILLER: M. Rodrigues REVIEWED: MNH Associates

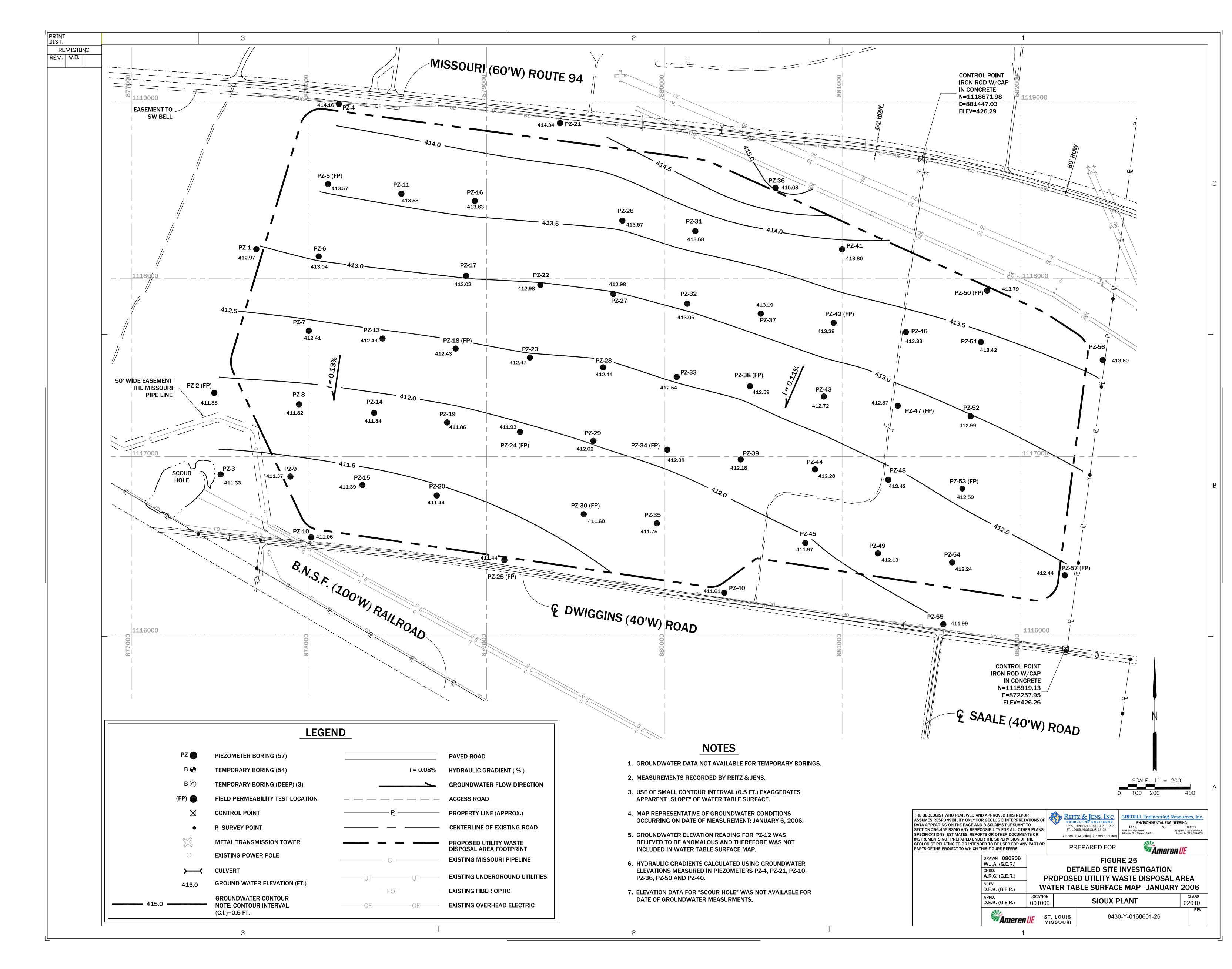
APPENDIX B HISTORICAL POTENTIOMETRIC SURFACE MAPS

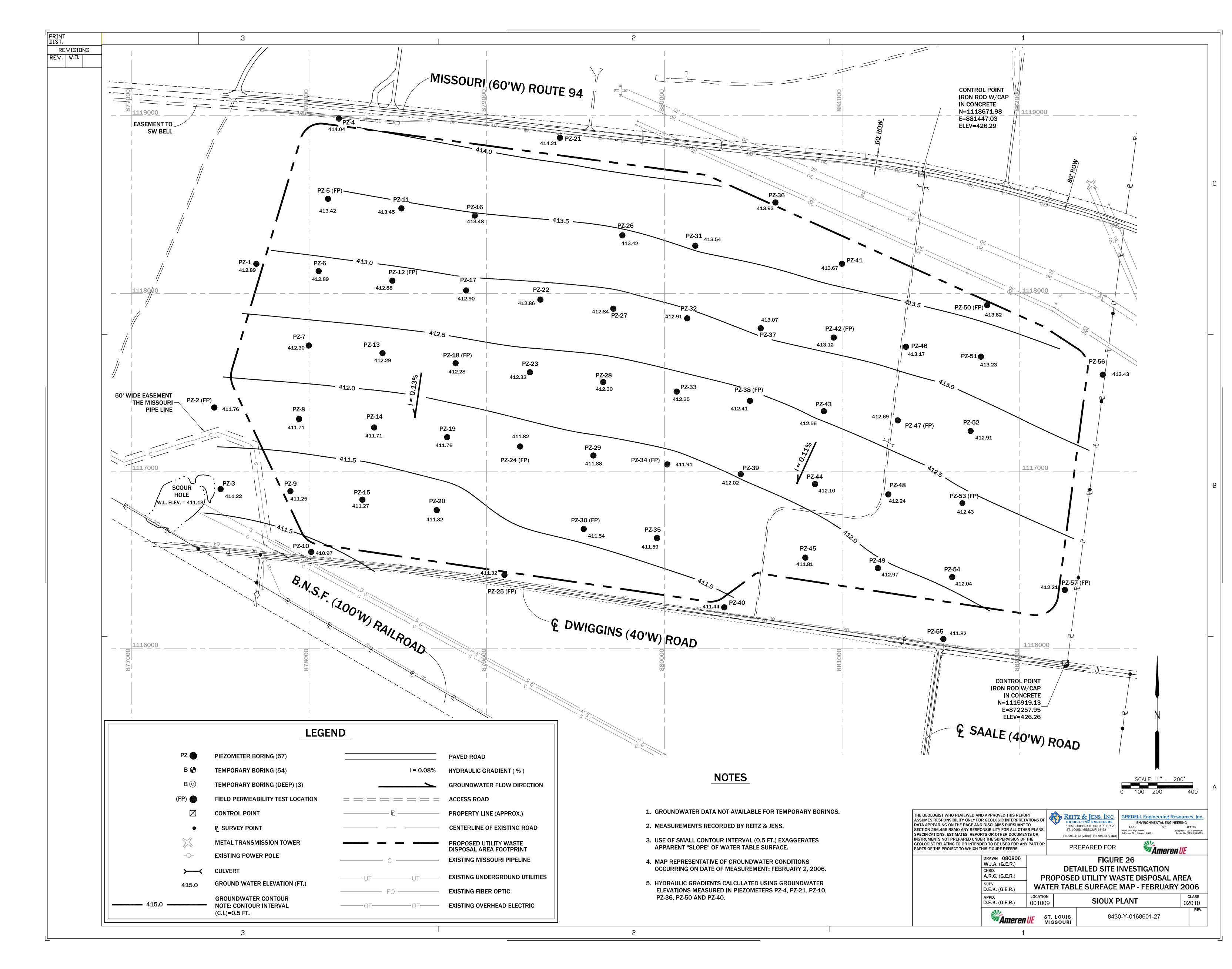


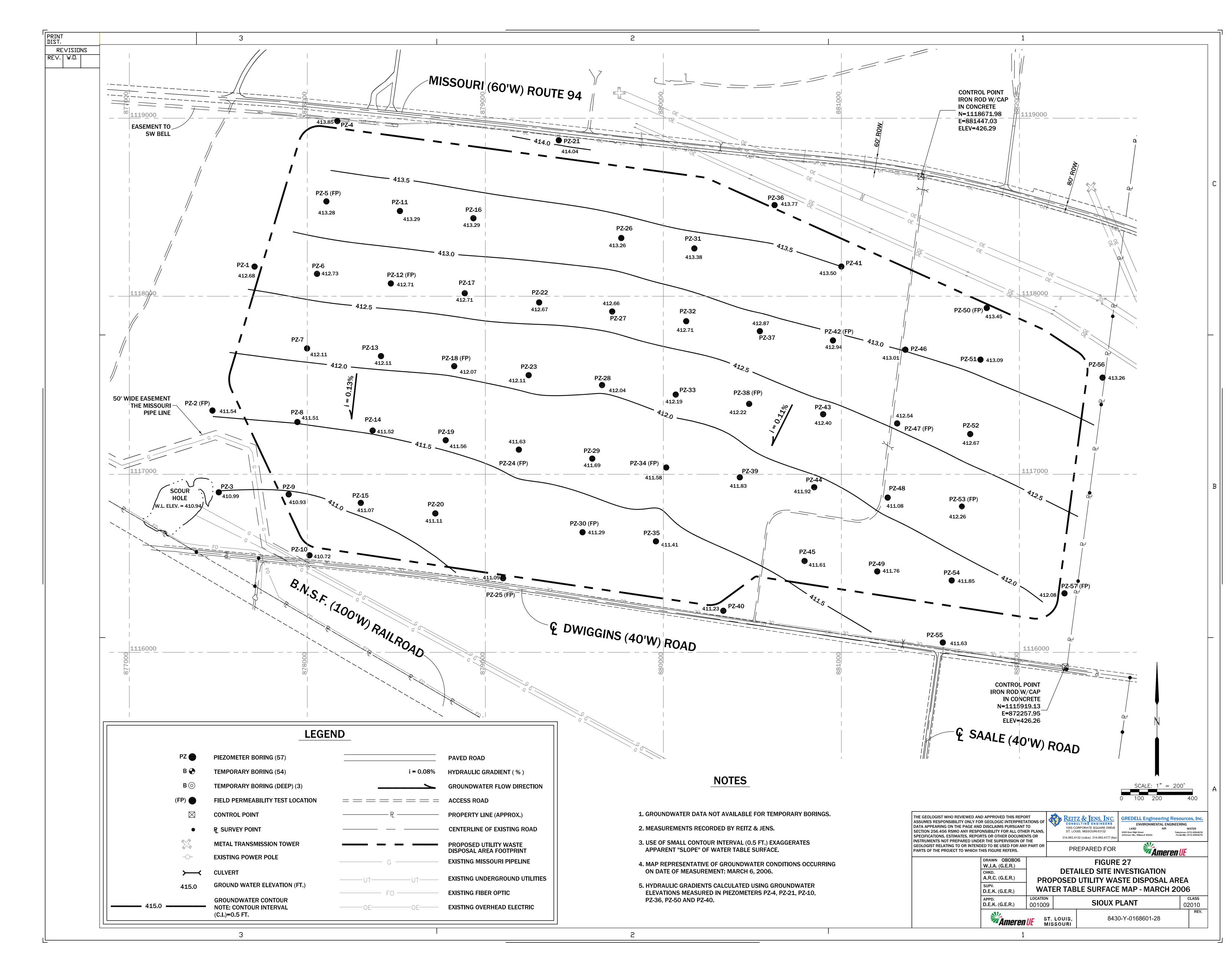


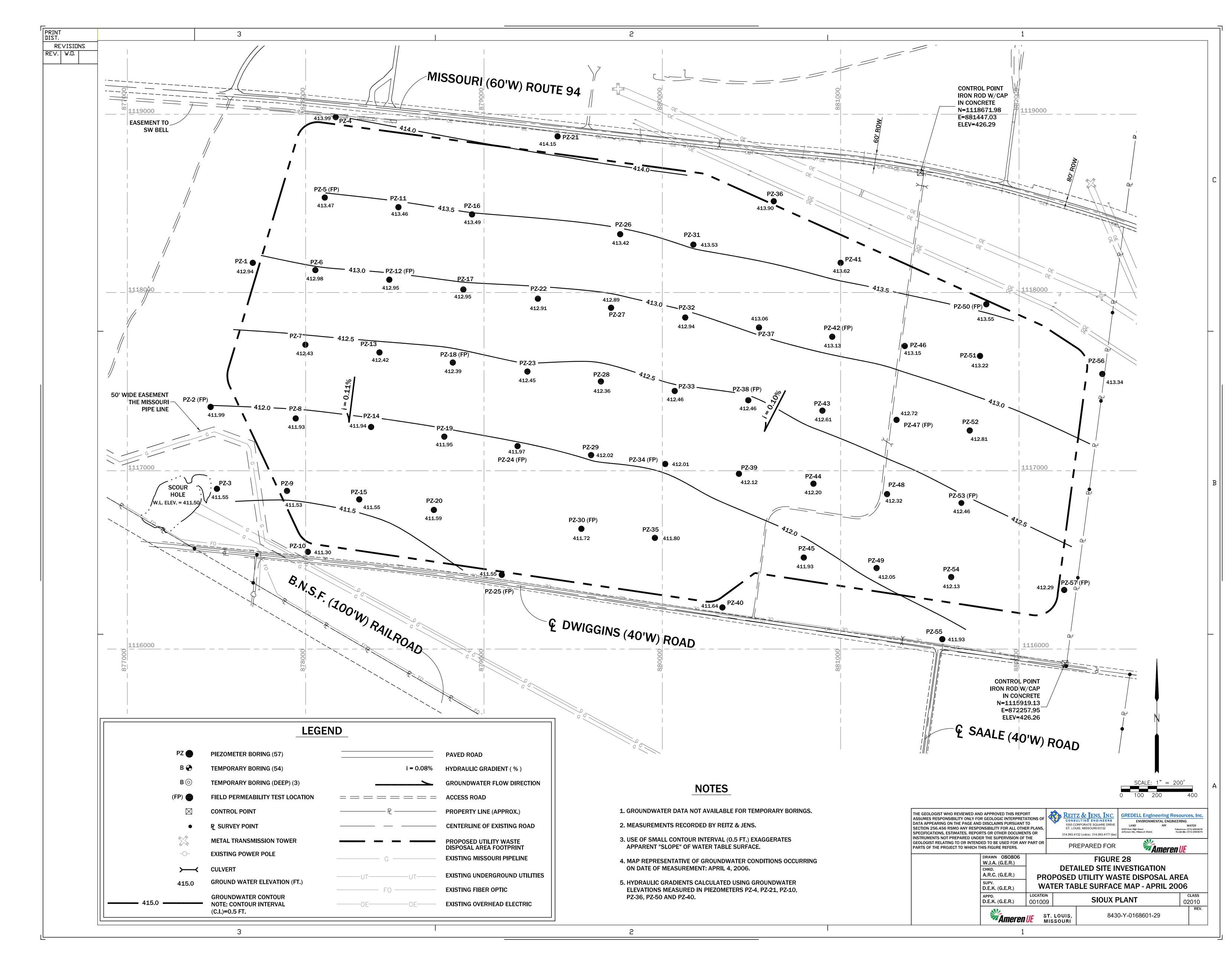


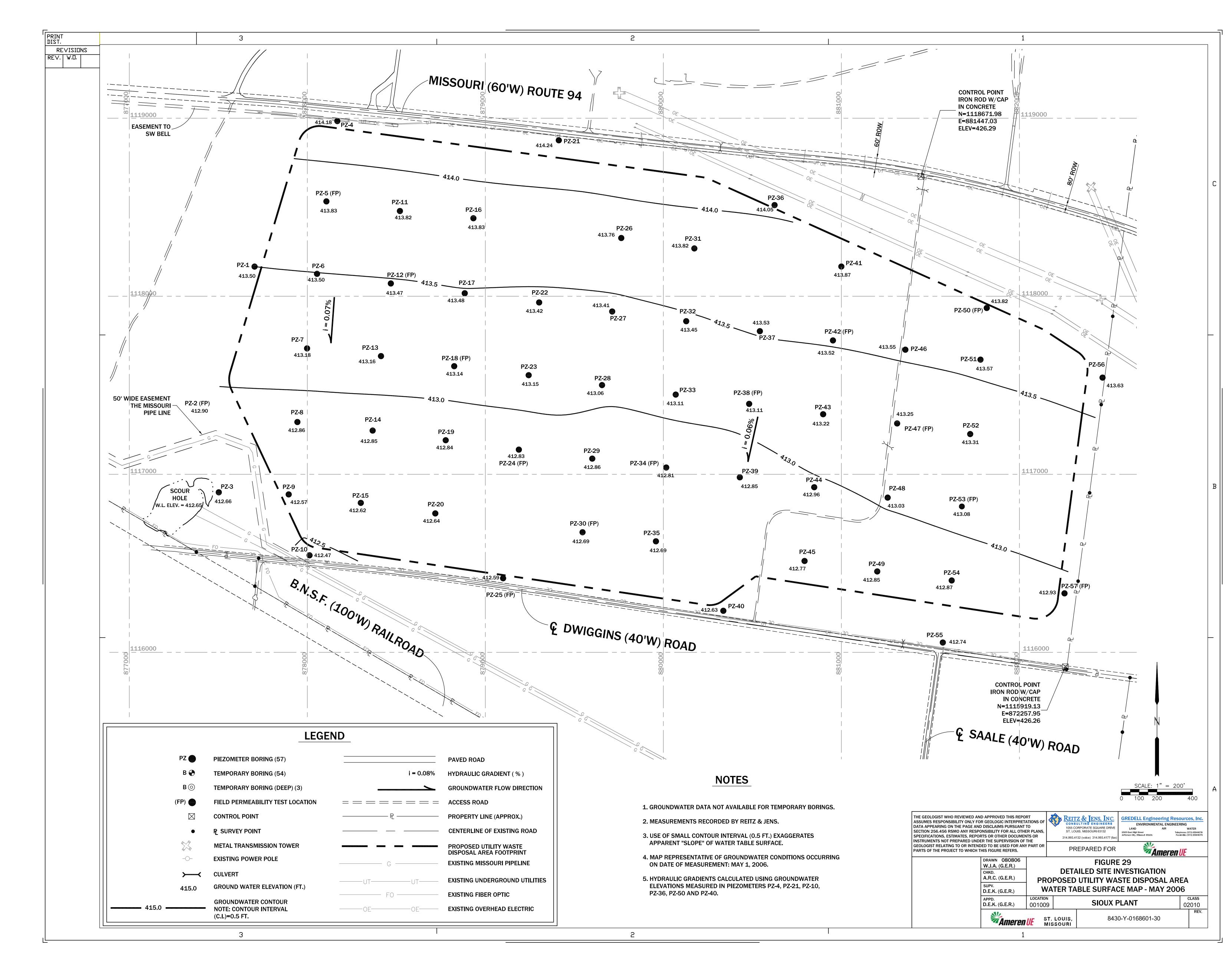


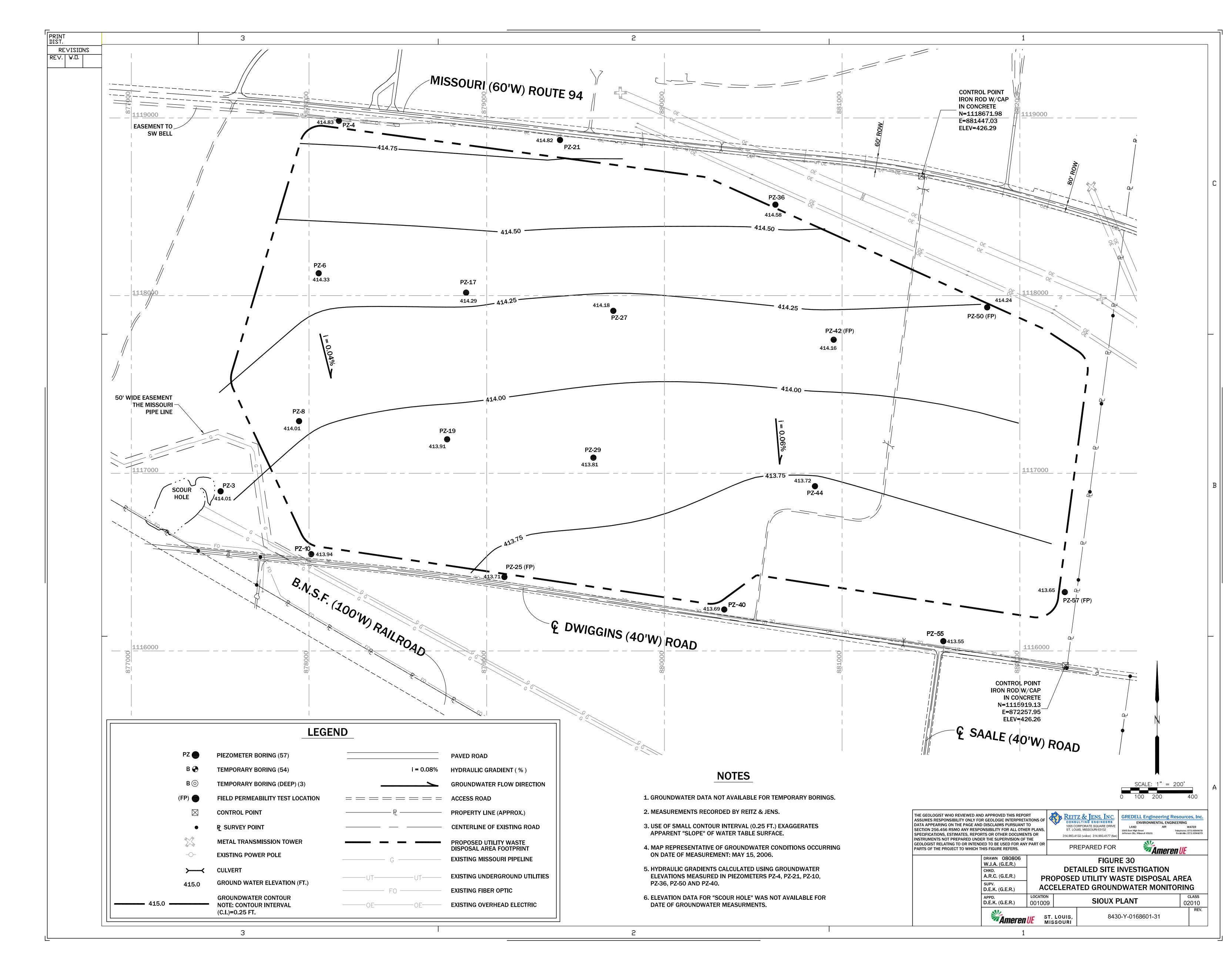


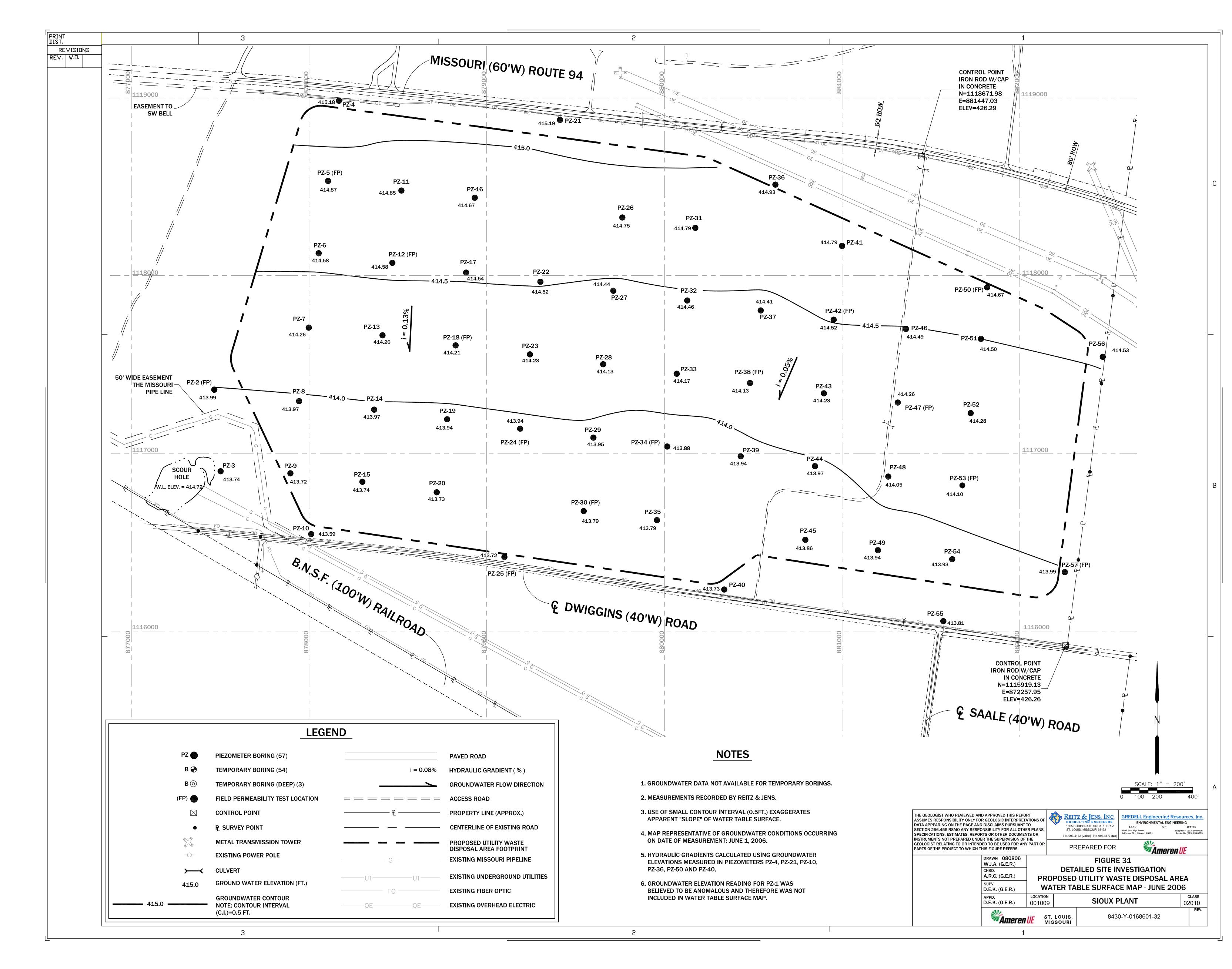


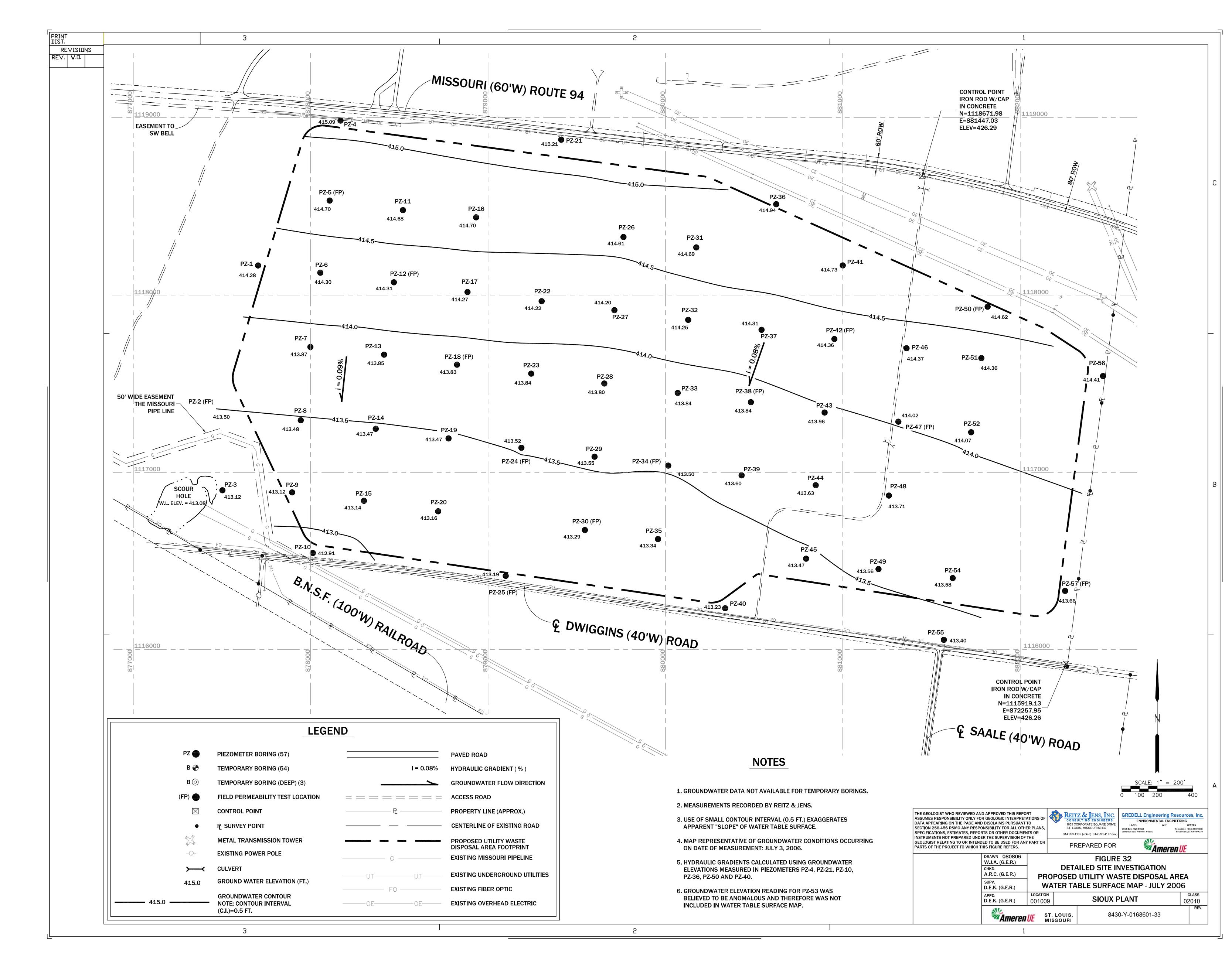


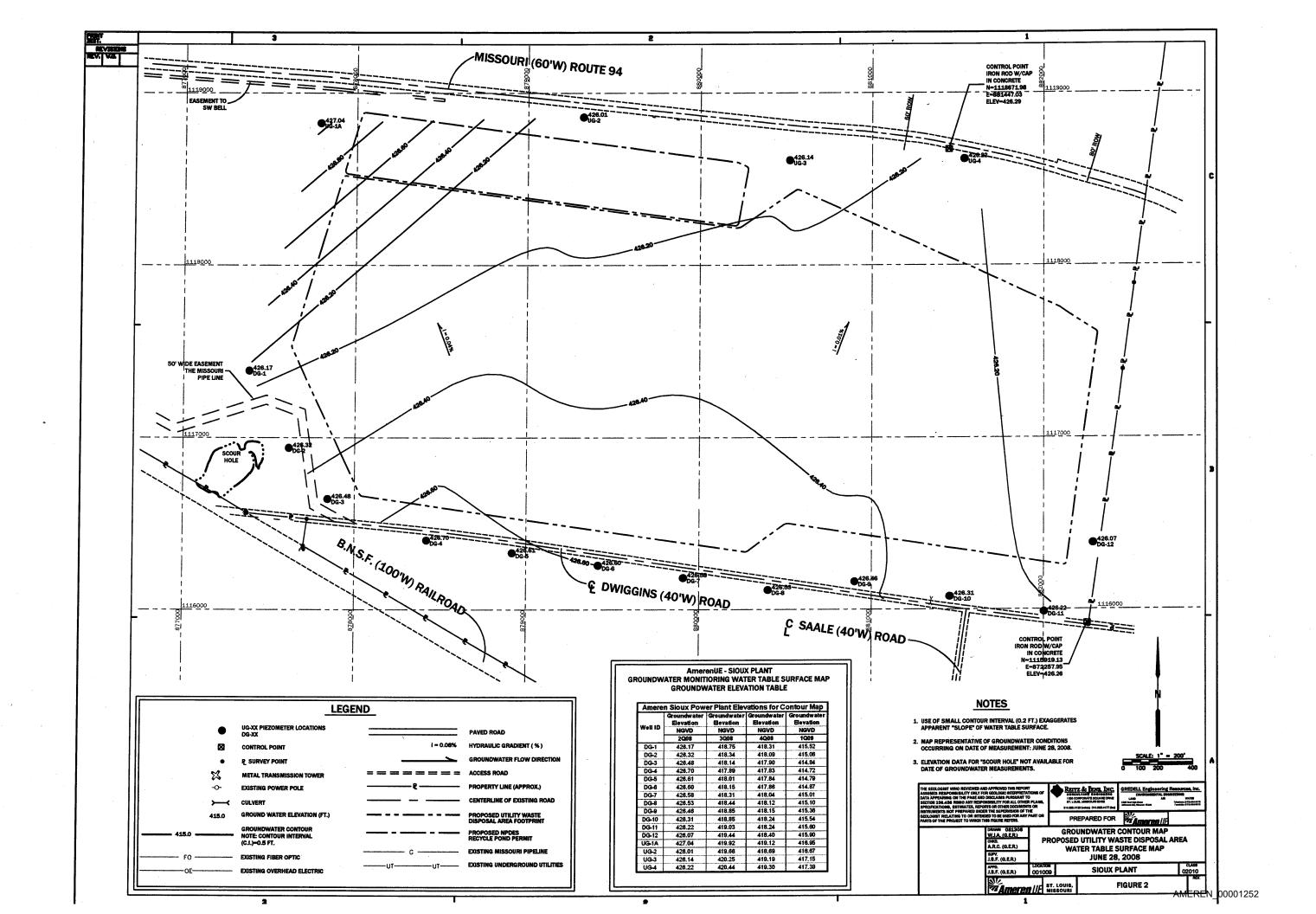


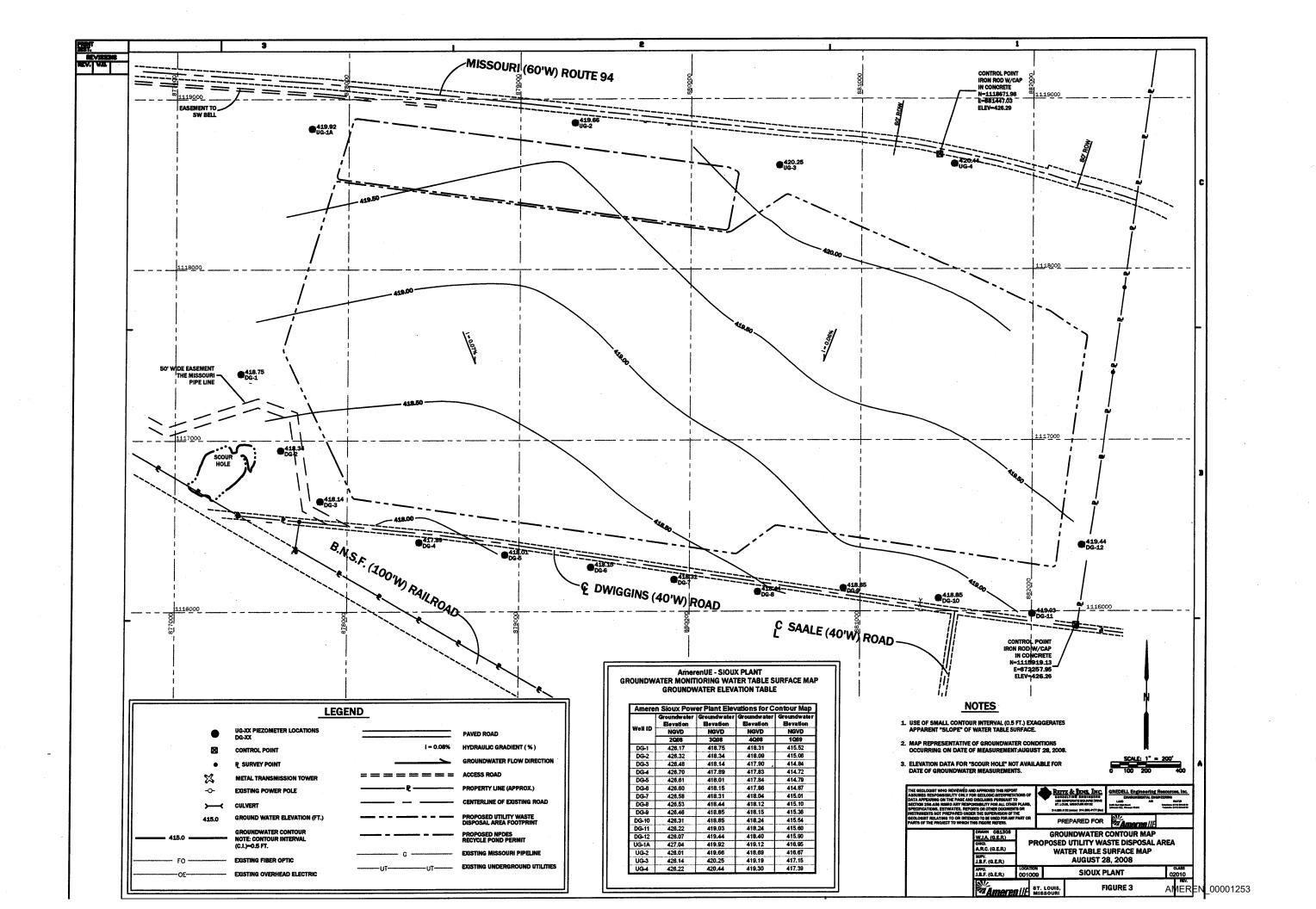


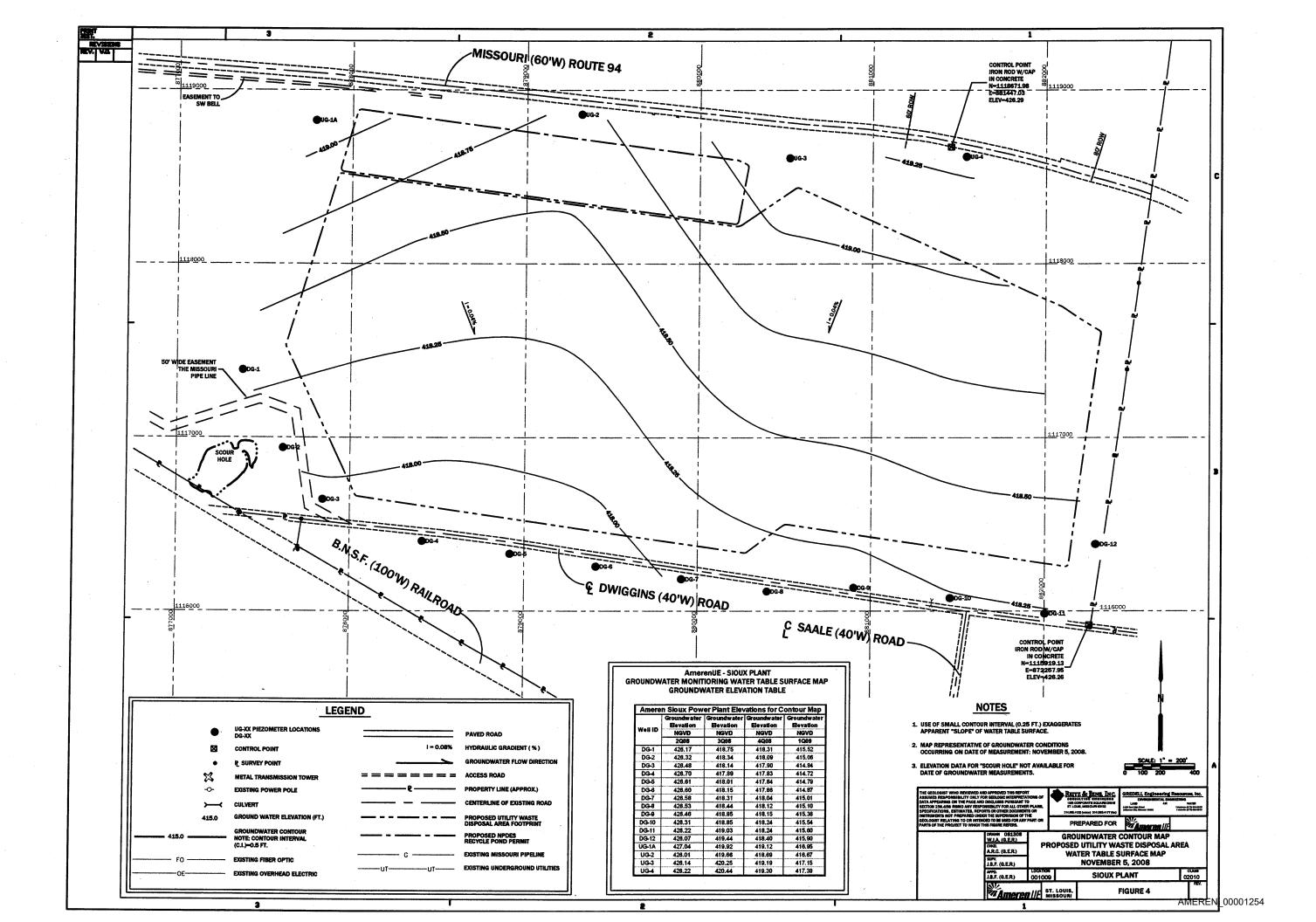


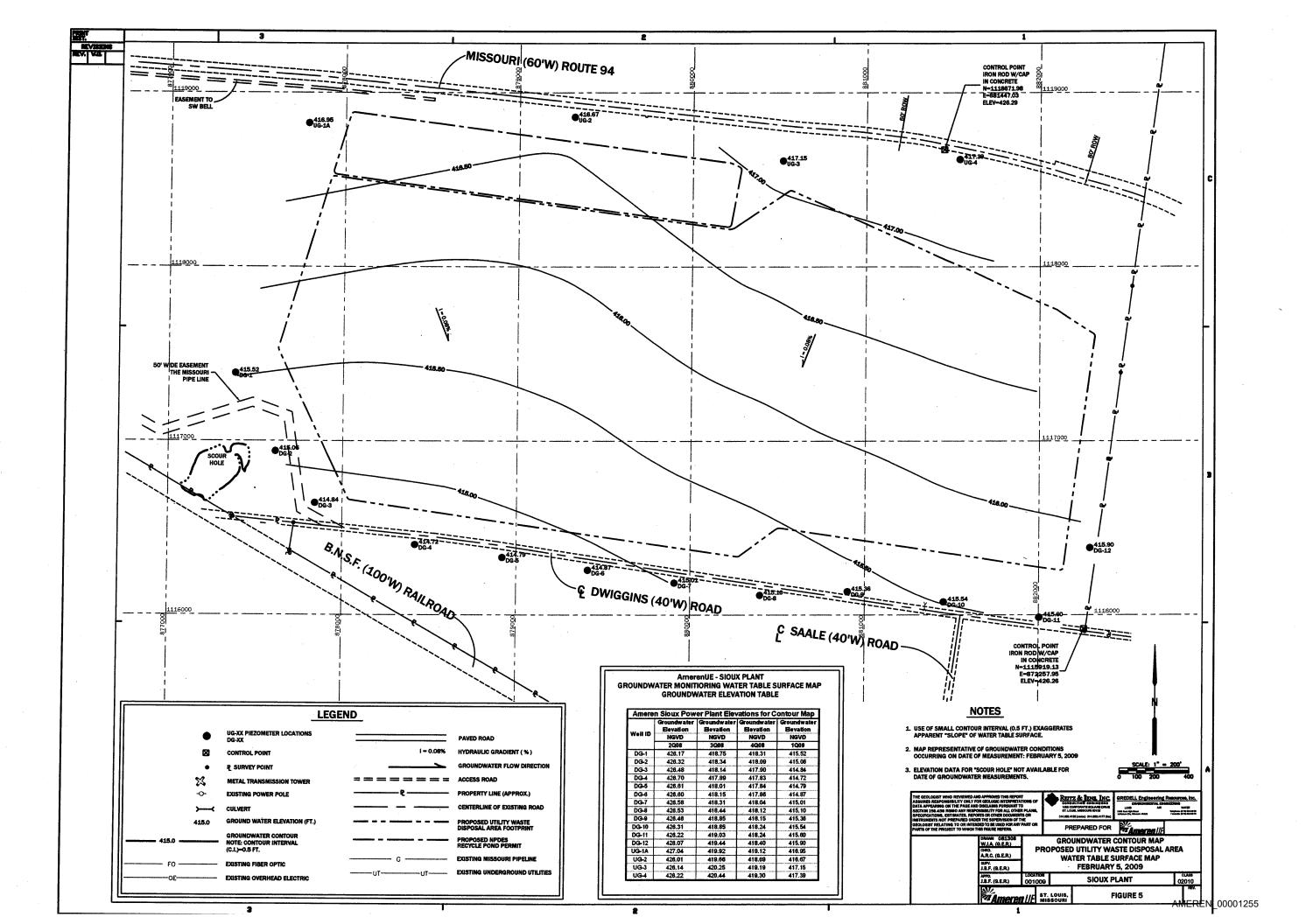












APPENDIX C POTENTIOMETRIC SURFACE MAPS FROM BACKGROUND CCR SAMPLING EVENTS













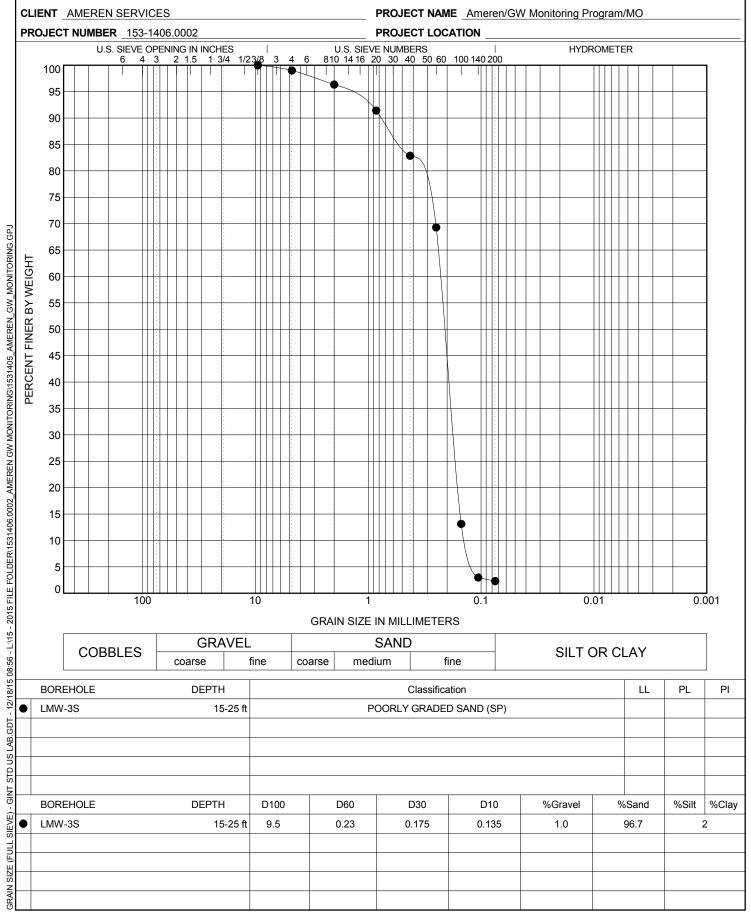


APPENDIX D GRAIN SIZE DISTRIBUTION



500 Century Plaza Drive, Suite 190 Houston, Texas 77073 **Golder** Telephone: (281) 821-6868 Fax: (281) 821-6870

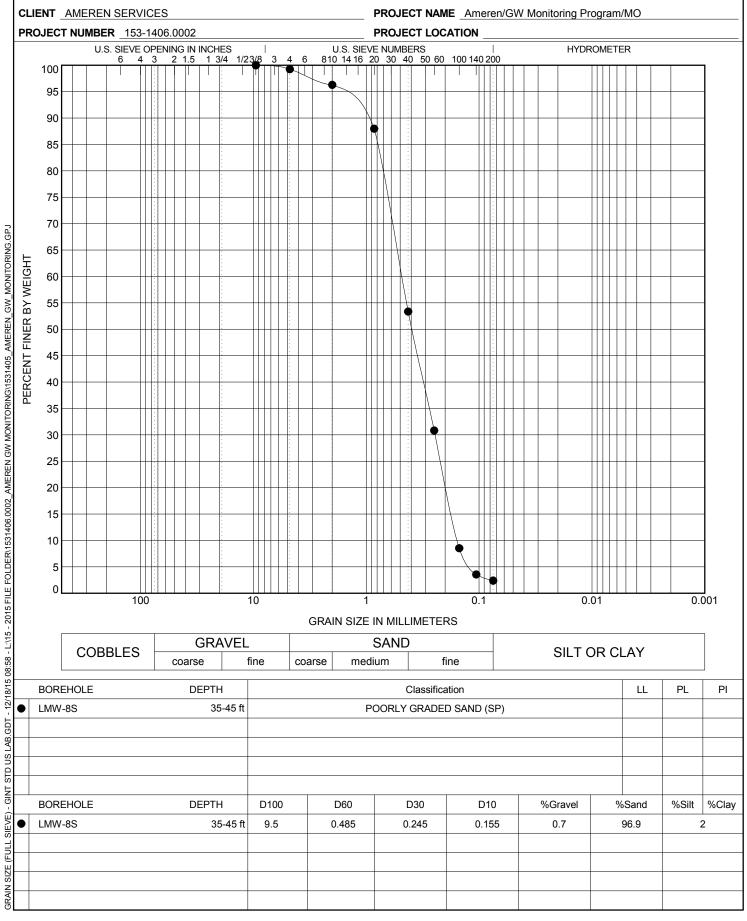
GRAIN SIZE DISTRIBUTION ASTM D6913 Method B





500 Century Plaza Drive, Suite 190 Houston, Texas 77073 **Golder** Telephone: (281) 821-6868 Fax: (281) 821-6870

GRAIN SIZE DISTRIBUTION ASTM D6913 Method B



APPENDIX E CCR MONITORING WELL CONSTRUCTION DIAGRAMS



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG LMW-1S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0003B SITE NAME: SIOUX ENERGY CENTER LOCATION: LMW-1S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 445.4 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 1121320.4 EASTING: 879427.2 DRILLER: J. DRABEK STATIC WATER LEVEL: 26.75 FT BTOC COMPLETION DATE: 12/15/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK . TOP OF CASING ELEVATION: 447.10 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: 1.7 FT - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 445.4 FT MSL DIAMETER OF RISER PIPE (in.): DIAMETER OF BOREHOLE (in.): - CONCRETE SEAL DEPTH (ft. bgs): ______ - TYPE AND AMOUNT OF ANNULAR SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 2 BAGS TYPE AND AMOUNT OF ANNULAR SEAL: HIGH SOLIDS BENTONITE 1.5 BAGS TOP OF BENTONITE SEAL DEPTH (ft. bgs): 24.0 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 1 BAG - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 28.7 FINE: 27.5 - CENTRALIZER (yes (no) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): 30.6 TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: _____COARSE: 3 \frac{1}{3} BAGS FINE: \frac{1}{3} BAG BOTTOM OF SCREEN DEPTH (ft. bgs): 40.4 - BOTTOM OF WELL DEPTH (ft. bgs): 40.8 BOTTOM OF FILTER PACK (ft. bgs): ____ TOTAL DEPTH OF BOREHOLE: 41.0 FT TYPE AND AMOUNT OF BACKFILL: 0.2 FT - NATURAL CAVE IN ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 75 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 14, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM
DATE CHECKED: 4/20/2016

PREPARED BY MEREN JOS OF BEZI



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG ___LMW-2S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0003B SITE NAME: SIOUX ENERGY CENTER LOCATION: LMW-2S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 445.2 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 1120332.8 EASTING: 879283.7 DRILLER: J. DRABEK STATIC WATER LEVEL: 27.04 FT BTOC COMPLETION DATE: 12/16/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK TOP OF CASING ELEVATION: 447.16 FT MSL - PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM 2.0 FT STICK UP: ___ PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 445.2 FT MSL DIAMETER OF RISER PIPE (in.): ___ DIAMETER OF BOREHOLE (in.): __ CONCRETE SEAL DEPTH (ft. bgs): ____ - TYPE AND AMOUNT OF ANNULAR SEAL: $\frac{3}{8}$ " BENTONITE CHIPS - 2 BAGS TYPE AND AMOUNT OF ANNULAR SEAL: HIGH SOLIDS BENTONITE 1.5 BAGS - TOP OF BENTONITE SEAL DEPTH (ft. bgs): 22.0 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 1 BAG - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 28.5 FINE: 27.0 NONE - CENTRALIZER (yes (no) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN COARSE: #1 FINE: #0 SIZE OF SAND PACK: _____ AMOUNT OF SAND: COARSE: 4 BAGS FINE: ¹/₃ BAG BOTTOM OF SCREEN DEPTH (ft. bgs): ___ BOTTOM OF WELL DEPTH (ft. bgs): _____ BOTTOM OF FILTER PACK (ft. bgs): ___ TOTAL DEPTH OF BOREHOLE: 41.0 FT - TYPE AND AMOUNT OF BACKFILL: ___ ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 50 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 14, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM

DATE CHECKED: 4/20/2016

PREPARED BY MEREN JOS US 221



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG ____LMW-3S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0003B SITE NAME: SIOUX ENERGY CENTER LOCATION: LMW-3S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 428.4 FT MSL GEOLOGIST: J. INGRAM NORTHING: 1119348.8 EASTING: 878856.4 DRILLER: J. DRABEK STATIC WATER LEVEL: 6.31 FT BTOC COMPLETION DATE: 12/18/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK TOP OF CASING ELEVATION: 430.17 FT MSL - PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ____1.8 FT PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 428.4 FT MSL DIAMETER OF RISER PIPE (in.): ___ DIAMETER OF BOREHOLE (in.): ___ 2.5 - CONCRETE SEAL DEPTH (ft. bgs): ______ NONE - TYPE AND AMOUNT OF ANNULAR SEAL: _____ - TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ " BENTONITE CHIPS - 2 BAGS - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 12.2 FINE: 11.5 NONE - CENTRALIZER (yes (no) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN COARSE: #1 FINE: #0 SIZE OF SAND PACK: _____ AMOUNT OF SAND: COARSE: 3 ½ BAGS FINE: ½ BAG BOTTOM OF SCREEN DEPTH (ft. bgs): _____ BOTTOM OF WELL DEPTH (ft. bgs): _____ - BOTTOM OF FILTER PACK (ft. bgs): ____ TOTAL DEPTH OF BOREHOLE: 25.0 FT TYPE AND AMOUNT OF BACKFILL: 0.6 FT - NATURAL CAVE IN ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 50 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 14, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM

DATE CHECKED: 4/20/2016



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG LMW-4S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0003B SITE NAME: SIOUX ENERGY CENTER LOCATION: LMW-4S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 427.3 FT MSL GEOLOGIST: J. INGRAM NORTHING: 1119226.6 EASTING: 879561.5 DRILLER: J. DRABEK STATIC WATER LEVEL: 5.50 FT BTOC COMPLETION DATE: 12/18/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK - TOP OF CASING ELEVATION: 429.40 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ___2.1 FT - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 427.3 FT MSL DIAMETER OF RISER PIPE (in.): DIAMETER OF BOREHOLE (in.): ___ - CONCRETE SEAL DEPTH (ft. bgs): 2.5 TYPE AND AMOUNT OF ANNULAR SEAL: NONE - TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ " BENTONITE CHIPS - 2 BAGS - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 12.5 FINE: 12.0 - CENTRALIZER (yes (no)) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): 14.9 TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: COARSE: 3 ½ BAGS FINE: ½ BAG BOTTOM OF SCREEN DEPTH (ft. bgs): - BOTTOM OF WELL DEPTH (ft. bgs): ______25.1 BOTTOM OF FILTER PACK (ft. bgs): ____ TOTAL DEPTH OF BOREHOLE: 25.1 FT TYPE AND AMOUNT OF BACKFILL: _____ ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 50 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 14, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM DATE CHECKED: 4/20/2016



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG ___LMW-5S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0003B SITE NAME: SIOUX ENERGY CENTER LOCATION: LMW-5S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 445.5 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 1119250.6 EASTING: 880348.6 DRILLER: J. DRABEK STATIC WATER LEVEL: 27.92 FT BTOC COMPLETION DATE: 12/14/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK TOP OF CASING ELEVATION: 447.36 FT MSL - PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ____1.9 FT PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 445.5 FT MSL DIAMETER OF RISER PIPE (in.): ____ DIAMETER OF BOREHOLE (in.): __ CONCRETE SEAL DEPTH (ft. bgs): ____ - TYPE AND AMOUNT OF ANNULAR SEAL: $\frac{3}{8}$ " BENTONITE CHIPS - 2 BAGS TYPE AND AMOUNT OF ANNULAR SEAL: HIGH SOLIDS BENTONITE 0.5 BAG - TOP OF BENTONITE SEAL DEPTH (ft. bgs): 26.0 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 1 BAG - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 32.0 FINE: 31.0 - CENTRALIZER (yes (no)) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN COARSE: #1 FINE: #0 SIZE OF SAND PACK: _____ AMOUNT OF SAND: COARSE: 3 BAGS FINE: \$\frac{1}{3}\$ BAG BOTTOM OF SCREEN DEPTH (ft. bgs): BOTTOM OF WELL DEPTH (ft. bgs): _____ 45.6 BOTTOM OF FILTER PACK (ft. bgs): ____ TOTAL DEPTH OF BOREHOLE: 45.6 FT TYPE AND AMOUNT OF BACKFILL: ____ ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 100 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 14, 2016. FT BTOR = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM

DATE CHECKED: 4/20/2016

PREPARED BY MEREN JOSO 1272 ZI



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG LMW-6S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0003B SITE NAME: SIOUX ENERGY CENTER LOCATION: LMW-6S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 444.1 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 1119782.0 EASTING: 880867.8 DRILLER: J. DRABEK STATIC WATER LEVEL: 21.70 FT BTOC COMPLETION DATE: 12/14/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK TOP OF CASING ELEVATION: 446.00 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ____1.9 FT PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 444.1 FT MSL DIAMETER OF RISER PIPE (in.): ___ DIAMETER OF BOREHOLE (in.): __ CONCRETE SEAL DEPTH (ft. bgs): ___ TYPE AND AMOUNT OF ANNULAR SEAL: $\frac{3}{8}$ "BENTONITE CHIPS - 1.5 BAGS TYPE AND AMOUNT OF ANNULAR SEAL: HIGH SOLIDS BENTONITE 0.5 BAG - TOP OF BENTONITE SEAL DEPTH (ft. bgs): 21.0 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 1 BAG - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 27.5 FINE: 26.5 NONE - CENTRALIZER (yes (no) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): _____ TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN COARSE: #1 FINE: #0 SIZE OF SAND PACK: _____ AMOUNT OF SAND: COARSE: 3 \frac{1}{3} BAGS FINE: \frac{1}{3} BAG BOTTOM OF SCREEN DEPTH (ft. bgs): ___ BOTTOM OF WELL DEPTH (ft. bgs): _____ 40.2 BOTTOM OF FILTER PACK (ft. bgs): ___ TOTAL DEPTH OF BOREHOLE: 40.2 FT TYPE AND AMOUNT OF BACKFILL: ___ ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 75 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 14, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM DATE CHECKED: 4/20/2016

PREPARED BY MEREN JOOS OF 2721



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG LMW-7S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0003B SITE NAME: SIOUX ENERGY CENTER LOCATION: LMW-7S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 442.2 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 1120261.0 EASTING: 88650.0 DRILLER: J. DRABEK STATIC WATER LEVEL: 20.78 FT BTOC COMPLETION DATE: 12/14/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK . - TOP OF CASING ELEVATION: 444.26 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ___2.1 FT - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 442.2 FT MSL DIAMETER OF RISER PIPE (in.): DIAMETER OF BOREHOLE (in.): ___ - CONCRETE SEAL DEPTH (ft. bgs): 2.5 TYPE AND AMOUNT OF ANNULAR SEAL: NONE - TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 5 BAGS - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 27.0 FINE: 26.0 NONE - CENTRALIZER (yes (no)) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): 30.0 TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: COARSE: 3 ½ BAGS FINE: 3 BAG BOTTOM OF SCREEN DEPTH (ft. bgs): _____ - BOTTOM OF WELL DEPTH (ft. bgs): ______ 40.2 BOTTOM OF FILTER PACK (ft. bgs): ____ TOTAL DEPTH OF BOREHOLE: 40.2 FT TYPE AND AMOUNT OF BACKFILL: _____ ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 75 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 14, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM DATE CHECKED: 4/20/2016



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG LMW-8S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0003B SITE NAME: SIOUX ENERGY CENTER LOCATION: LMW-8S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 444.8 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 1121024.3 EASTING: 880328.8 DRILLER: J. DRABEK STATIC WATER LEVEL: 23.24 FT BTOC COMPLETION DATE: 12/15/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK TOP OF CASING ELEVATION: 446.80 FT MSL - PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ___2.0 FT PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 444.8 FT MSL DIAMETER OF RISER PIPE (in.): ____ DIAMETER OF BOREHOLE (in.): __ CONCRETE SEAL DEPTH (ft. bgs): ____ - TYPE AND AMOUNT OF ANNULAR SEAL: $\frac{3}{8}$ " BENTONITE CHIPS - 1.75 BAGS - TYPE AND AMOUNT OF ANNULAR SEAL: HIGH SOLIDS BENTONITE 1.6 BAGS - TOP OF BENTONITE SEAL DEPTH (ft. bgs): 27.0 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 1 BAG - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 32.5 FINE: 31.5 NONE - CENTRALIZER (yes (no) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: COARSE: 3 BAGS FINE: \$\frac{1}{3}\$ BAG BOTTOM OF SCREEN DEPTH (ft. bgs): BOTTOM OF WELL DEPTH (ft. bgs): _____ 45.2 BOTTOM OF FILTER PACK (ft. bgs): ____ TOTAL DEPTH OF BOREHOLE: 45.2 FT TYPE AND AMOUNT OF BACKFILL: ____ ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 100 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 14, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM DATE CHECKED: 4/20/2016



CHECKED BY: J. INGRAM

DATE CHECKED: 4/20/2016

ABOVE GROUND MONITORING WELL CONSTRUCTION LOG LMW-9S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0003B SITE NAME: SIOUX ENERGY CENTER LOCATION: LMW-9S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 443.7 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 1121905.9 EASTING: 879849.3 DRILLER: J. DRABEK STATIC WATER LEVEL: 23.59 FT BTOC COMPLETION DATE: 12/18/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK - TOP OF CASING ELEVATION: 445.57 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ____1.9 FT - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 443.7 FT MSL DIAMETER OF RISER PIPE (in.): DIAMETER OF BOREHOLE (in.): ___ - CONCRETE SEAL DEPTH (ft. bgs): 2.5 TYPE AND AMOUNT OF ANNULAR SEAL: NONE - TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 3 BAGS - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 27.5 FINE: 26.5 NONE - CENTRALIZER (yes (no) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): 29.5 TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: COARSE: 3 BAGS FINE: \$\frac{1}{3}\$ BAG BOTTOM OF SCREEN DEPTH (ft. bgs): - BOTTOM OF WELL DEPTH (ft. bgs): ______ BOTTOM OF FILTER PACK (ft. bgs): 39.7
 TYPE AND AMOUNT OF BACKFILL: 0.3 FT - NATURAL CAVE IN 39.7 TOTAL DEPTH OF BOREHOLE: 40.0 FT ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 50 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 14, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

PREPARED BY MEREN JOSO OF ZZI



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG BMW-1S

V Associates							
PROJECT NAME: AMEREN CCR GW	/ MONITORING	PROJECT NUMBER: 153-1406.0003B					
SITE NAME: SIOUX ENERGY CENT	ER	LOCATION: BMW-1S					
CLIENT: AMEREN MISSOURI		SURFACE ELEVATION	ON: 426.0 FT MSL				
GEOLOGIST: J. INGRAM	NORTHING: 1121709		EASTING: 876755.6				
DRILLER: J. DRABEK	STATIC WATER LEV	EL: 7.35 FT BTOC	COMPLETION DATE: 12/8/2015				
DRILLING COMPANY: CASCADE		DRILLING METHODS: SONIC					
LOCK.	CAP						
	TOF	OF CASING ELEVATION:	427.77 FT MSL				
STICK UP: 1.8 FT	P	ROTECTIVE CASING (yes)	no): 4" X 5' ALUMINUM				
STICK OF .	PE	A GRAVEL OR SAND					
1.4. A.	GRO	OUND SURFACE ELEVATION	N: 426.0 FT MSL				
A. A							
14. 4.1 12. 1	——— DIAI	METER OF RISER PIPE (in.)):				
	——— DIAI	METER OF BOREHOLE (in.)	6.0				
	CON	ICDETE SEAL DEDTIL (# b.	ns): 2.5				
00000 00000 900000 00000 900000 00000 900000 000000	COI	NCRETE SEAL DEPTH (ft. b	gs):				
900 000 000 000 000 000 000 000 000 000							
\$6563 \$6563	T) (D		LAR SEAL: NONE				
	TYP	E AND AMOUNT OF ANNU	LAR SEAL: NONE				
00000 00000 00000 00000	TOF	OF BENTONITE SEAL DEF	PTH (ft. bgs): 2.5				
			ONITE SEAL: 3 " BENTONITE CHIPS - 2 BAGS				
100 P 100 P	TOF	OF SAND PACK DEPTH (ff	t. bgs):COARSE: 12.5 FINE: 12.0				
	CEN	ITRALIZER (yes (no) - TY	PE:NONE				
			gs):				
	T)/D	AF OF CODEFN.	2" V 0 9! SCHEDHI E 40 DVC				
			2" X 9.8' SCHEDULE 40 PVC 0.010 IN				
		REEN SLOT SIZE (in.):	COARSE: #1 FINE: #0				
	SIZE	E OF SAND PACK:	COARSE: #1 FINE: #0 COARSE: 3.5 BAGS FINE: \(\frac{1}{3}\) BAG				
	AMC	DUNT OF SAND:	CONTROL: 0.0 Brose Tine. 3 Bros				
	ВОТ	TOM OF SCREEN DEPTH ((ft. bgs):				
	ВОТ	TOM OF WELL DEPTH (ft. b	ogs):				
			04.0				
TOTAL DEPTH OF BOREHOLE: 25.0 FT	BOT	TOM OF FILTER PACK (ft. I	bgs):				
ADDITIONAL NOTES: FT BGS = FEET BELC							
50 GALLONS OF H20 USED DURING DRILL							
MISSOURI EAST ZONE. VERTICAL DATUM: FT BTOC = FEET BELOW TOP OF CASING.			IATES, INC ON JANUARY 14, 2016.				
	C ID FILE DE LITTORITE DE						

CHECKED BY: J. INGRAM

DATE CHECKED: 4/20/2016



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG BMW-3S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0003B SITE NAME: SIOUX ENERGY CENTER LOCATION: BMW-3S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 424.1 FT MSL GEOLOGIST: J. INGRAM/M. GORE NORTHING: 1121792.9 EASTING: 875809.5 DRILLER: M. RODRIGUES STATIC WATER LEVEL: 8.65 FT BTOC COMPLETION DATE: 11/8/2016 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK - TOP OF CASING ELEVATION: 426.69 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: ___2.6 FT - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 424.1 FT MSL DIAMETER OF RISER PIPE (in.): DIAMETER OF BOREHOLE (in.): ___ - CONCRETE SEAL DEPTH (ft. bgs): 2.5 TYPE AND AMOUNT OF ANNULAR SEAL: HIGH SOLIDS BENTONITE TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 – TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 1 BUCKET - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 11.6 FINE: 10.8 - CENTRALIZER (yes (no) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): 14.0 TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC 0.010 IN SCREEN SLOT SIZE (in.): ___ SIZE OF SAND PACK: COARSE: #1 (20-30) FINE: #0 (30/65) AMOUNT OF SAND: COARSE: 4 BAGS FINE: ½ BAG - BOTTOM OF SCREEN DEPTH (ft. bgs): _____ - BOTTOM OF WELL DEPTH (ft. bgs): 24.2 BOTTOM OF FILTER PACK (ft. bgs):

 TYPE AND AMOUNT OF BACKFILL:

 NONE TOTAL DEPTH OF BOREHOLE: 24.2 FT ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 50 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON DECEMBER 8, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM

DATE CHECKED: 8/3/2017

PREPARED BY MEREN COUNTY

APPENDIX F WELL DEVELOPMENT FORMS



Remove Surge Wock

Proje	ct Ref:	Ameren G	W Monit	oring	-30 F		Project	No.: 153	-1406. [♂]	003
Loca	tion	LMV	V-1							
Monito	red By:	35		Date	12015		Time	1400	>	j
Well	Piezon	neter Dat								
Depth o	f Well (fron	(circle one) n top of PVC o			42.47		1111	feet		
		m top of PVC)	26.75		feet			
	of Casing		g		2			╡		
								inches		
Casing Volume					3.6.	4=2	0	cubic feet		176 . 1 G. 11
					VI			gallons		4 42 day 11mm
Deve	lopmer	nt / Purgi	ng Dis	charg	e Data		1.4			= 98 gal 470
Purging	Method				- (Vonterra	62			1
Start Pu	rging			Date	12/20/15 Time			1414		
Stop Pu	rging			Date				1550		1
Monitori	ng]	1-00	,	
Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (_S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
1/20 1		20	18.79	8.33	0.861	71000	6.00	-230.0	26.36	very cloudy
1	1435	60	18.92	8-33	0.815	71000	5.89	-227.3	27.85	Very Cloudy
-	1450	85	19.01	8-30	0.821	71000	5.93	- 254 0	27.96	very closely
-	1505	120	18.62	8-25	0.789	71000	6.62	-240.8	27.25	very flordy
1	1530	130	18.59	8.07	0.787	51-3	6-48	-153,8	26.80	cloudy
	1546	135	18-83	8.11	0.800	4.92	6.31	-210.8	27.12	clear
4	1550	140	18.98	8.10	0.801	5.92	6.24	-196.0	27.05	clear
						10° , 1 = 1		diam A		
				- 1					Vi.	
									113-	
	ad j		100.50							
									-	



Project	Ref: A	meren GV	/ Monito	ring			Project	No.: 153-	1406. 00	
Locati	on	LMW-	5							
Monitore	d By:	22		Date	12/23/1	ſ	Time	072	5	
Well P	iezom	eter Data	a		٦.					
		(circle one)						,		
Depth of V	Well (from	top of PVC or	ground)		27.04			feet		
Depth of V	Nater (fron	top of PVC	or ground)		42.70			feet		
Radius of	Casing				2			inches		-4
					- Common			feet		+ (Deal from day)
Casing Volume				6.3.3	= 19		cubic feet		1201	
								gallons		+50gal from don't
Develo	opmen	t / Purgi	ng Dis	charge	e Data					The second - 61 gain
ourging M	lethod				Water	ra			EW.	
Start Purg	ing			Date	12/23/15		Time	774	t	and the second
Stop Purg	ing			Date	12/22/15		Time	1150		
Monitoring							•			to the second
Date	Time	Volume Discharge (gals)	Temp	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
וונב/גו	0813	30	16.50	8.86	1.102	71000	7.64	-206.4	27.42	muddy,
4 - 17	6835	60	16.50	8.97	1.155	71000	7.75	-256.0	27.48	muddy
	5885	65	_			_		-		pump broke dewn
	1057	65	10.01/	-		1	_	-		resume purge
	1101	70	15.94	8.37	1.183	71000	20.90	-235.3		muddy
	1120	85	16.36	7.76	1.187	30.0	19.15	-135.4	27.15	stratt cloudy
	1142	90	16.46	7.96	1.192	9.68	10.26	- 131.1	27.13	cleny
	1147	93	16.54		1.206	7.01	10-23	-133-2	27.07	clear

		- X								
			19.0				-			

						1891		<u> </u>		
	46.6									

block



Project Ref: Ameren GW Monitoring

	Monitore	u by.	725		Date	1160	lle	Time	04	50 074	D .
	Well F	Piezom	eter Data	9							
			(circle one)					,			
	Depth of	Well (from	top of PVC or	ground)		84	,21		feet		
	Depth of	Water (from	n top of PVC	or ground)		3.	HI	447	feet		
	Radius of	Casing					(e "		linches		
					1 8		_		feet		
	Casing V	olume									2124
							7.0	G	gallons	7.0	6+3=21.24
											+58
	Devel	opmen	t / Purgi	ng Dis	charge	Data		je P			100
	Purging M	Method				(N 41	tera	}			71 24
	Start Purging Date						715	Time	74	0	70.24
	Stop Pur				Date	101	128/18	Time	134		
	Otop i dit	amg			Date	(9)	100113	Time	(3-		
	Monitorin	g									
ſ				T							
	Date	Time	Volume Discharge	Temp	pН	Spec.Cond.	Turbidity	Dissolved Oxygen	Redox Potential	WL (ft	Appearance of Water and Comme
		3	(gals)	(° <u>C</u>)	Pit	(MS/cm)	(NTU)	(mg/L)	(+/- mV)	BTOC)	Appearance of Water and Comme
	1/28	800	30	14.01	650	1.037	71000	2.44	204.5	8.84	Recor + mulla
	1	320	60	12.93	7.42	1.036	71000	2.50	239.2	8.87	(1 11
Bu		340	90	12.54	8.32	1.028	71000	2.49	233.0	8.89	n /1
0 11		900	120	13.19	8.34	1.023	71000	3.33	233.9	2.90	1) 4
Ha.		970	150	13.45		1:037	314	3.24	229.0	8.91	(levi)
m		940	100	13.49	851	1.033	258	3.31	230.0	8.92	(lenge)
93		100	190	13.51	7.41	1.234	583	3.23	231.3	295	Lewflow
	0.00	1026	195	13. 37	7.41	1.023	291	3.86	-37.3	8.35	11
	-	1040	205	12.47	7.01	1.134	619	2.11	-5/3	8.85	in the contract of the contrac
	-	1100	215	12.39	6.81	1.03(512	2.13	-54.4	8.85	Siste Clary
		1120	225	13.75	7.12	5501	71000	2.17	-58.1	8.85	plus back at Bol
		1140	245	14.6	730	1.033	7120	2.7.8	-113.8	8135	5 = 0.0 = 1 1:
		1200	245	14,24	7:13	1.034	71000	2.93	-102.4	8.45	- STOP FOR PUT BU
An	-	1230	275	14.24	7. 33	1.036	134	3.14	-137.4	8,65	-Clewin
,00		1250	285	14,70	7.87	1.034	0611	1 20	-146.8	8.65	- Clew
		1300	The state of the s	14.47		1.035	324	1.37	-146.7	8.45	- Cley
		1310	295	14.69	7.50	1.034	29.3	1.23	-147.3	8.46	
	1100	1320	300	14.75	7.52	1034	22.7	1.20	- (37.9	3.65	
10.		1330	305	147	7.44	103M (.035	15.5	1,23	1387	B. 45	Ole
		1340	310	170/07	7.90	(,033	9.97	(100	-1343	51.42	Bine
			12 5	-							
. 0		1						T Bloo		e manie e da	
						- 6	do	199			
			11 - 12 14				317 -3130			Type	
							-				
											1

Project No.: 153-1406.



	Ref: A	meren GV	/ Monito	oring			Project	No.: 153-	1406. 6	003
ocati	ion	LMh	1-4:	5						
onitore	ed By:	<u>122</u>		Date	1271	14	Time	1/14/1	6	j
Vell F	Piezom	eter Data	1	ē						
epth of \	Well (from	(circle one) top of PVC or	ground)		27.2			feet		
epth of Water (from top of PVC or ground)					5-50			feet		
adius of Casing					(e	4.00		inches	2	7. (3 = 23.)
av	43	Marylan Brank	74.	10				feet	11	7. (2 - 25.)
asing Vo	olume				78	7	_	cubic feet		450
				W.	36114	7		gallons		
evel	opmen	t / Purgi	ng Dis	charge	e Data	4		in		73.15010
urging M	Method	\	- MA		Wate	ra				
art Purg	ging		1	Date	1/27	2/14	Time	1310		
op Purg	ging		168	Date	1/28,	16	Time	163	0	
onitoring							- 64	2000		
Unitolini	9				-1 -10: A -10	/4,78		1		
Date	Time	Volume Discharge	Temp	рН	Spec.Cond.	Turbidity	Dissolved Oxygen	Redox	WL (ft	Annana - 618/4
127	Time	(gals)	(°Z)	pit	(MS/cm)	(NTU)	(mg/L)	Potential (+/- mV)	втос)	Appearance of Water and Comments
BI	1340	4005	13.92	7.76	0.474	76000	3.54	~ 73.8	8.11	Brown - MULL
1	1400	10	14.23	7.61	0.854	71000	5,13	-14.4	8.11	11 11
	1440	30	14,17	7.47	0.969	71000	2.64	14.4	8.13	11 11 3
75	1500	60		7.43	0.145	71000	7.26	14.4	8,74	- CEE BACK- ISSUE
	1619	90	14.24		0.977	1000	7.84	43.4	8.75	13 Sulye Block
1	11/1/1/1			100		71000	1.14			
	1700	136	14.112	750	0.982			482	2,74	· Very Molly / SZUT
	1700	136	14.29	7.41	0.782	71100	0.88	70.4	\$174 \$17.80	very muly 15 zers
12/2	1700									Se BOILT
(22)	1700	185		7,41		71100	0.88	70.4	A7.80	SEBUILT STAT Wahrla pun
126	1700 1400 1445 1500	136	13.48	7.41 6.72, 7.83	1.094	71300	0.88	70.4		SEBUILT STAT Wahrla pur
126	1700 1400 1445 1500	136 180 150 340	13.76	7.41 7.83 2.02	1.094	71300 71300 71300 71300	0.88	70.4 -41,8 -18.1 -5.1	7.98 7.98 7.98	Start water par muly STANDY.
125	1700 (400 (445 1500 (530)	136 150 213 150 310 370	13.76	7.41 7.03 201	1.044 1.028 1.031 Lo33	71300 71300 71300 71300 71300	0.88	70.4 -41,0 -18.1 -5.1	7.80 7.98 7.98 7.99	SE BOILT STAIT WENTER PUR MUNICIPALITY
125	1700 (400 (445 1500 (530)	136 180 150 340	13.76	7.41 7.03 201	1.094	71300 71300 71300 71300	0.88	70.4 -41,8 -18.1 -5.1	7.98 7.98 7.98	SE BOILT STAT Watsla par mudi, ISANOV, u " 4 STOP
125	1700 (400 (445 1500 (530)	136 150 213 150 310 370	13.76	7.41 7.03 201	1.044 1.028 1.031 Lo33	71300 71300 71300 71300 71300	0.88	70.4 -41,0 -18.1 -5.1	7.80 7.98 7.98 7.99	SE BOILT STAT Watsla par mudi, ISANOV, u " 4 STOP
(2)	1700 (400 (445 1500 (530)	136 150 213 150 310 370	13.76	7.41 7.03 201	1.044 1.028 1.031 Lo33	71300 71300 71300 71300 71300	0.88	70.4 -41,0 -18.1 -5.1	7.80 7.98 7.98 7.99	SE BOILT STAT Watsla par mudi, ISANOV, u " 4 STOP
125	1700 (400 (445 1500 (530)	136 150 213 150 310 370	13.76	7.41 7.03 201	1.044 1.028 1.031 Lo33	71300 71300 71300 71300 71300	0.88	70.4 -41,0 -18.1 -5.1	7.80 7.98 7.98 7.99	SE BOILT STAT Watsla par mudi, ISANOV, u " 4 STOP
125	1700 (445) (445) (530) (470) (470)	136 150 213 150 310 370	13.76	7.41 7.03 201	1.044 1.028 1.031 Lo33	71300 71300 71300 71300 71300	0.88	70.4 -41,0 -18.1 -5.1	7.80 7.98 7.98 7.99	SE BOILT STAT Watsla par mudi, ISANOV, u " 4 STOP
125 125	1700 (445) (445) (530) (470) (470)	136 150 213 150 310 370	13.76	7.41 7.03 201	1.044 1.028 1.031 Lo33	71300 71300 71300 71300 71300	0.88	70.4 -41,0 -18.1 -5.1	7.80 7.98 7.98 7.99	SE BOILT STAT Watsla par mudi, ISANOV, u " 4 STOP
(2)	1700 (445) (445) (530) (470) (470)	136 150 213 150 310 370	13.76	7.41 7.03 201	1.044 1.028 1.031 Lo33	71300 71300 71300 71300 71300	0.88	70.4 -41,0 -18.1 -5.1	7.80 7.98 7.98 7.99	SE BOILT STAT Watsla par mudi, ISANOV, u " 4 STOP



Golder Associates WELL DEVELOPMENT/PURGING FORM

			/ Monito	oring	Project No.: 153-1406.							
Locati	ion	LMV	V-5									
Monitore	ed By:	33		Date	12 22 1	5	Time	085	4			
Well F	Piezom	eter Data	a									
Depth of \	Well (from	(circle one) top of PVC or	ground)		47.46			feet				
Depth of \	Water (fro	n top of PVC	or ground)		27,92			feet				
Radius of	Casing				12			inches				
								feet		The state of the s		
Casing Vo	olume				7 .3 =	21		Cubic feet	+	-100 gal H20 used in 8		
					7 1		gallons	,	-100 gal H20 used in 8			
Devel	opmen	t / Purgii	ng Dis	charge	e Data					121 911 1120		
Purging N	lethod				Wat	cura						
Start Purg	ging			Date	12/22/1	5	Time	086	4			
Stop Purg	ina			Date	18/22/15		Time	1418				
	,9			2410	1141-110		1 11110	1,1,0				
Monitoring	9											
			THE RESERVE			THE RESERVE OF THE PARTY OF THE	Section 1997	THE RESERVE OF THE PERSON NAMED IN				
Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments		
		Discharge		8.14			Oxygen	Potential		Appearance of Water and Comments		
		Discharge (gals)	(°)		(S/cm)	(NTU)	Oxygen (mg/L)	Potential (+/- mV)	8.49 28.30			
	1003	Discharge (gals)	(°_) 15.50 14.10 14.74	8.14	(_S/cm) 1.075 1.063	71000 71000 255	Oxygen (mg/L) 5.41 5.44 5.14	Potential (+/- mV)	8.49 28.30 21.91	m-ddy		
	1003 1023 1030	Discharge (gals) 100 130 135 145	15.50 14.10 14.74 14.96	8.14 8.10 8.01 3.97	(_S/cm) 1.075 1.075 1.077 1.052	(NTU) 71000 71000 255 291	Oxygen (mg/L) 5.91 5.14 5.19 7.11	Potential (+/- mV) -65.5 -60.9 -70.6 -58.4	8.49 28.30 21.91 21.86	muddy muddy Very cloudy Very cloudy		
	1003 1023 1030 1040	Discharge (gals) 100 130 135 145 150	15.50 15.10 14.74 14.96	8.14 8.10 8.01 3.97 7.95	(_S/cm) 1.075 1.075 1.077 1.052 1.065	(NTU) 71000 71000 255 291 465	Oxygen (mg/L) 5.91 5.91 5.91 5.11 6.15	Potential (+/- mV) - 65.5 - 60.9 - 70.6 - 58.4 - 71.5	8.49 28.30 21.91 21.86 23.45	muddy muddy Very cloudy Very cloudy Muddy		
	1003 1023 1030 1040 1050	Discharge (gals) / 00 13 v //3 5 14 5 15 v 153	15.50 14.10 14.74 14.10 14.10	8.14 8.10 8.01 7.93 7.95 7.18	(_S/cm) 1.075 1.063 1.047 1.052 1.065	71000 71000 71000 255 291 465 164	Oxygen (mg/L) 5.91 5.91 5.99 7.11 6.15	Potential (+/- mV) - \$5.5 - 60.9 - 70.6 - 58.4 - 71.5 - 28.5	88.49 28.30 27.91 27.86 27.95 24.89	muddy muddy Very cloudy Very cloudy Muddy Cloudy		
Date	1003 1023 1030 1040 1050 1110 1125	Discharge (gals)	15.50 14.10 14.74 14.10 14.10 14.93	8.14 8.10 8.01 7.97 7.95 7.78	(_S/cm) 1.075 1.063 1.047 1.052 1.065 1.037 1.084	71000 71000 255 291 465 264 265	Oxygen (mg/L) 5.91 5.91 5.14 5.17 6.15 7.21 7.40	Potential (+/- mV) - \$5.5 - 60.9 - 70.6 - 58.9 - 11.5 - 28.5 - 40.0	38.49 28.30 27.91 27.86 27.95 24.89 24.73	muddy word cloudy very cloudy very cloudy Cloudy Cloudy		
	1003 1023 1030 1040 1050 1110 1125	Discharge (gals) / 00 13 v /3 5 14 5 15 0 153 155	(°_) 15.50 16.10 14.74 14.96 14.10 14.98 14.93	8.14 8.10 8.01 7.73 7.75 7.78 7.86	(_S/cm) 1.075 1.063 1.047 1.052 1.065 1.039 1.084	(NTU) 71000 71000 255 291 465 164 365	Oxygen (mg/L) 5.91 5.91 5.11 6.15 7.21 7.40 7.08	Potential (+/- mV) - 45.5 - 60.1 - 70.6 - 58.4 - 71.5 - 28.5 - 40.0 - 56.2	870C) 28.49 28.30 27.86 27.86 27.45 24.69 24.73 27.90	muddy word cloudy very cloudy very cloudy cloudy cloudy cloudy		
	1003 1023 1030 1040 1050 1110 1125 1140	Discharge (gals) / 00 13 v /3 5 14 5 15 0 153 155 156 /5 %	15.50 14.10 14.74 14.10 14.08 14.93 14.93 14.94	8.14 8.10 8.01 7.93 7.18 7.86 7.86 7.86	(_S/cm) 1.075 1.063 1.047 1.052 1.065 1.039 1.084 1.079	(NTU) 71000 71000 255 291 465 264 365 132 61.5	Oxygen (mg/L) 5.91 5.91 5.11 6.15 7.21 7.40 7.08	Potential (+/- mV) - 45-5 - 60.9 - 70.6 - 58.4 - 71.5 - 28.5 - 40.0 - 56.2 - 59-3	870C) 28.49 28.30 27.86 27.86 27.45 24.89 27.43 27.90 17.91	muddy very cloudy very cloudy very cloudy cloudy cloudy cloudy cloudy stylycloudy		
	1003 1023 1030 1040 1050 1110 1125 1140 1155	Discharge (gals) / 50 13 v /3 5 14 5 15 0 153 155 156 /5 %	15.50 16.10 16.74 14.10 14.10 14.10 14.95 14.95 14.96 14.74 15.07	8.14 8.10 8.01 7.97 7.18 7.86 7.86 7.86 7.87	(_S/cm) 1.075 1.063 1.047 1.052 1.065 1.039 1.084 1.079 1.076	(NTU) 7,000 7,000 255 291 465 164 365 132 64-5	Oxygen (mg/L) 5.91 5.91 5.11 5.11 6.15 7.21 7.40 7.08 6.82	Potential (+/- mV) -\$5.5 -\$6.7 -\$6.7 -\$8.4 -\$1.5 -\$6.5 -\$6.2 -\$9.3 -\$5.2	870C) 28.49 28.30 27.86 27.86 27.45 27.45 27.40 27.40 27.40	muddy very cloudy very cloudy very cloudy very cloudy cloudy cloudy cloudy Significancy		
	1003 1023 1030 1040 1050 1110 11125 1140 1155 1210	Discharge (gals) / O O 13 v /3 S 14 S 15 0 153 155 156 /5 % 160 161	15.50 16.10 16.34 14.10 14.10 14.13 14.95 14.95 14.94 15.07 15.04	8.14 8.10 8.01 1.97 1.95 7.86 7.86 7.89 7.87	(_S/cm) 1.075 1.063 1.047 1.052 1.065 1.039 1.079 1.079 1.078 1.078	(NTU) 71000 71000 255 291 465 264 265 132 64-5 40.0	Oxygen (mg/L) 5.91 5.91 5.11 5.11 6.15 7.21 7.40 7.08 6.79 6.82	Potential (+/- mV) - \$5.5 - \$6.9 - 70.6 - 58.4 - 71.5 - 28.5 - 40.0 - 56.2 - 51.3 - 58.6 - 62.3	870C) 28.49 28.30 27.86 27.86 27.45 27.49 27.73 27.90 17.91 27.85	muddy very cloudy very cloudy very cloudy		
	1003 1023 1030 1040 1050 1110 1125 1140 1155	Discharge (gals) / 50 13 v /3 5 14 5 15 0 153 155 156 /5 %	15.50 16.10 16.74 14.10 14.10 14.10 14.95 14.95 14.96 14.74 15.07	8.14 8.10 8.01 7.97 7.18 7.86 7.86 7.86 7.87	(_S/cm) 1.075 1.063 1.047 1.052 1.065 1.039 1.084 1.079 1.076	(NTU) 7,000 7,000 255 291 465 164 365 132 61.5 40.0 40.0	Oxygen (mg/L) 5.91 5.91 5.11 6.15 7.21 7.40 7.08 6.93 6.48	Potential (+/- mV) - \$5.5 - \$6.9 - 70.6 - 58.4 - 71.5 - 28.5 - 40.0 - 56.2 - 59.3 - 52.6 - 62.3 - 61.9	8.49 28.30 27.86 27.86 27.86 27.89 27.89 27.90 27.90 27.90	muddy very cloudy very cloudy very cloudy Clear		
	1003 1023 1030 1040 1050 1110 1125 1140 1155 1210	Discharge (gals) / O O 13 v /3 S 14 S /5 O 153 155 156 /5 % 160 161	15.50 16.10 14.74 14.10 14.10 14.95 14.95 14.96 14.74 15.07 15.04 15.27	8.14 8.10 8.01 1.97 7.18 7.18 7.18 7.18 7.18 7.18 7.18 7.1	(_S/cm) 1.075 1.063 1.047 1.052 1.065 1.039 1.079 1.079 1.076 1.078	(NTU) 71000 71000 255 291 465 264 265 132 64-5 40.0	Oxygen (mg/L) 5.91 5.91 5.11 5.11 6.15 7.21 7.40 7.98 6.93 6.48 6.57	Potential (+/- mV) - \$5.5 - \$6.9 - 70.6 - 58.4 - 71.5 - 28.5 - 40.0 - 56.2 - 51.3 - 58.6 - 62.3	8.49 28.30 27.86 27.86 27.86 27.89 27.90 27.90 27.90 27.90 27.90	muldy very cloudy very cloudy very cloudy very cloudy cloudy cloudy cloudy cloudy cloudy Clear Clear Clear Clear		
	1003 1023 1030 1040 1050 1110 11125 1140 1155 1210 1225 1235	Discharge (gals) / O O 13 v /3 S 14 S 15 0 153 155 156 /5 % 160 161	15.50 14.10 14.74 14.90 14.10 14.93 14.94 15.07 15.04 15.04 15.27 14.96	8.14 8.10 8.01 1.97 7.18 7.18 7.18 7.18 7.18 7.18 7.18 7.1	(_S/cm) 1.075 1.063 1.047 1.052 1.065 1.039 1.079 1.079 1.076 1.078 1.078	(NTU) 7,000 7,000 2,55 2,91 465 2,64 3,65 13,2 6,4.5 40.0 41.0 45.1 3,9.6	Oxygen (mg/L) 5.91 5.91 5.11 6.15 7.21 7.40 7.08 6.93 6.48	Potential (+/- mV) - \$5.5 - \$6.9 - 70.6 - 58.4 - 71.5 - 40.0 - 56.2 - 59.3 - 52.6 - 62.3 - 61.9 - 60.0	8.49 28.30 27.86 27.86 27.86 27.89 27.90 27.90 27.90 27.90 27.90 27.90	muldy very cloudy very cloudy very cloudy very cloudy cloudy cloudy cloudy cloudy cloudy Clear Clear Clear Clear Clear Clear Clear		
	1003 1023 1030 1040 1050 1110 11125 1140 1155 1210 1225 1235 1230 1305	Discharge (gals) / O O 13 v / 3 S 14 S 15 0 153 155 156 / 5 % 160 161 162	15.50 16.10 14.74 14.10 14.10 14.95 14.96 14.96 14.96 14.96 15.07 15.04 15.03	8.14 8.10 8.01 7.95 7.86 7.86 7.87 7.87 7.87 7.85 7.86 7.87	(_S/cm) 1.075 1.063 1.047 1.052 1.065 1.039 1.079 1.079 1.078 1.078 1.078 1.079 1.079	(NTU) 7,000 7,000 2,55 2,91 465 2,64 3,65 13,2 6,7,5 40.0 45,1 3,1,6 32,6	Oxygen (mg/L) 5.91 5.91 5.11 6.15 7.21 7.40 7.08 6.93 6.48 6.57 7.18	Potential (+/- mV) - \$5.5 - \$6.7 - 70.6 - 58.4 - 71.5 - 28.5 - 40.0 - 56.2 - 59.3 - 52.6 - 62.3 - 61.9	8.49 28.30 27.86 27.86 27.86 27.89 27.90 27.90 27.90 27.90 27.90	muldy very cloudy very cloudy very cloudy very cloudy cloudy cloudy cloudy cloudy cloudy Clear Clear Clear Clear		
	1003 1023 1030 1040 1050 1110 11125 1140 1155 1210 1225 1235 1235 1230	Discharge (gals) / O O 13 v /3 S 14 S 15 0 153 155 156 /58 160 161 162 164 168	15.50 14.10 14.74 14.90 14.90 14.93 14.96 14.96 14.96 15.03 14.91	8.14 8.10 8.01 7.95 7.36 7.36 7.86 7.87 7.87 7.85 7.86 7.84 7.85	(_S/cm) 1.075 1.075 1.052 1.052 1.065 1.039 1.079 1.079 1.074 1.074 1.074 1.074 1.074 1.077	(NTU) 7,000 7,000 2,55 2,91 465 2,64 3,65 40.0 45.1 3,9.6 32.6 28.1	Oxygen (mg/L) 5.91 5.91 5.91 5.91 6.15 7.21 7.40 7.08 6.92 6.48 6.57 7.19 7.90	Potential (+/- mV) - \$5.5 - \$6.9 - 70.6 - 58.4 - 71.5 - 28.5 - 40.0 - 56.2 - 59.3 - 52.6 - 62.3 - 61.9 - 60.0 - 60.0	870C) 28.49 28.30 21.91 21.86 21.95 21.90 11.91 21.86 21.96 21.96 21.96	muldy very cloudy very cloudy very cloudy very cloudy cloudy cloudy cloudy cloudy cloudy clear		
	1003 1023 1030 1040 1050 1110 11125 1140 1155 1210 1225 1235 1235 1320	Discharge (gals) / O O 13 v / 3 S 14 S 15 0 153 155 156 / 5 % 160 161 162 164 168 140	15.50 14.10 14.10 14.10 14.10 14.95 14.95 14.96 15.03 14.91 15.03 14.92 15.03	8.14 8.10 8.01 7.95 7.36 7.86 7.87 7.87 7.85 7.86 7.87 7.85 7.85 7.84 7.85 7.84	(_S/cm) 1.075 1.075 1.052 1.052 1.065 1.039 1.079 1.074 1.074 1.074 1.074 1.075 1.078 1.081 1.081	(NTU) 7,000 7,000 2,55 2,91 465 2,64 3,65 40.0 45.1 3,9.6 3,6 28.1 36.2	Oxygen (mg/L) 5.91 5.91 5.91 5.91 6.15 7.21 7.40 7.08 6.93 6.48 6.57 7.19 7.90 7.10	Potential (+/- mV) -\$5.5 -\$6.9 -\$8.4 -\$1.5 -\$6.2 -\$1.3 -\$6.2 -\$1.3 -\$6.9	870C) 38.49 28.30 27.86 27.86 27.89 27.90 27.90 27.90 27.90 27.90 27.90 27.90 27.90	muddy very cloudy very cloudy very cloudy very cloudy cloudy cloudy cloudy cloudy cloudy cloudy Clear		
	1003 1023 1030 1040 1050 1110 11125 1140 1155 1210 1225 1235 1235 1320 1335	Discharge (gals) / 00 13 v /3 S 14 S 15 0 153 155 156 /58 160 161 162 164 163 170 175	15.50 14.10 14.10 14.10 14.10 14.95 14.95 14.96 15.03 14.91 15.03 14.92 15.03	8.14 8.10 8.01 7.95 7.86 7.86 7.87 7.87 7.87 7.85 7.84 7.85 7.84 7.85 7.84 7.85	(_S/cm) 1.075 1.075 1.052 1.052 1.065 1.039 1.079 1.074 1.074 1.074 1.074 1.075 1.081 1.081 1.069	(NTU) 7,000 7,000 255 291 465 132 61.5 40.0 40.0 45.1 39.6 32.6 28.1 36.2	Oxygen (mg/L) 5.91 5.91 5.91 5.91 6.15 7.21 7.40 7.08 6.93 6.48 6.57 7.17 7.10 7.10 7.21	Potential (+/- mV) -\$5.5 -\$6.9 -\$1.5	38.49 28.30 27.86 27.86 27.86 27.89 27.90 27.90 27.90 27.90 27.90 27.90 27.90 27.90 27.90	muddy Very cloudy Very cloudy Very cloudy Very cloudy Cloudy Cloudy Cloudy Cloudy Cloudy Clear		

Renove Surge Block



Golder Associates WELL DEVELOPMENT/PURGING FORM

				No.: 153-1406.	
Location LMW-6	5				
Monitored By: 「	Date	1/12/16	Time	0800	Maria e de Santa Tille
Well Piezometer Data					
Depth of Well (from top of PVC or ground)		42.13		feet	
Depth of Water (from top of PVC or ground)		21,70		feet	
Radius of Casing		2		inches	
				feet	- Latlin
Casing Volume		713=21.3		cubic feet	+75 gal from arrive
				gallons	
Development / Purging Disc	harg	e Data			+75 gal from drilling =97 gal total
Purging Method		Watern	1.03		
Start Purging	Date	1/12/1/2	Time	0835	
Stop Purging	Date	1/12/16	Time	-frest	16/0
Monitoring					

Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
12/16	0910		11.14	6.75	1.696	71000	1,00	43.0	22.0	modely
	0930	80	11.62	7.28	1.725	7/000	5.01	23.0	21,90	muddy
1 (N1E)	0945	90	13.27	7.35	1.746	71000	4.89	21.8	21.42	med ster
	0950	96	4			-	-			Remove Surye blow
	1000	100	13.04	7.50	1,756	147	4.74	14.1	21.95	cloudy , low flow
	1010	120	12.52	7.32	1.754	149	4.70	Z0.7	21.93	cloudy
	1052	150	12.90	7.76	1.752	99.0	4.44	9.8	28.95	cloudy
	1040	146	12.62	7.35	1.751	86.5	4.41	14.5	1100	Cloudy
	1100	150	12.36	4-29	1.731	114.0	4.31	74.3	21.91	Clardy
	1120	156	12.16	7.27	1.727	123.0	4.51	1.55	21.92	e lendy
	1140	163	12.29	7.35	1.722	125	4.78	17.9	21.90	clady
	1200		12.87	7.34	1.741	128	5.01	20.7	21.94	cloudy
	1220		12.16	1.21	1.731	132	5.05	14-2	21.92	cloudy
	1240	186	12-18	7.29	1.707	70.7	5.31	12.9	21.90	cloudy
	1300		12.31	7.25	1-739	48.9	4.59	13-2	21.86	clear
	1315	195	12.36		1.728	42.3	4.23	5.0	21,90	clear
	1330	200	12.00	7.34	1.732	36.6	5,00	10.3	71.91	clear
	1350	207	12.12	7.29	1.717	34.6	4.66	1.9	21.89	Clear
	1405	711	12.04	7.32	1.714	34.4	4.82	1.8	21.95	clear
	1425	216	11-57	7.25	1.701	28.1	5.16	-4-3	71.90	Clear
	1440	220	12.25	7.29	1,719	33.9	5.10	-5.9	21.90	Clear
		236	11.71	7.23	1.698	39.8	4,91	-5-3	21.88	dow
	1520	739	11.76	720	1-658	36.3	5.51	27.6	21.70	clear
	1548	250	11.92	-	1.672	17.3	7.71	20000	71.87	Clear
	1555		13-18	7.15	1.755	5.94	5.96	26.2	21.85	CLEAT
	1605	270	13.72	7.35	1.760	5.13	5.71	19.0	22.00	alegr



Project	Ref: A	meren GW	/ Monito	oring	. Wite		Project I	No.: 153-	1406. 80	•3
Locati	on	LMW	-75							
Monitore	d By:	35		Date	1/13/16		Time	1066		- 1.54/) - 204/2
Well P	iezom	eter Data	ı							
Depth of V	Vell (from	(circle one) top of PVC or	around)		≈ 42.2			feet		
		n top of PVC			70.7	2]feet		
Radius of			3,		2		linches			
					N 1 -			feet		
asing Volume					7.11 . 3 =	- IV-SIN-7-	cubic feet gallons		+ 75 gal He o from	
Develo	opmen	t / Purgir	ng Dis	charge	e Data					
ourging M	lethod				Water	4				97 gal botal
Start Purg	ing			Date	1/13/14		Time	1008		0
Stop Purg	ing			Date	1/13/16		Time	1135		
/lonitoring										
Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (_S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
1316	1100	75	14.13	7.51	1.254	8.74	6.46	22 4	20.70	clear
	1110	85	14.56	800	1.263	9.21	6.58	-14.8	20.69	cler
	1120	160	14.60	8.13	1.263	7.85	7.22	-25.5	70.60	clear, fow flow
,										
								,		
			l				1			



Project	Ref: A	meren GV	/ Monito	oring			Project N	No.: 153-	1406. O	643
Locat	ion	LMU	1-8:	5						
Monitore	ed By:	JS		Date	1/13/16		Time	1145		
Well F	Piezom	eter Data	a							
		(circle one)								
Depth of	Well (from	top of PVC or	ground)		47.20			feet		
Depth of	Water (fro	m top of PVC	or ground)		23.24	TELF		feet		
Radius of	Casing				2			inches		
					AL -			feet		
Casing V	olume				7.2.3	= 23		cubic feet gallons		+100 gal Hzo from
Devel	opmer	nt / Purgi	ng Dis	charge	e Data		(A) (S			+100 gal Hzo from
Purging N	/lethod			15.0	Wa terma			No. 14		
Start Purg	ging			Date	1/13/16] Time	1217		
Stop Purg				Date	1/13/16		Time	1630		
Otop i dig	anig			Date	1113/16		1 mie	1630		
Monitorin	g									
Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
1/13/11	1245	25	15.03	8.30	1.284	7.23	7.51	-38.1	23,51	clear
	1300	45	16.04	8.26	1.318	438	6-11	-47.8	23.42	Cloudy
July Climit	1320	62	16.35	8.19	1-311	236	6.70	-44.3	23.45	Cloudh
	1340	80	16.37	8.14	1.316	71000	5.72	-51.1	23.36	yery cloudy
	1355	115	-		-	_			1-	Remove Kuige Block *
	1400	135	16.13	8.12	1.312	108	6.11	-49.5	23.50	cloudy
	1415	170	16.27	8 09	1.311	71.6	7.83	-55.2	-	cloudy
	1425	175	16.16	8.16	1.308	286	5.69	-56.0		Elear, for flow
-	1435	180	15.92	8.12	1.298	20.8	6.77	- 47-3	25.30	clear
	1445	186	16.05	8.10	1.296	14.7	6.82	47.2	23.24	Clear
_	1455	189	15.84	8.09	1.289	15.9	7.52	-46.0	73.37	clear
	1515	191	15.84	8.11	1-296	16-1	7.97	-47.0	23.37	clear
—	1525	195	15.91	8-12	1-296	16.0	8.08	-48.9	23.35	cleav
-	1535	196	16.12	8-11	1.302	14.6	8.30	-46.3	23.29	Clear
	1545	198	15.81	8.11	1.292	19.1	8.56	-49.0	25.31	clear
	1555	700	15.74	8.09	1.289	16.3	8.04	-49.5	23.30	Cleav
	1605	202	15.74	9.09	1.289	12.8	8.16	-48.5		clear
	1615	205	15.52	6.07	1.782	11.5	8-39	-45.2		clear
	1625	208	15.57	8.07	1.284	8.45	8.22	-45.5	23.70	Near
			- '				-0			
		1		T						



Depth of W	d By:	LM'	W-9.	<						
Nell P i		355)						mary little in the
Depth of W	iezom			Date	1/14/1	ما	Time	075	0	
	ICZUIII	eter Data	a							
enth of M	Vell (from	(circle one) top of PVC or	ground)		41.61			feet		
chai oi A	Vater (fror	n top of PVC	or ground)		23.59			feet		
Radius of (Casing				2			inches		
					<u>`</u>			feet		
Casing Vol	lume				6.4 3	- 20.	-	cubic feet		
					. • •	<u> </u>		gallons		
Develo	pmen	t / Purgii	ng Disc	charge	Data					
Purging Me					Water	150				+50 gal Hz O from
Start Purgi	ing			Date	1/11/1/16		Time	075	7	
Stop Purgi	ng			Date	1/14/16		Time	1117		+50 gal Hzo from
					11111				1	0-0-2
Monitoring									las, here	E-12 A Lander
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
114/16	0904	110	_	_	-	1=			-	Pienere surge block
' '	1007	150	16.09	7.66	1.426	23.0	7.01	-8.0	24.00	Clear
	IDIH	155	17.64	7.75	1.459	38.0	5.42	-22.5		clear, for flow
	022	157	17.18	7.75	1.447	41.9	5.67	-26.5	23.92	clear
	040	161	17.35	7.76	1.443	32-4	6.78	-25.6	23.86	clear
	050	163	11, 24	779	1.431	25.1	6-41	-26.3	73.79	Clear
	1100	165	16.54	779	1,473	18.9	6.53	-24.4		clear
	1110	166	16.36	7.75	1418	15.9	6.38	-74.4	73.76	Clear
	115	168	16.33	7.72	1.419	8.68	6.52	-23.6	23.77	clear
		-								
										182H2 W S
						1				
				67 1	L Mark	75				
						THE !				



_ocat	iọn	KA	14-	15						
/lonitore	ed By:	7	57	Date	1/22/	16	Time	08 40) -	
Well F	Piezom	eter Data	4							0.143
	1020111	(circle one)	"			,				
epth of	Well (from	top of PVC or	ground)	55.1	1 25.9	515	A	feet	1	1 1 1
Depth of V	Water (fron	n top of PVC	or ground)	V	7.3	5000	10-	feet & TJ	R	374.11
Radius of			W.	00	2.0			4		
	Odomy			1 1	4.0			imphes	6	
asing Vo	nlume				6.5x		14.5	cubic feet	-	
	orun, no				4	- 30	-	gallons	6	,5 totalsullas
				-					4,	20.00
Devel	opmen	t / Purgir	ng Disc	charge	Data					
urging N	1ethod				We	tra.				
Start Purg	ing			Date	10/21	114	Time	082		
Stop Purg	ing	李		Date	1/2-2/	6	Time	154	14	
1200			1	1	0					
/lonitoring	9		Asic	- 19			- 1 (Pales	- 2		STARTED UNS modify Appearance of Water and Comments
	S A S	Volume		9		B 36	Dissolved	Redox		THE REPORT OF THE PARTY OF
Date	Time	Discharge	Temp	pH	Spec.Cond.	Turbidity	Oxygen	Potential	WL (ft	Appearance of Water and Comments
		(gals)	(°)		(NS/cm)	(NTU)	(mg/L)	(+/- mV)	BTOC)	
1/22	900	55	12.84	7.21	0. 804	71000	1,61	1244	9.30	Cloudy Blowish - nu
1	430	65	13.20	745	17.704	71000	1.52	153.9	9.15	Crabe g 70. sarky
	940	20	13.12	7.45	0 763	71000	1147	1660	9.00	Com Clouds
	950	26	1354	7,40	0.743	21000	0.86	168.9	921	
1	1000	95	13.54	7,39	0.745	71000	0.83	1703	1.25	Clove
-	1010	120	13.29	7.58	0.764	7130	1.06	1345	9.23	- LUST FUTONS
-	1949	130	1307	7.34	0,760	7600	0.64	171.7	9.15	- 22 57 70 70-3
	1050	95	13.02	7.33	0.737	7/000	8.74	170.7	9.25	
	1100	35	13.01	7.33	0.744	71000	0.65	170.4	9.75	Strubussilary
	III	165	13.00	アン	0,764	273	0.45	170,8	9.25	clewer.
	1150	175	13.00	7.4	0.718	198	0.58	1707	8.20	Clewer Stories
	1130	185	12.94	731	0.763	138	0.68	169.3	8,73	
	1150	195	13.14	7.29	0.412	204	0.59	168.2	5.73	- Out of school good
	-	200	10.33	2.33	0716	7.00		173.7	7.50	Brust - Ling Had
		203	11.05	7.14	0.757	113	1.24	193.1		-Restati
		204		7.34	0.757	125	1.25	166.9	7.52	
	1250	309	With		0.759	113	11.23	1681	717	
		212.	10.42		0,732	128	1.22	174.1	7.57	STUP WI Waterla. contine
		214	10.60		0.724	132	1.23	1305		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	1757	219		7.27	0.774	112	1.24	175.9	7.41	4: 14:
		220	1248		0.756	374	0.99	-33.2	- U I	frull,
	(408		2.31	7.74	237.62	3/000		-84.8		
	1435	235			0.754	797	1.13	-83.2	7,45	clear a.
	1451		12.78	7.54	0.721	29.7	81.95	-41.2	2.40	SLatter weter @ 14
					The second leading to the second	79:6	The second second second second			



Project	Ref: A	meren GV	V Monito	ring			Project I	No.: 153-	1406.	
Locat	ion				BMV	-15				
Monitore	ed By:	25	T.	Date	1/22		Time	0200).	Da
Well F	Piezom	eter Data	a							PASEZ
Depth of	Well (from	(circle one) top of PVC or	around)		2.	5.95		feet		
		n top of PVC			5	25	-	feet		
Radius of			5,			2.00		inches	CFE	MAP
						6.00		feet		1 1
Casing V	olume				6.		-19.5	cubic feet	49.	5 totalsas
Devel	opmen	t / Purgi	ng Disc	charge	e Data				ww	
Purging N	Method		- No. 100			JUNGT	ec			
Start Purg	ging			Date	1/22/	11 Ea	Time	CY	2	
Stop Purg	ging			Date	1/35/	116	Time	(3)	1547	
Monitorin	9									
Date	Time	Volume Discharge (gals)	Temp (°4)	рН	Spec.Cond. (<u>M</u> S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
1/27	1500	234	10.39	7.44	0,761	19.6	1.26	-4309	7.45	lles
1/12	1510	241	10.37	7.40	0.752	27.8	1.31	-60.3	7.45	Cled
1/27	1520	243	10.32	7,41	0,743	12.6	1.33	-57.2	2.46	llew.
1/27	1530	245	10.31	X. V.	0.760	19.1	1.35	-59.2	744	
124	1,730		10.32	20.0	0.959	10	1.30	37.4	7.4.4	
THE R										
			-				2			
							TOUT .			
T. T.	1111/27									
			 							
						1				
	 	-	-							
								·		
	h	-		- 20		010	19			



Project Ref: Ameren GW Monitoring

	Locati	ion	BA	W-3	35				7 7]		
	Monitore	ed By:	M-60R		Date	11/10/2	1016	Time	1300) —	1700	arts f	- 1
	Wall E	liozom	eter Data			MIMITAC			1030		•	Stickup	2.6
	WEILL	1620111	(circle one)								1	,	
	Depth of \	Well (from	top of PVC or	ground)		2	6.74		feet		127	2) to rev 6.7 = 4	
	Depth of \	Water (fron	n top of PVC o	or ground)	-	5	3-65		feet				
	Radius of	Casing					2		inches		Nes	ed to rev	6VP
								- 1	feet		700	,	
	Casing Vo	olume					WAY.		cubic feet		401	17-14	- 1 . [
							6.7		gallons		10 1	6. 3 - 17	r gan
	Devel	opmen	t / Purgir	ng Disc	charge	Data							
	Purging N	flethod				Wal	era		19.3	*			
	Start Purg	ging			Date	11/10/2	616	Time	130	20	11/11/16 1	030	
	Stop Purg	jing			Date	11/10/20	गर	Time	170		12/14/16 14 11/11/16	2	
	Manitaria				,			•			11/11/16		
	Monitorin	9	1				1		100				-
	Data	Time	Volume	Temp	-11	Spec.Cond.	Turbidity	Dissolved	Redox	WL (ft			
	Date	Time	Discharge (gals)	(<u>°</u> <u>C</u>)	pН	(<u>M</u> S/cm)	(NTU)	Oxygen (mg/L)	Potential (+/- mV)	BTOC)	Appearance of \	Vater and Comments	
		1200					<u> </u>			8.95	START	1	
0	11/10	1320	20 40	17.21	7,49	0.638	>1000	4.59	-202	8.96	Plovely		
	<u> </u>	1330	100/60		7.39	0,744	71000	5-37	-271	8,99	Cloudy		
2		1350	20/80	16.73	7.19	0-739	> 1000		-418	2.94	Cloudy		
3 4	$\vdash\vdash$	1400	20/100	16.8	7,22	BARRAN	21000	1-90	-451	8.93	Cloudi		-
5	\vdash	1410	20/140	6.45	7.69	8.613	71000	3,02	-438	8.95	Cloudy		-
		1420	20/ 100	16.75	7.54	0.613	> 1000	3 31	-483	\$ 94	Clardy		-
67		1430	30/190	16.33	7.69	0.606	>1000	3.76	-492	\$ 9U	Clouds		1
		1440	20/200	16.39	7.51	0.603	71000	4-75	-486	8.96	Corts		
8	1	1450	26/220	16.73	7,21	6.602	> 1000	a.99	-484	8.93	Cloudy		1
12	Y	1500	20/240	16.48	7.70	0-595	坐 817	3.74	-478	8.91	Clouds		1
Above	1550	100	10/250	16,43	7.73	0.608	776	5,30	- 455	8.90	Clarely	- Deg Dec	ease f
Above Screen		1600	10/260	14.70		0.577	478	7.02	-413	8-91	Cloudy	Flon	rate
Julian		1610	10/270	15,26	7-38	6,580	600	6.54	-401	8.90	Cloudy	1/3	
1		1620	10/280	14.49	7.36	0,569	435	6.21	-41a	8.92	Clarke		1
	\sqcup	1630	10/290	14-33		0.560	324	643	- 406		Cloudy		
	<u> </u>	1640	10/300	13,99		0,955	264	5.93	- 418	8.91	Clevely.		1.
Buled	<u> </u>	1650	10/310	13.61	7-36	0.549	2/2	4.11	- 414	8.90	Cloudy 50	epped @	1650
recalipance	11/11	MANOO	10/330	18							Started	11/11	
equip "en"	105	10.40	20/340			0.78	182	4-53	-220	8.92	Cloudy		
		1100	10/350		7,41	0.768	164	225	-237	8:91	Cloudy		
recalibrated equipment		1110	10/360	18.78	7,25	0,761	139	4,66	-29(8.90	Clardy		
Lomores - M		1130	20 /380	18.91	4-26	0,740	131	4-51	-209	8.91	Cloudy		
GUYON		1150	20/400	18.65	7-26	0.720	132	H-80	-264	8,93	cloudy		
hock		1910	20/420	10.13	7.60	0.733	62	5,22	-255	8.91	Clardy		-
D.	1	1230	70/440	1273	7-21	0.714	162	4.42	- 287	8.92	Clardy		

Project No.: 153-1406.



Project	Ref: A	meren GW	/ Monito	ring			Project I	No.: 153-	1406.		
Locati	on	BHW	-35								•
Monitore	d By:	M-Got	Œ	Date	11/10/2	616	Time	130	0-1700	34	
Woll B	iozom	eter Data			11/10/2	016		1030	_		
Well	ICZUIII	(circle one)	ŧ							1 1	1.1
Depth of \	Vell (from	top of PVC or	ground)		ંગ્રેદ	.74		feet		727.0'	STIEL
Depth of \	Nater (fron	n top of PVC o	or ground)		8,	65		feet] Stiel
Radius of	Casing				ò			inches			276
					e.			feet			
Casing Vo	olume				_			cubic feet			
					Ь	. 7		gallons			
Devel	opmen	t / Purgir	ng Disc	charge	e Data						
Purging N	lethod				1/4	va					
Start Purg				Date	1410134		Time	12	00	11/11/2016	6 1630
Stop Purg	-			Date	15/10/20		Time		100	11/11/2016	-
pg	9				11/14/0	.0	1 ,,,,,,			.,,.,,	
Monitoring	9										
		Volume	т				Dissolved	Redox			
Date	Time	Discharge	Temp (° <u>C</u>)	pH .	Spec.Cond. (<u>*1</u> S/cm)	Turbidity (NTU)	Oxygen	Potential	WL (ft BTOC)	Appearance of Wate	r and Comments
		(gals)	<u> </u>				(mg/L)	(+/- mV)			
11/11/16	1230	20/440	18,93	7.21	0.714	62	4.42	-287	8,12	Cloudy	
	13/0	20/480	1867	7,25	0.703	523	4,56	-284	8.91	Gudy	
	1330	20/900	10.73	7,00	0,+13	64.2	4-32	- 327	8.92	Pause to coo	1 Dry D
	1350	20/500	17.37	7.61	0.723	46,2	5.02	-277	8,90	Clarky	7-4
	HUON	vsoy	16,			131			8,92	1350-1400	Flushed & c
		<u> </u>		- 4						@ highest	Flow rate
	1410	START	16ALON		-	 				by allo	minute bread
	1420	10/510	76.44	7.61	0,414	131	4.55	-250	8,92	Clardy	
	1440	20/530	15,94	7.56	0.711	70	5,97	-283	8,91	Cloudy	
·	1510	10/546	14.40	7,39	0.704	107	2-36	-316	8,90	Clardy 3/c	ned down v
	1530	10/984		6.96	0.6.74	30.6	3,41	-320	8-91	Cloudy	
	1550	10/570	13,36	7,42	0.677	35.1	5.10	-239	8-90	Claudy	
	1620	10/580	13.24	7,52	0,683	19.7	6,22	-187	8.92	cloudy	
	1650	10/590	13,05	7.59	0,683	16,5	6-73	-151		Clady	
		<u> </u>	 								
								f. 1.			
						-					
· · · · · · · · · · · · · · · · · · ·		111	-			-					
		1				 	<u> </u>				
						 		ļ		. \	
		L					L				

APPENDIX G CCR MDNR WELL CERTIFICATION FORMS

/ \	OURI DEPARTMEN	-	REF NO		DATE RECEIVED			
	JRAL RESOURCES			0512888			02/04/20	016
	SION OF		CR NO		CHECK NO.		17007	r o
	LOGY AND LAND S	URVEY	STATE WELL NO)		REVENU		<u> </u>
	368-2165		A206260 (02/09/2016				020416
MONITORING W			ENTERED NRBA	SSM	APPROVED B	BY		ROUTE
CERTIFICATION	RECORD		PH1 PH2	PH3				
INICODA A TION OUR	DI IED DV DDIMADV OOR	ITD A OTOD OD		//2016 02/08/2016				
NOTE: THIS FORM IS NOT TO BE USED	PLIED BY PRIMARY CON FOR NESTED WELLS	NIRACIOR OR	DRILLING CO	DNIRACIOR				
OWNER NAME AMEREN MISSOURI C/O B	ILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUTO	SKY				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDBERGH BLVD.		CITY ST LOUIS			STATE MO	ZIP 631:	27	NUMBER
SITE NAME SIOUX ENERGY CENTER					WELL NUMBER LMW 1S			COUNTY ST CHARLES
SITE ADDRESS 8501 N STATE ROUTE 94					CITY WEST ALTON			STATIC WATER LEVEL 26.8 FT
SURFACE COMPLETION TYPE	LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D		LE SURFACE COI	MPLETION GROUT	LOCATIO	N OF WEL	L
X ABOVE GROUND	LENGTH <u>5.0</u> FT.	PLACED DIAMETER 12.0	IN.	X CONCRET	E	LAT	38° :	<u>54</u> ' <u>46.32</u> "
FLUSH MOUNT	DIAMETER 4.0 IN.	LENGTH <u>2.5</u> FT.		OTHER		LONG	90°	<u>17</u> ' <u>30.75</u> "
					_		LLEST	LARGEST
LOCKING CAP				SURFACE COMPL	ETTION	-	1/4	1/4 1/4
WEEP HOLE		-	─~	STEEL X AL	LUMINUM PLASTIC	SEC	19	TWN. <u>48</u> NORTH
		IF		L — —		RANGE	6	Direction <u>E</u>
							RING FOR:	7
				_		RADIONI EXPLOSI		PETROLEUM PRODUCTS ONLY METALS VOC
		_		RISER		svocs		PESTICIDES/HERBICIDESS
ELEVATION	FT.			ı	TER <u>2.0</u> IN.	PROPOS	ED LIGE O	E WELL
ANNULAR SEAL				RISER PIPE LENGT HOLE DIAMETER			GRATION WELL	
LENGTH21	1 <u>.5</u> FT.			WEIGHT OR SDR#		EXTRA	CTION WELL	OPEN HOLE
SLURRY CH	upo.					PIEZON	METERS	
H H	ANULAR	-		MATERIAL	_	DIRECT	PUSH	
CEMENT/SLURRY IF CEMENT/BENTOI	NITE MIV-			STEEL	X THERMOPLASTIC (PVC)		PTH	FORMATION
				OTHER		FROM	ТО	DESCRIPTION
BAGS OF CEMENT				L_		0.0	1.5	FILL GRVL
%OF BENTONITE U: WATER USED/BAG:						1.5 12.0	12.0	SDY SLT SDY CLY SLT
WATER USED/BAG.	GAL.	L		BENTONITE SEAL		15.0	15.0 41.0	SND
				LENGTH: <u>3.5</u>	_			
				CHIPS PELL	ETS GRANULAR			
				SLURRY SATURATED ZONE	HYDRATED			
SECONDARY FILTE	R PACK			- DATOMATED ZONE	HIDRAIED			
LENGTH:		-						
				SCREEN DIAMETE	ED: O OIN			
			SCREEN DIAMETER:2.0IN. SCREEN LENGTH:9.8FT.					
DEPTH TO TOP OF	PRIMARY		DIAMETER OF DRILL HOLE: 6.0IN.					
FILTER PACK:			DEPTH TO TOP _	31.2FT.				

TOTAL DEPTH: _41.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 12/15/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: <u>12.3</u>FT.

SCREEN MATERIAL

OTHER

/ \ management	OURI DEPARTMEN	_	REF NO		DATE RECEIVED			
	RAL RESOURCES)512889			02/04/201	6
	ION OF		CR NO		CHECK NO.		170079	
	OGY AND LAND S	URVEY	STATE WELL NO)		REVENU		
	368-2165		A206261 C	2/09/2016				020416
MONITORING WE			ENTERED NRBA	SSM	APPROVED B	Y	F	OUTE
CERTIFICATION	RECORD		PH1 PH2	PH3				
			02/08/2016 02/08					
NFORMATION SUPP	LIED BY PRIMARY CON	NTRACTOR OR	DRILLING CO	NTRACTOR				
OWNER NAME AMEREN MISSOURI C/O BILI	L KUTOSKY	CONTACT NAME AMEREN MISSOUR	RI C/O BILL KUTOS	SKY				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDBERGH BLVD.		CITY ST LOUIS			STATE MO	ZIP 6312	27	NUMBER
SITE NAME SIOUX ENERGY CENTER					WELL NUMBER LMW 2S			COUNTY ST CHARLES
SITE ADDRESS 8501 N STATE ROUTE 94					CITY WEST ALTON			STATIC WATER LEVEL 27.0 FT
	LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND DI		E SURFACE COM	MPLETION GROUT	LOCATIO	N OF WELL	
	_ENGTH _ <u>5.0</u> FT.	PLACED DIAMETER 12.0		X CONCRETI	_	LAT	38° 54	' 26 E6"
	DIAMETER <u>4.0</u> IN.	LENGTH _2.5 FT.	IV.	OTHER			<u>36</u> <u>34</u> 90 ° 17	·
							LLEST	LARGEST
							1/4	1/4 1/4
LOCKING CAP				SURFACE COMPLI				
WEEP HOLE		1_	-	STEEL X ALI	UMINUM PLASTIC			VN48 NORTH
		- 11				RANGE	RING FOR:	Direction <u>E</u>
						RADION	JCLIDES	PETROLEUM PRODUCTS ONLY
				RISER		EXPLOSI SVOCS		METALS VOC PESTICIDES/HERBICIDESS
ELEVATION	FT	r '	11	RISER PIPE DIAMET	TER 2.0IN			LOTTOIDEOTTERBIOIDEGO
				RISER PIPE LENGTI		PROPOS	ED USE OF	WELL
ANNULAR SEAL				HOLE DIAMETER			GRATION WELL	X OBSERVATION
LENGTH19.5	EFT.			WEIGHT OR SDR#	SCH40	EXTRA	CTION WELL	OPEN HOLE
SLURRY CHIP	s					PIEZON DIRECT		
PELLETS GRAM		- $ $ $ $		MATERIAL	_			
CEMENT/SLURRY IF CEMENT/BENTONI	TF MIX:			STEEL)	X THERMOPLASTIC (PVC)	DEF		FORMATION
				OTHER		FROM	ТО	DESCRIPTION
BAGS OF CEMENT US				L		0.0		GRVL FILL
%OF BENTONITE USE						1.0		SDY SLT
WATER USED/BAG:	GAL.			BENTONITE SEAL		6.2 10.0		CLY SLT STY SND
				LENGTH:5.0		25.0		IND
				CHIPS PELLE	ETS GRANULAR			
				SLURRY				
				SATURATED ZONE	HYDRATED			
SECONDARY FILTER LENGTH:1.		_						
LLINGIAI.	<u>u</u>			SCREEN				
				SCREEN DIAMETE				
			_	SCREEN LENGTH:				
DEPTH TO TOP OF P				DIAMETER OF DRI				
FILTER PACK:	<u>18.0</u> FT.			PEF 111 10 10P	P31.2FT.			

TOTAL DEPTH: _41.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 12/16/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: <u>23.0</u>FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMEN		REF NO		DATE RECEIVED			
NATURAL RESOURCES		CR NO	00512890	CHECK NO.		02/04/20	16
DIVISION OF	LIDVEV	OKTO		onzortio.		170079	9
GEOLOGY AND LAND S (573) 368-2165	URVEY	STATE WELL		1	REVENU	E NO.	
MONITORING WELL		A206262 ENTERED NR	02/09/2016	APPROVED B	Y		020416 ROUTE
CERTIFICATION RECORD		PH1 PH2		AFFROVEDB	ī		ROUTE
		02/08/2016 02	/08/2016 02/08/2016				
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NTRACTOR OR	DRILLING	CONTRACTOR				
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KU	ГОЅКҮ				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDBERGH BLVD.	CITY ST LOUIS			STATE MO	ZIP 631:		NUMBER
SITE NAME SIOUX ENERGY CENTER				WELL NUMBER LMW 3S			COUNTY ST CHARLES
SITE ADDRESS 8501 N STATE ROUTE 94				CITY WEST ALTON			STATIC WATER LEVEL 8.41 FT
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D		HOLE SURFACE COI	MPLETION GROUT	LOCATIO	ON OF WELI	L
X ABOVE GROUND LENGTH 5.0 FT.	PLACED DIAMETER 12.0	<i>/</i>	X CONCRET	_	LAT	38 °5	4' 26 94"
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH <u>2.5</u> FT.		OTHER			<u> </u>	
					SMA	LLEST	LARGEST
LOCKING CAP			SURFACE COMPL	ETTION	_	1/4	1/4 1/4
WEEP HOLE	-			LUMINUM PLASTIC	SEC.	19 7	WN48 NORTH
	ΙΓ				RANGE	6	Direction <u>E</u>
					MONITO	RING FOR:	PETROLEUM PRODUCTS ONLY
					EXPLOS	1/	METALS VOC
ELEVATION FT.	_ '		RISER	TER 2.0IN.	svocs		PESTICIDES/HERBICIDESS
LLEVATIONTT.			RISER PIPE LENGT	·	PROPOS	ED USE OF	WELL
ANNULAR SEAL			HOLE DIAMETER			IGRATION WELL	X OBSERVATION
LENGTH0.0FT.		+	WEIGHT OR SDR#	SCH40	PIEZON	CTION WELL	OPEN HOLE
SLURRY CHIPS			MATERIAL		DIREC		
PELLETS GRANULAR CEMENT/SLURRY				X THERMOPLASTIC (PVC)	DEI	PTH	FORMATION
IF CEMENT/BENTONITE MIX:			OTHER		FROM	ТО	DESCRIPTION
BAGS OF CEMENT USED:			L		0.0	10.0	STY CLY
%OF BENTONITE USED:					10.0		SDY SLT
WATER USED/BAG: GAL.	L L		→ BENTONITE SEAL		10.9 22.0		SND SND
			LENGTH:10.0				
			CHIPS PELL	ETS GRANULAR			
			SATURATED ZONE	HYDRATED			
SECONDARY FILTER PACK							
LENGTH: <u>0.1</u> FT.	7 1 1		SCREEN				
			SCREEN DIAMETE	ER: <u>2.0</u> IN.			
			SCREEN LENGTH	:9.8FT.			
DEPTH TO TOP OF PRIMARY			DIAMETER OF DR DEPTH TO TOP				
FILTER PACK: 13.0FT			I DELIGIOLOP _	<u> 15.∠</u> F .	l	1	

TOTAL DEPTH: _25.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 12/08/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____12.0FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMEN	IT OF	REF NO		DATE RECEIVED			
NATURAL RESOURCES		CR NO	00512891	CHECK NO.		02/04/20	16
DIVISION OF		CRINO		CHECK NO.		170079)
🛮 🧸 🛞 🛮 GEOLOGY AND LAND S	URVEY	STATE WELL N	NO		REVENU		
(573) 368-2165		A206263	02/09/2016				020416
MONITORING WELL		ENTERED NRE	BASSM	APPROVED B	Y		ROUTE
CERTIFICATION RECORD		PH1 PH2	PH3				
INFORMATION OF IRRUST BY BRIDE BY COM	ITD A OTOD OF		08/2016 02/08/2016				
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NIRACTOR OF	R DRILLING C	ONTRACTOR				
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOL	JRI C/O BILL KUT	OSKY				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDBERGH BLVD.	CITY ST LOUIS			STATE MO	ZIP 631:	27	NUMBER
SITE NAME SIOUX ENERGY CENTER	1			WELL NUMBER LMW 4S			COUNTY ST CHARLES
SITE ADDRESS 8501 N STATE ROUTE 94				CITY WEST ALTON			STATIC WATER LEVEL 5.5 FT
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D		OLE SURFACE COM	MPLETION GROUT	LOCATIO	N OF WELL	-
X ABOVE GROUND LENGTH 5.0 FT.	PLACED DIAMETER 12.0		X CONCRET	E	ΙΔΤ	38° 5	4' 25 62"
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH _2.5 FT.	2 IIV.	OTHER			90° 1	
'	•					LEST	LARGEST
			011051.05.001101			1/4	1/4 1/4
LOCKING CAP	C		SURFACE COMPL				
WEEP HOLE	l r	\neg \mid	STEEL X AL	UMINUM PLASTIC	SEC RANGE		WN. <u>48</u> NORTH Direction E
	- 11					RING FOR:	Direction <u>L</u>
					RADIONI	JCLIDES	PETROLEUM PRODUCTS ONLY
			RISER		EXPLOS SVOCS	VES X	METALS VOC PESTICIDES/HERBICIDESS
ELEVATIONFT.		1.1	RISER PIPE DIAME	TER2.0IN.			
			RISER PIPE LENGT	H17.0FT.	PROPOS	ED USE OF	WELL
ANNULAR SEAL		11	HOLE DIAMETER		l 🛏	GRATION WELL	X OBSERVATION
LENGTH0.0FT.		+	WEIGHT OR SDR#	SCH40	PIEZON	CTION WELL	OPEN HOLE
SLURRY CHIPS			MATERIAL		DIRECT		
PELLETS GRANULAR CEMENT/SLURRY			MATERIAL STEEL	X THERMOPLASTIC (PVC)	DEI	тн	FORMATION
IF CEMENT/BENTONITE MIX:			OTHER	<u> </u>	FROM	ТО	DESCRIPTION
BAGS OF CEMENT USED:			L U		0.0	4.5	STY CLY
%OF BENTONITE USED:					4.5		STY SND
WATER USED/BAG: GAL.					7.5	11.4	SND
	L	_	BENTONITE SEAL		11.4		STY SND
			LENGTH: 9.5	ETS GRANULAR	15.6		SND
			SLURRY	ETS GRANULAR	21.7	25.0	SND
			SATURATED ZONE	HYDRATED			
SECONDARY FILTER PACK							
LENGTH: <u>0.1</u> FT.	7 11		SCREEN				
			SCREEN DIAMETE	R: 2.0IN.			
			SCREEN LENGTH:				
DEPTH TO TOP OF PRIMARY			DIAMETER OF DRI				
FILTER PACK: 12.4FT.		2.2	DEPTH TO TOP	<u>15.2</u> FT.			

TOTAL DEPTH: _25.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 12/08/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: <u>12.6</u>FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMEN		REF NO		DATE RECEIVED			
NATURAL RESOURCES		CR NO	00512892	CHECK NO.		02/04/201	6
DIVISION OF	LIDVEV	o.c.co		onzonno.		170079	
GEOLOGY AND LAND S (573) 368-2165	URVEY	STATE WELL		1	REVENU	E NO.	
MONITORING WELL		A206264 ENTERED NR	02/09/2016	APPROVED B	V		020416 ROUTE
CERTIFICATION RECORD		PH1 PH2		AFFROVED B	1	,	KOOTE
		02/08/2016 02	/08/2016 02/08/2016				
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NTRACTOR OR	DRILLING	CONTRACTOR				
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KU	ГОЅКҮ				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDBERGH BLVD.	CITY ST LOUIS			STATE MO	ZIP 631:	27	NUMBER
SITE NAME SIOUX ENERGY CENTER				WELL NUMBER LMW 5S			COUNTY ST CHARLES
SITE ADDRESS 8501 N STATE ROUTE 94				CITY WEST ALTON			STATIC WATER LEVEL 27.9 FT
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D		HOLE SURFACE COI	MPLETION GROUT	LOCATIO	N OF WELL	
X ABOVE GROUND LENGTH _5.0 FT.	PLACED DIAMETER 12.0	<i>/</i>	X CONCRET	E	ΙΔΤ	38° 54	' 25 84"
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH <u>2.5</u> FT.		OTHER			90° 1	
					SMA	LLEST	LARGEST
LOCKING CAP			SURFACE COMPL	ETTION	_	1/4	1/4 1/4
WEEP HOLE	ү —	→ _	STEEL X A	LUMINUM PLASTIC	SEC.	19 T	NN48 NORTH
	ΙΓ				RANGE	6	Direction <u>E</u>
					MONITO	RING FOR:	PETROLEUM PRODUCTS ONLY
					EXPLOS	ves X	METALS VOC
ELEVATION FT.	_ '		RISER	TER 2.0IN.	SVOCS	Ш	PESTICIDES/HERBICIDESS
LLEVATIONTT.			RISER PIPE LENGT		PROPOS	ED USE OF	WELL
ANNULAR SEAL			HOLE DIAMETER	8.0IN.	l 🛏	GRATION WELL	X OBSERVATION
LENGTH <u>23.5</u> FT.		++	WEIGHT OR SDR#	SCH40	PIEZON	CTION WELL	OPEN HOLE
SLURRY CHIPS			MATERIAL		DIRECT		
PELLETS GRANULAR CEMENT/SLURRY				X THERMOPLASTIC (PVC)	DEI	PTH	FORMATION
IF CEMENT/BENTONITE MIX:			OTHER	_	FROM	ТО	DESCRIPTION
BAGS OF CEMENT USED:			L =		0.0	20.0	SDY STY
%OF BENTONITE USED:					20.0		STY CLY
WATER USED/BAG: GAL.			─ BENTONITE SEAL		30.0 35.8		SDY SLT SND
			LENGTH:5.0		38.0		SND
			CHIPS PELL	ETS GRANULAR			
			SLURRY SATURATED ZONE	HYDRATED			
SECONDARY FILTER PACK			SATURATED ZONE	HIDRAIED			
LENGTH:1.0FT.	-						
			SCREEN SCREEN DIAMETE	:B· 2 OIN			
			SCREEN LENGTH:				
DEPTH TO TOP OF PRIMARY			DIAMETER OF DR	ILL HOLE: 8.0IN.			
FILTER PACK: 31 4FT			DEPTH TO TOP _	<u>35.2</u> FT.			

TOTAL DEPTH: _45.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 12/14/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____13.6FT.

SCREEN MATERIAL

OTHER

/ \ ~~~~~~	SOURI DEPARTMEN		REF NO		DATE RECEIVED			
	URAL RESOURCES		CR NO	00512893	CHECK NO.		02/04/20	16
4 A a=a	SION OF		CKNO		CHECK NO.		170079	
	LOGY AND LAND S	URVEY	STATE WELL N	10		REVENU	E NO.	
, ,) 368-2165 (E. I.		A206265	02/09/2016			1.	020416
MONITORING W			PH1 PH2	ASSM PH3	APPROVED B	Υ		ROUTE
CLIVIII ICATION	INLOOND			08/2016 02/08/2016				
INFORMATION SUP	PLIED BY PRIMARY COI	NTRACTOR OR	DRILLING C	ONTRACTOR			<u>, </u>	
OWNER NAME AMEREN MISSOURI C/O B	ILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUTO	DSKY				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDBERGH BLVD.		CITY ST LOUIS			STATE MO	ZIP 631:	27	NUMBER
SITE NAME SIOUX ENERGY CENTER					WELL NUMBER LMW 6S			COUNTY ST CHARLES
SITE ADDRESS 8501 N STATE ROUTE 94					CITY WEST ALTON			STATIC WATER LEVEL FT
SURFACE COMPLETION TYPE	LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D		DLE SURFACE COI	MPLETION GROUT	LOCATIO	N OF WELL	
X ABOVE GROUND	LENGTH _5.0 FT.	PLACED DIAMETER 12.0	IN.	X CONCRET	E	LAT. <u>38</u> ° <u>54</u> ' <u>31.08</u> "		
FLUSH MOUNT	DIAMETER 4.0 IN.	LENGTH 2.5 FT.		OTHER		LONG	90°_1	<u>7' 12.56"</u>
				_	_		LLEST	LARGEST
LOCKING CAP				_ SURFACE COMPL	ETTION	_	1/4	1/4 1/4
WEEP HOLE		7-		STEEL X A	LUMINUM PLASTIC	SEC	<u>19</u> T	WN. <u>48</u> NORTH
				L		RANGE		Direction <u>E</u>
				_		RADIONI	RING FOR: JCLIDES	PETROLEUM PRODUCTS ONLY
				RISER		EXPLOS SVOCS		METALS VOC PESTICIDES/HERBICIDESS
ELEVATION	FT.	F '		1	TER2.0IN.			
				RISER PIPE LENGT	ΓΗ <u>31.9</u> FT.		ED USE OF	
ANNULAR SEAL				HOLE DIAMETER			GRATION WELL CTION WELL	X OBSERVATION OPEN HOLE
LENGTH18	<u>8.5</u> F1.		+	WEIGHT OR SDR#	SCH40	1 =	METERS	OT ENTINEE
	HIPS RANULAR	_		MATERIAL		DIRECT	T PUSH	
CEMENT/SLURRY				STEEL	X THERMOPLASTIC (PVC)	DEI	PTH	FORMATION
IF CEMENT/BENTO	NITE MIX:			OTHER		FROM	ТО	DESCRIPTION
BAGS OF CEMENT	USED:			L		0.0	12.7	SLT
%OF BENTONITE U						12.7		SDY SLT
WATER USED/BAG:	GAL.	L L		BENTONITE SEAL		14.0 20.0		SLT SND
				LENGTH: <u>6.0</u>	_	30.0		SND
				CHIPS PELL	LETS GRANULAR			
				SLURRY SATURATED ZONE	HYDRATED			
SECONDARY FILTE	ER PACK				···-··			
LENGTH:		-		CORECT				
				SCREEN DIAMETE	ER: 2.0IN			
			SCREEN DIAMETER: 2.0IN. SCREEN LENGTH: 9.8FT.					
DEPTH TO TOP OF	PRIMARY			DIAMETER OF DR				
FILTER PACK:	27 8FT			DEPTH TO TOP _	<u>30.2</u> FT.			

TOTAL DEPTH: _40.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 12/14/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____12.2FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTME	NT OF	REF NO		DATE RECEIVED			
NATURAL RESOURCE		0512894	02/04/2016				
DIVISION OF	CR NO		CHECK NO. 170079				
🛮 🧸 🛮 🛞 🛮 GEOLOGY AND LAND	SURVEY	STATE WELL NO)		REVENU		
(573) 368-2165		A206266	02/09/2016				020416
MONITORING WELL		ENTERED NRBA	ASSM	APPROVED B	Υ	-	ROUTE
CERTIFICATION RECORD		PH1 PH2	PH3 8/2016 02/08/2016				
INFORMATION CUIDDUIFD BY DDIMARY C							
INFORMATION SUPPLIED BY PRIMARY C NOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	JNTRACTOR OR	DRILLING CO	JNTRACTOR				
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUTO	SKY				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDBERGH BLVD.	CITY ST LOUIS			STATE MO	ZIP 6312	27	NUMBER
SITE NAME SIOUX ENERGY CENTER				WELL NUMBER LMW 7S	1		COUNTY ST CHARLES
SITE ADDRESS 8501 N STATE ROUTE 94				CITY WEST ALTON			STATIC WATER LEVEL 20.8 FT
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	SURFACE COMPL		LE SURFACE COI	MPLETION GROUT	LOCATIO	N OF WELL	-
X ABOVE GROUND LENGTH <u>5.0</u> FT.	PLACED DIAMETER 12.0	IN.	X CONCRET	E	LAT.	38° 54	<u>4</u> ' <u>35.82</u> "
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH <u>2.5</u> FT.		OTHER		LONG	<u>90</u> ° <u>1</u>	<u>7' 15.21"</u>
				_		LLEST	LARGEST
LOCKING CAP			_ SURFACE COMPL	ETTION		1/4	1/4 1/4
WEEP HOLE	-	─	STEEL X A	LUMINUM PLASTIC	SEC	<u>19</u> T	WN48 NORTH
	١r				RANGE		Direction <u>E</u>
	11					RING FOR:	
					RADIONU EXPLOSI		PETROLEUM PRODUCTS ONLY METALS VOC
	_		RISER		svocs		PESTICIDES/HERBICIDESS
ELEVATIONFT.			1	TER <u>2.0</u> IN.	PPOPOO	ED HOE OF	WELL
ANNULAR SEAL			RISER PIPE LENGT HOLE DIAMETER			ED USE OF GRATION WELL	VVELL X OBSERVATION
LENGTH0.0FT.			WEIGHT OR SDR#		EXTRA	CTION WELL	OPEN HOLE
SLURRY CHIPS]		PIEZON		
PELLETS GRANULAR	-		MATERIAL	_	DIRECT	PUSH	
CEMENT/SLURRY IF CEMENT/BENTONITE MIX:			STEEL	X THERMOPLASTIC (PVC)	DEF		FORMATION
			OTHER		FROM	ТО	DESCRIPTION
BAGS OF CEMENT USED:			L		0.0		GRVL FILL
%OF BENTONITE USED: WATER USED/BAG: GAL.					1.0 5.0		SLT SND
WATER OSED/BAG. GAE.	L		BENTONITE SEAL		6.0		SLT
			LENGTH:24.5	_	10.0		GRVL
			CHIPS PELL	ETS GRANULAR	12.5	40.0	SND
			SLURRY SATURATED ZONE	HYDRATED			
SECONDARY FILTER PACK	ГП		OATONATED ZONE	HIDRATED			
LENGTH: 1.0FT.	-						
			SCREEN	- D - 0 0 1 1 1			
			SCREEN DIAMETE SCREEN LENGTH:				
DEPTH TO TOP OF PRIMARY			DIAMETER OF DR				
FILTER PACK: 27.8FT.		*****	DEPTH TO TOP _	30.2FT.			

LENGTH OF PRIMARY FILTER

PACK: <u>12.2</u>FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMEN	-	REF NO		DATE RECEIVED			
NATURAL RESOURCES		0512895	02/04/2016				
DIVISION OF	CR NO		CHECK NO.	CHECK NO. 170079			
🛮 🧸 🛞 🛮 GEOLOGY AND LAND S	URVEY	STATE WELL NO)		REVENUE I		
(573) 368-2165		A206267	02/09/2016				020416
MONITORING WELL		ENTERED NRBA	ASSM	APPROVED B	Y	RO	UTE
CERTIFICATION RECORD			PH3				
			3/2016 02/08/2016				
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NTRACTOR OR	DRILLING CO	ONTRACTOR				
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOUI	RI C/O BILL KUTO	SKY				VARIANCE GRANTED BY DNR
OWNER ADDRESS 3750 S LINDBERGH BLVD.	CITY ST LOUIS			STATE MO	ZIP 63127		NUMBER
SITE NAME SIOUX ENERGY CENTER	1			WELL NUMBER LMW 8S	l l		COUNTY ST CHARLES
SITE ADDRESS 8501 N STATE ROUTE 94				CITY WEST ALTON			STATIC WATER LEVEL 23.2 FT
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND DI SURFACE COMPL PLAMETER 12.0	ETION WAS			LOCATION		2.20
X ABOVE GROUND LENGTH 5.0 FT. FLUSH MOUNT DIAMETER 5.0 IN.	DIAMETER 12.0 LENGTH 2.5 FT.	IIV.	X CONCRET OTHER			38 ° 54' 4 90 ° 17' 1	
			4		SMALLI		LARGEST
							1/4 1/4
LOCKING CAP			SURFACE COMPL				
WEEP HOLE	Tr	\neg	STEEL X AL	UMINUM PLASTIC			I. <u>48</u> NORTH
	- 11				MONITORIN		rection <u>E</u>
					RADIONUCL	IDES PET	ROLEUM PRODUCTS ONLY
			Γ		EXPLOSIVES SVOCS	_	TALS VOC STICIDES/HERBICIDESS
ELEVATION FT.	_ '	11	RISER RISER PIPE DIAME	TER 2.0IN	SVOCS	L PES	STICIDES/RERBICIDESS
LEEVATIONTT.			RISER PIPE LENGT	· · · · · · · · · · · · · · · · · · ·	PROPOSED	D USE OF WI	ELL
ANNULAR SEAL			HOLE DIAMETER		GAS MIGRA	ATION WELL	X OBSERVATION
LENGTH <u>24.5</u> FT.			WEIGHT OR SDR#	SCH40	EXTRACTION		OPEN HOLE
SLURRY CHIPS					DIRECT PU		
PELLETS GRANULAR	\dashv \mid \mid		MATERIAL	7			
CEMENT/SLURRY IF CEMENT/BENTONITE MIX:			STEEL OTHER	THERMOPLASTIC (PVC)	DEPT		FORMATION
			I U —		FROM	ТО	DESCRIPTION
BAGS OF CEMENT USED:			h		0.0		Y SLT
%OF BENTONITE USED: WATER USED/BAG: GAL.					17.8 22.0	22.0 SLY 25.0 SNI	/ SLT
WATER OSEDIBAG. GAE.			BENTONITE SEAL		25.0		/ SLT
			LENGTH:4.5		30.0	45.0 SNI	
			CHIPS PELL	GRANULAR GRANULAR			
			SLURRY SATURATED ZONE	HYDRATED			
SECONDARY FILTER PACK	ГП		SATURATED ZONE	HYDRATED			
LENGTH:1.0FT.	-						
			SCREEN				
			SCREEN DIAMETE				
			SCREEN LENGTH: DIAMETER OF DRI				
DEPTH TO TOP OF PRIMARY			DEPTH TO TOP				
FILTER PACK: 32.3FT.			1				

TOTAL DEPTH: _45.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 12/15/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____12.7FT.

SCREEN MATERIAL

OTHER

/ \	SOURI DEPARTMEN	-	REF NO		DATE RECEIVED				
NATURAL RESOURCES				0512896	02/04/2016				
	SION OF		CR NO CHECK NO.			170079			
1507	LOGY AND LAND S	URVEY	STATE WELL NO)		REVENU		<u> </u>	
` ,	368-2165		A206268 (02/09/2016				020416	
MONITORING W			ENTERED NRBA	SSM	APPROVED B	Υ		ROUTE	
CERTIFICATION	RECORD		PH1 PH2	PH3					
	D. I.E.D. D.V. D.D.II. (A.D.V. O.D.)			/2016 02/08/2016					
NOTE: THIS FORM IS NOT TO BE USED	PLIED BY PRIMARY CON FOR NESTED WELLS	NIRACTOR OR	DRILLING CC	DNIRACIOR					
OWNER NAME AMEREN MISSOURI C/O BI	ILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUTO	SKY				VARIANCE GRANTED BY DNR	
OWNER ADDRESS 3750 S LINDBERGH BLVD.		CITY ST LOUIS			STATE MO	ZIP 6312	27	NUMBER	
SITE NAME SIOUX ENERGY CENTER					WELL NUMBER LMW 9S			COUNTY ST CHARLES	
SITE ADDRESS 8501 N STATE ROUTE 94					CITY WEST ALTON			STATIC WATER LEVEL 23.6 FT	
SURFACE COMPLETION TYPE	LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D SURFACE COMPL		LE SURFACE COI	MPLETION GROUT	LOCATIO	N OF WEL	L	
X ABOVE GROUND	LENGTH <u>5.0</u> FT.	PLACED DIAMETER 12.0	IN.	X CONCRET	E	LAT	<u>38</u> ° _ 5	<u>54' _52.1</u> "	
FLUSH MOUNT	DIAMETER 4.0 IN.	LENGTH <u>2.5</u> FT.		OTHER		LONG	90 °	<u>17</u> ' <u>25.39</u> "	
					_		LLEST	LARGEST	
LOCKING CAP				SURFACE COMPL	ETTION	_	1/4	1/4 1/4	
WEEP HOLE		-	─~	STEEL X AL	LUMINUM PLASTIC	SEC	19	TWN. <u>48</u> NORTH	
		IT				RANGE		Direction <u>E</u>	
							RING FOR:	1	
				_		RADIONU EXPLOSI		PETROLEUM PRODUCTS ONLY METALS VOC	
		_		RISER		svocs		PESTICIDES/HERBICIDESS	
ELEVATION	FT.			1	TER2.0IN.				
ANNULAR SEAL							PROPOSED USE OF WELL GAS MIGRATION WELL X OBSERVATION		
LENGTH).0FT.		WEIGHT OR SDR# SCH40 EXTRACTION WELL				OPEN HOLE		
							METERS		
SLURRY CH PELLETS GR	RANULAR	-		MATERIAL		DIRECT	PUSH		
CEMENT/SLURRY IF CEMENT/BENTOI	NITE MIV.			STEEL	X THERMOPLASTIC (PVC)		PTH	FORMATION	
				OTHER		FROM	ТО	DESCRIPTION	
BAGS OF CEMENT	USED:			L		0.0	12.3	FILL SND	
%OF BENTONITE U						12.3	15.0	GRVL	
WATER USED/BAG:	GAL.			BENTONITE SEAL		15.0 22.0		CLY SLT STY SND	
				LENGTH:25.0		25.0	40.0	SND	
				CHIPS PELL	ETS GRANULAR				
				SLURRY	П				
SECONDARY FILTE	R PACK			SATURATED ZONE	HYDRATED				
LENGTH:		-							
				SCREEN					
		-		SCREEN DIAMETE SCREEN LENGTH:					
DEDTH TO TOP OF	DDIMADV		=	DIAMETER OF DR					
DEPTH TO TOP OF FILTER PACK:				DEPTH TO TOP					

TOTAL DEPTH: 40.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 12/18/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____12.2FT.

SCREEN MATERIAL

OTHER

()	DEPARTMEN	_	RE	EF NO			DAT	E RECEIVED					
NATURAL RESOURCES			0.5	00512903			02/04/2016						
DIVISION (Ci	CR NO CHECK NO.			CK NO.	170079							
	AND LAND S	URVEY	ST	TATE WELL	NO				REVENU				
(573) 368-2	2165		A2	206275	02/0	9/2016					02	0416	
MONITORING WELL				NTERED NR	RBASS	М		APPROVED B	Y		ROUT	E	
CERTIFICATION RECO	ORD		PH										
INFORMATION OURDUIED I	V/ DDIMA DV/ 00A	ITDAOTOD				16 02/08/2016							
INFORMATION SUPPLIED E		NIRACIOR	OR DI	RILLING (CON	TRACTOR							
OWNER NAME AMEREN MISSOURI C/O BILL KUTOS	SKY	CONTACT NAI AMEREN MISS		C/O BILL KU	TOSK	(/ARIANCE GRANTE DNR	D BY
OWNER ADDRESS 3750 S LINDBERGH BLVD.		CITY ST LOUIS					STA MO	TE	ZIP 63127 NUMBER			NUMBER	
SITE NAME SIOUX ENERGY CENTER								L NUMBER V 1S				COUNTY ST CHARLES	
SITE ADDRESS 8501 N STATE ROUTE 94							CITY	/ ST ALTON			S	STATIC WATER LEV 7.4 FT	EL
	AND DIAMETER OF E COMPLETION	DIAMETER AN SURFACE CO PLACED			HOLE	SURFACE COI	MPLE"	TION GROUT	LOCATIO	N OF WEL	L		
X ABOVE GROUND LENGTH	<u>5.0</u> FT.	DIAMETER	<u>12.0</u> IN.			X CONCRET	ΓE		LAT	38°_5	54' <u>50.2</u>	22"	
FLUSH MOUNT DIAMETE	ER <u>4.0</u> IN.	LENGTH 2.5	FT.			OTHER				90°	18' <u>4.</u> 5		
						_				LLEST		LARGEST	4/4
LOCKING CAP		_		_	_	SURFACE COMPL	ETTIC	N		1/4		1/4	_ 1/4
WEEP HOLE		ነ		ゴ —	-	STEEL X A	LUMINUN	PLASTIC	SEC	19	TWN.	48 NORTH	1
				11	L				RANGE			tion <u>E</u>	
									MONITO	RING FOR:	7	LEUM PRODUCTS ONLY	
									EXPLOSI		METAL	s voc	
ELEVATION ET		_ []			- 1	RISER		0.011	svocs	L	PESTIC	CIDES/HERBICIDESS	
ELEVATIONFT.					- 1	RISER PIPE DIAME RISER PIPE LENGT			PROPOS	ED USE OI	F WFI I	 I	
ANNULAR SEAL					- 1	HOLE DIAMETER				GRATION WELL		X OBSERVATION	
LENGTH0.0FT.			_		٠ اــــــــــــــــــــــــــــــــــــ	WEIGHT OR SDR#		SCH40	EXTRA	CTION WELL		OPEN HOLE	
SLURRY CHIPS									PIEZON DIRECT	METERS			
PELLETS GRANULAR		-				MATERIAL							
CEMENT/SLURRY IF CEMENT/BENTONITE MIX:						OTHER	X THE	RMOPLASTIC (PVC)		PTH		FORMATION	
BAGS OF CEMENT USED:						U OTTER			FROM	ТО		DESCRIPTION	
					-				0.0	8.5	SDY S		
%OF BENTONITE USED: WATER USED/BAG: GAL.									8.5 15.6	15.6 17.5	STY C	;LY	
WW. 2.1. 6625, 57.6. 67.2.		L			—	BENTONITE SEAL			17.5		STY C	CLY	
						LENGTH:9.5			18.5	25.0	SND		
					-	CHIPS PELL	LETS	GRANULAR					
						SATURATED ZONE		HYDRATED					
SECONDARY FILTER PACK						_							
LENGTH: <u>0.1</u> FT.		-											
						SCREEN DIAMETE	=R·	2 0101					
		F				SCREEN LENGTH:							
DEPTH TO TOP OF PRIMARY						DIAMETER OF DR	ILL HO	DLE: <u>6.0</u> IN.					
FILTER PACK: 12.5FT						DEPTH TO TOP _	1	<u>5.2</u> FT.					

TOTAL DEPTH: 25.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x JOHN SUOZZI 006284 12/08/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: <u>12.5</u>FT.

SCREEN MATERIAL

OTHER

0	≋ ≋
A	(4)

MISSOURI DEPARTMENT OF NATURAL RESOURCES GEOLOGICAL SURVEY PROGRAM

MONITORING WELL CERTIFICATION RECORD

OFFICE US	E ONLY	DATE RECEI	VED
REFERENCE N	10.	CHECK NO.	
STATE WELL	NO.	REVENUE N	O
ENTERED	APPROVED	DATE	TROUTE

NOTE: This for	orm is not to be used for	nocted w	allo.			ENTERE)	APPROVE)	DATE		ROUTE	
	SITE INFORMATION	nesteu w	3113							1		1	1
	NAME WHERE WELL IS LOCATED			IP	RIMARY P	HONE NUMBER	R WITH ARE	A CODE IV	VELL NUM	MBER TV	WELL COM	PLETION	DATE
Sioux Energy	Center							diameter and the second	BMW-3	C-3000	11/08/20		
PROPERTY OWNER 8501 N State I	MAILING ADDRESS Rd 94				ř.,	West	Alton		STA M		ZIP CODE 63386		
PHYSICAL ADDRESS 8501 N State	S OF PROPERTY WHERE WELL IS LO Rd 94	OCATED				CITY West	Alton		1	Oharles			
NAME OF SITE OR O	CLEANUP PROJECT GW Monitoring		NR/EPA PI			OR REGULATO	RY SITE ID I	NUMBER (IF	APPLICA	ABLE)	VARIANCE I	NUMBER	(IF ISSUED)
PRIMARY CONTRAC	CTOR NAME (PLEASE PRINT)					PERMIT I	NUMBER	to	comply v	6.607(3), RSM vith all rules a Sections 256	and regulatio	ns promul	
SURFACE COMP	LETION									OF WELL (D/I			
TYPE Above Ground	LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER SURFACE	COMPLETI			SURFACE CO	MPLETION (SROUT La	titude _3		54	5	0.93N _"
☐ Flush Mount	Length 2.57 FT. Diameter 4 IN.	Diameter				☑ Concrete ☐ Other		Loi	ngitude _	90 .	18	, 1	6.53W "
		'n	7 -	-		CE COMPLET	TION	SM Se	ction	½ Tow	nship		rth
Elevation 424.12	2FT.			_ _	COMPL	OR CASING (ETION) ing Diameter	IF OPEN H	OLE TY	PE OF W Direct Pu Gas Migra Observati Piezomet	ELL (CHECK sh		Inclinor	er
ANNULAR SEAL Length 9	FT.					ing Length	16.5	FT. MC	ONITORIN Explosive	G FOR (CHE	CK ALL TH		7)
☑ Slurry ☐ Ch					Weight O	r SDR#	S40	吕	Radionuc	s/Herbicides lides on-petroleum)	☐ SVOC	S	ata
☐ Cement/Slurry					MATER		(D) (O)	_		EPTH TO			SCRIPTION RING LOG*)
IF CEMENT/BENT	TONITE MIX:					☑ Thermople	60 61	-	FROM	10	+		
Bags of Cement Used % of Bentonite Used	1			_									
Water Used Per Bag	GAL.			7	Length 2	NITE SEAL 2.5 Pellets ted Zone							
SECONDARY FIL	TER PACK LENGTH												
0.8	FT.												
DEPTH TO TOP OF FILTER PACK		were product of the control of the c			SCREEI Screen D Screen Le Diameter Depth To	iameter ength Of Drill Hole	9.8	N. FT. N.					
LENGTH OF PRIM	MARY FILTER PACK	200 - 200 -			1.76	N MATERIAL							
12.5	57 FT.				☐ Steel	☑ Thermopla	astic (PVC)						
	_	Andrew Control of the	marid .		- Julei			ТО	TAL DEP	TH: F		ing Log At	ttached
	submit additional as-built diagra iameter and grout used.	ms showing	well con	structio	n details	including ty	pe and siz		ATIC WA . 65	TER LEVEL FT		NSTALLE No	ED .
I hereby certify t	hat the monitoring well herein	described v	vas cons	structed	in acco	rdance with	Missouri I	Departme	nt of Na	atural Res	ources re	quirem	ents.
MONITORING	INSTALLATION CONTRACTOR		PERMIT N	JMBER	DATE Q_2	8-17		NG WELL IN CE (IF APPI		TION CONTR	ACTOR	PERMIT	NUMBER
1	\checkmark		4398		00	11	1						

415 (8-16) SEND COMPLETED FORM ALONG WITH \$100 CERTIFICATION FEE TO: MISSOURI DEPARTMENT OF NATURAL RESOURCES, MISSOURI GEOLOGICAL SURVEY, WELLHEAD PROTECTION SECTION, PO BOX 250, ROLLA, MO 65402 PHONE: 573-368-2165 FAX: 573-368-2317 EMAIL: welldrillers@dnr.mo.gov RECORD (AND FEE) MAY BE SUBMITTED ONLINE: dnr.mo.gov/mowells

APPENDIX H STATISTICAL ANALYSIS PLAN





STATISTICAL ANALYSIS PLAN

Prepared in accordance with the United States Environmental Protection Agencies Coal Combustion Rule, part 40 CFR 257.93 for Ameren Missouri's SCPB Surface Impoundment at the Sioux Energy Center, St. Charles County, Missouri



Submitted To: Ameren Missouri

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EXECUTIVE SUMMARY

This Statistical Analysis Plan (SAP) was developed to meet the requirements of United States Environmental Protection Agency (USEPA) 40 CFR Part 257 "Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities; Final Rule" (the Rule or CCR Rule). The Rule requires owners or operators of an existing Coal Combustion Residuals (CCR) Surface Impoundment to install a groundwater monitoring system and develop a sampling and analysis program (§§ 257.90 - 257.94). Ameren Missouri has determined that the SCPB (Fly Ash) Surface Impoundment at the Sioux Energy Center in St. Charles County, Missouri is subject to the requirements of the CCR Rule.

As a part of the groundwater sampling and analysis requirements of the Rule, statistical methods as described in Section §257.93(f) of the Rule need to be implemented to statistically evaluate groundwater quality. The selected statistical method must then be certified by a qualified professional engineer stating that the statistical method is appropriate for evaluating the groundwater monitoring data for the CCR Unit. Detailed descriptions of the acceptable statistical data methods are provided in the USEPA's *Statistical Analysis of Groundwater Data at RCRA Facilities, Unified Guidance* (USEPA, 2009) (Unified Guidance). The Unified Guidance is also recommended in the CCR Rule to be used for guidance in the selection of the appropriate statistical evaluation method.

This SAP details the statistical procedures to be used to establish background conditions, to implement detection monitoring, and to implement assessment monitoring (if needed) for Ameren Missouri at the above mentioned CCR Unit. Detailed information on collection, sampling techniques, preservation, etc. are provided in the Groundwater Monitoring Plan (GMP) for the CCR Unit specified above. This SAP is a companion documents to the GMP and assumes that data analyzed by the procedures described in this SAP are from samples that were collected in accordance with the GMP.

This SAP was prepared by Golder Associates, Inc. (Golder) on behalf of Ameren in order to document appropriate method of groundwater data evaluation in compliance with CCR Rules. The methods and groundwater data evaluation techniques used in this SAP are appropriate for evaluation of the groundwater monitoring data for the above mentioned CCR Unit and are in compliance with performance standards outlined in Section §257.93(g) of the CCR Rule.



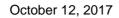


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Physical Independence Confidence Interval Method Selection Table 2



1.0 BASELINE STATISTICS

This section discusses the procedures, methods, and processes that will be implemented as part of the Detection Monitoring statistical evaluation. Detection Monitoring will begin after eight rounds of sampling are completed at each monitoring well for each of the Appendix III and Appendix IV parameters. This background monitoring period provides baseline data for each monitoring well which can be used as the basis of the statistical evaluation. Detection monitoring will be completed on a semiannual basis unless adequate groundwater flow is not available for semiannual sampling and proper documentation as outlined in §257.94(d) is completed. Detection monitoring will analyze for Appendix III analytes as outlined in the Groundwater Monitoring Plan for this CCR Unit.

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1.1 STATISTICAL DATA PREPARATION AND INITIAL REVIEW

Many of the statistical comparison tests used in detection, and assessment monitoring require various analyses to be completed prior to the data being used for the calculation of statistical limits. This section discusses the methods and procedures for completing this initial review of the data. The analyses required include testing for statistical independence, physical independence, and procedures to evaluate potential outliers.

1.1.1 Physical and Statistical Independence of Groundwater Samples

Detection, and Assessment Monitoring statistical evaluations assume that background and downgradient sampling results are statistically independent. The Unified Guidance states that "Physical independence of samples does not guarantee statistical independence, but it increases the likelihood of statistical independence." (Section 14.1, Unified Guidance). Physical independence is most likely achieved when consecutive groundwater samples are collected from independent volumes of water within a given aquifer zone. Using the Darcy Equation, minimum time intervals between sampling events can be calculated in order to confirm the minimum time interval for groundwater to travel through the borehole is less than the time between sampling events (**Table 1, Physical Independence**). This minimum time can be calculated as displayed in Section 14.3.2 of the Unified Guidance.



11.0

Table 1: Physical Independence										
	Hydraulic	Average Hydraulic								
Well ID	Conductivity	Gradient	Effective Porosity	Well Bore Volume	Minimum Time					
Symbol	K	I	n	D	T_{min}					
Units	Feet/Day	Feet/Foot	%	Feet	Days					
LMW-1S	31	0.0003	0.35	0.5	18.6					
LMW-2S	56	0.0003	0.35	0.5	10.4					
LMW-3S	35	0.0003	0.35	0.5	16.5					
LMW-4S	28	0.0003	0.35	0.5	20.8					
LMW-5S	56	0.0003	0.35	0.5	10.4					
LMW-6S	56	0.0003	0.35	0.5	10.4					
LMW-7S	45	0.0003	0.35	0.5	12.9					
LMW-8S	75	0.0003	0.35	0.5	7.8					
LMW-9S	22	0.0003	0.35	0.5	26.0					
BMW-1S	16	0.0003	0.35	0.5	37.2					

Table 1: Physical Independence

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Notes:

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BMW-3S

Average hydraulic gradient and effective porosity taken from table 2 in the Groundwater Monitoring Plan (GMP)

0.35

0.5

- Hydraulic Conductivity taken from table 3 of the Groundwater Monitoring Plan (GMP)
- Calculation completed using the Darcy Equation as outlined in section 14.3.2 of the Unified Guidance.

1.1.2 Data Review - Testing For Outliers

Careful review of the data is critical for verifying that there is an accurate representation of the groundwater conditions. Early identification of anomalous data (outliers) helps play a key role in a successful SAP. Possible causes for outliers include:

- Sampling error or field contamination;
- Analytical errors or laboratory contamination;

0.0003

- Recording or transcription errors;
- Faulty sample preparation, preservation, or shelf-life exceedance; or
- Extreme, but accurately detected environmental conditions (e.g., spills, migration from the facility).

The following sections outline a few graphical and statistical tests that should be completed prior to the data being used to calculate statistical limits.

1.1.2.1 Time Series Plots

Time Series plots are a quick and simple method to check for possible outliers. Time series plots should be generated with the concentration of the analyte on the Y-axis and the sample date (time) on the X-axis. If any data points look to be potential outliers, the data should be flagged and further evaluated as described in Section 1.1.2.2 below.



1.1.2.2 Dixon's and Rosner's Tests

If graphical methods demonstrate that potential outliers exist, further investigation of these data points can be completed using Dixon's test for datasets with fewer than 25 samples and Rosner's test with datasets greater than 20 samples. Formal testing should only be performed if an observation seems particularly high compared to the rest of the dataset. If statistical testing is to be completed to whether an outlier exists, it should be cautioned that these outlier tests assume that the rest of the data (other than the outlier) are normally distributed. Additionally, because log-normally distributed data often contain one or more values that appear high relative to the rest, it is recommended that the outlier test be run on the transformed values instead of their original observations. This way, one can avoid classifying a high log-normal measurement as an outlier just because the test assumptions were violated. Most groundwater statistical packages can complete Dixon's and Rosner's tests and more information about Dixon's and Rosner's tests is provided in Sections 12.3 and 12.4 of the Unified Guidance. If the test designates an observation as a statistical outlier, the source of the abnormal measurement should be investigated. In general, if a data point is found to be a statistical outlier, it should not be used for statistical evaluation. However, outlier removal should be performed carefully, and typically only when a specific cause for the outlier can be identified.

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In some cases where a specific cause for an outlier cannot be identified, professional judgment can be used to determine whether the outlier significantly affects the statistical results to the extent that removal is deemed necessary. If an outlier value with much higher concentration than other background observations is not removed from background prior to statistical testing, it will tend to increase both the background sample mean and standard deviation. In turn, this may substantially raise the magnitude of the prediction limit or control limit calculated from that data set. Thus, experience shows that it is a good practice to remove obvious outliers from the database even when independent evidence of the source of the outlier does not exist. The removal of outliers tends to normalize the data and therefore produce a more robust statistical limit. Outlier removal also tends to produces a more conservative statistical limit, since the data variability is decreased, thereby decreasing the standard deviation.

1.2 Upgradient Monitoring Wells

Following the identification and removal of outliers, the upgradient data are further reviewed to determine appropriate methods for statistical evaluation to maintain adequate statistical power while minimizing the chance of false positives. The following sections describe the procedures and methods that should be used, based on the background dataset, to compare the background datasets, to calculate the data distribution, to handle non-detect (ND) data, and to select appropriate statistical evaluation methods (interwell vs intrawell).

1.2.1 Calculate for Mean and Standard Deviation

Following outlier removal, initial summary statistics including mean and standard deviation should be calculated for the background monitoring well datasets. While these summary statistics are easily



completed in many groundwater statistical software packages, it is important to account for values that have low or zero values as described below.

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1.2.1.1 Reporting of Low and Zero Values

1.2.1.1.1 Estimated Values (J Flag)

Estimated values are values that have a concentration between the method detection limit (MDL¹) and the practical quantitation limit (PQL²) for any given compound. These values are typically displayed with a J flag in laboratory report packages and are often referred to as "J-values". In most cases, The Unified Guidance recommends using the estimated value provided for statistical evaluation. Estimated values are typically used because the accuracy and power of most statistical evaluations lose power as the percentage of non-detects increases. While they are below the PQL, estimated values are considered detectable concentrations for statistical calculations, which has the effect of lowering the percentage of non-detects.

This "rule" should be applied with care, as there is an exception. Estimated values are not considered detectable concentrations if all values for a single constituent are less than the PQL. This is discussed in more detail in Section 1.3.5 of this document.

1.2.1.1.2 Non-Detects Values (ND)

Non-Detect Values (ND) are concentrations that were not detected at a concentration above the MDL. ND values are typically displayed with a "U" or "ND" flag in laboratory data report packages. The following approaches for managing ND values are based on recommendations in the Unified Guidance and are applicable for use with the statistical evaluation procedures that will be further discussed and used in this SAP (prediction intervals, confidence intervals, and tolerance intervals):

- If <15% ND, substitute ½ the PQL;
- If between 15% to 50% ND, use the Kaplan-Meier or robust regression on ordered statistics to estimate the mean and standard deviation;
- If >50% but less than 100% ND, use a non-parametric test; or
- If 100% of values are less than the PQL, use the Double Quantification Rule.

1.2.2 Data Distribution

Statistical evaluations of groundwater data require an understanding of the data distribution for each analyte in each monitoring well. Data typically fall into one of the following distributions:

² PQL = minimum concentration of an analyte (substance) that can be measured with a high degree of confidence that the analyte is present at or above that concentration (typically 5-10x higher than the MDL).



¹ MDL = lowest level of an analyte (substance) that the laboratory can reliably detect with calibrated instrumentation; generally based on results of an annual "MDL study" performed in accordance with 40 CFR Part 136, Appendix B; MDLs are generally set using laboratory grade deionized water spiked with a known concentration and thus do not account for effects of matrix interference inherent in typical groundwaters.



Normal distribution - Sometimes referred to as Gaussian distribution, a normal distribution is a common continuous distribution where data form a symmetrical bellshaped curve around a mean. Normally distributed data are tested using parametric methods.

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- Transformed-normal distribution Similar to a normal distribution, however, data are asymmetrical until transformation is applied to all data which then causes it to form a bell-curve. Transformed-normal data distributions are also tested use parametric methods.
- Non-Normal Distribution When the data are not or cannot be transformed into a symmetrical distribution. Non-normal data distributions are tested using Nonparametric methods.

Testing for data distributions can be completed in several different ways including the skewness coefficient, probability plots with Filliben's test, or the Shapiro-Wilk/Shapiro-Francia Test. All of these methods may be employed, however, the Shapiro-Wilk and Shapiro-Francia tests are generally considered the best method according to the Unified Guidance. The Shapiro-Wilk test is best for sample sizes under 50 while the Shapiro-Francia test is best with larger datasets of 50 or more observations. Most groundwater statistical software packages can complete both Shapiro-Wilk and Shapiro-Francia tests and a detailed discussion of the testing procedures is provided in Section 10.5.1 of the Unified Guidance.

Based on the outcome of the data distribution testing, data will use either Parametric or Non-parametric tests. It is important to note that non-parametric testing usually requires larger datasets in order to minimize the Site Wide False Positive Rate (SWFPR) therefore when the raw data are not normally distributed, a transformed-normal distribution is preferred when possible.

1.2.3 Temporal Trend

Most statistical tests assume that the sample data are statistically independent and identically distributed. Therefore, samples collected over a period of time should not exhibit a time dependence. A time dependence could include the presence of trends or cyclical patterns when observations are graphed on a time series plot. Trend analysis methodologies test to see whether the dataset displays an increasing, decreasing, or seasonal trend. A statistically significant increasing or decreasing trend could indicate a release from the CCR unit (or alternative source) and further investigation of the cause of the trend may be necessary.

If a trend is suspected, a Theil-Sen trend line should be used to estimate slope and the Mann-Kendall Trend Test should be used to evaluate the slope significance (Chapter 14, Unified Guidance). If a statistically significant trend is reported, based on a Sen's slope/Mann-Kendall trend test, the source of the trend should be investigated. If the trend can be shown to be a result of an upgradient or off-site source, the data can be de-trended and used to calculated statistical limits. De-trending can be accomplished by computing a linear regression on the data (see Section 17.3.1 of the Unified Guidance) and then using the regression residuals instead of the original measurements in subsequent statistical analysis.



1.2.4 Comparing Background Datasets (Spatial Variation)

After physical independence, outlier, trend, and summary statistical testing is completed, the datasets from the background monitoring wells should be compared to one another for each individual constituent. The comparison of these background datasets is useful for determining whether spatial variability exists in the background dataset, and can also be used to decide whether an interwell or intrawell approach is more appropriate for statistical evaluation.

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Box and whisker plots can be used to perform side by side comparison for each well and can be completed for each individual analyte to determine if the variance is equal across the background datasets. If the box plots appear to be staggered and do not appear to be from the same population (same variance) then a Lavene's test using an α of 0.01 should be used as a check to determine if the background datasets have spatial variation. Testing methods and procedures are provided in Section 11.2 of the Unified Guidance.

The preferred method for comparing background datasets is a Mann-Whitney (or Wilcoxon Rank Sum) Test, which evaluates the ranked medians of both the historical and new dataset populations. An α of 0.05 should be used for this evaluation. After calculation, if the Mann-Whitney statistic does not exceed the critical point, the test assumes that the two data populations have equal medians, and therefore are likely from the same statistical distribution. The testing methods and procedures for this analysis are provided in Section 16.2 of the Unified Guidance.

If spatial variability is identified within the background dataset, an additional investigation may be needed in order to confirm that the variability is not caused by impacts from the CCR unit. If there is spatial variability and it is not caused by impacts from the CCR unit, then an intrawell approach to statistical evaluation may be appropriate.

1.3 Compliance Monitoring Wells and Statistically Significant Increases

After completing the previously described analyses of the background data, a statistical evaluation of the compliance monitoring data should be completed to determine if there are any Statistically Significant Increases³ (SSIs) that could trigger assessment monitoring. Section §257.93(F) of the CCR Rule specifies the list of methods that can be used for statistical evaluation. These specific methods to be used for statistical evaluation of data from the RMSGS are detailed below. Further, the Unified Guidance is recommended in the CCR Rule to be used for guidance in the selection of the appropriate statistical evaluation method. This section provides a guide to choosing the correct statistical evaluation to analyze the compliance wells for SSIs, the basic principles of each method, and response activities for identified SSIs.

³ SSI = a verified statistical exceedance; under compliance monitoring programs, the first time an exceedance is reported it is an initial statistical exceedance and is only considered an SSI if a confirmatory result verifies the initial exceedance.



1.3.1 Interwell vs Intrawell Statistical Analysis

1.3.1.1 Interwell Statistical Analysis

An interwell statistical evaluation compares the groundwater results from the compliance (downgradient) monitoring wells to a pool of background (typically upgradient) monitoring well results. If results from the downgradient wells are statistically higher (or significant) than the background dataset then an exceedance is triggered. This upgradient verses downgradient method typically assumes that:

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- Naturally, un-impacted groundwater characteristics in the compliance monitoring wells is comparable and equal on average to the background monitoring wells.
- Upgradient and downgradient monitoring well samples are drawn from the same aquifer and are screened in essentially the same hydrostratigraphic position.
- The aquifer unit is homogeneous and isotropic.
- Groundwater flow is in a definable pathway from upgradient to downgradient wells beneath the CCR Unit.

An interwell approach is preferable for statistical evaluation because it compares data to a background dataset that is not influenced by the CCR Unit. Interwell methods should be used with two exceptions: (1) there are significant differences in the datasets of the background wells (as indicated by methods described in Section 1.2.4) or (2) it can be demonstrated that groundwater geochemistry at all wells (background and compliance) is not impacted by the CCR Unit.

1.3.1.2 Intrawell Statistical Analysis

An intrawell statistical evaluation compares the groundwater results from a compliance monitoring well to historical data collected from that same compliance monitoring well. This method can be used for CCR monitoring when groundwater data from the background monitoring wells is statistically different than that of the compliance monitoring wells or when it can be shown that there is no impact from the CCR Unit in either upgradient or downgradient/compliance wells.

1.3.2 Statistical Power

As discussed above, one of the primary goals of the selection of a proper statistical evaluation method is to limit the potential for results to falsely trigger a SSI while also maintaining sufficient statistical power to detect a true SSI. Falsely triggering a SSI when no release from the CCR unit has occurred is referred to as a false positive. The False Positive Rate (FPR), typically denoted by the Greek letter α , is also known as the "significance level". The FPR is the probability that a future compliance observation will be declared to be from a different statistical distribution than the background data. If the FPR is set too high, it can lead to the conclusion that there is evidence of impact when none exists. Conversely, if the FPR is set too low, it can lead to a false conclusion that no contamination exists, when it actually does exist (also known as a "false negative"). Ultimately, the ability to accurately identify SSIs depends on the selection of an appropriate FPR, which is referred to as the statistical power. FPRs are set for each parameter (or for each



parameter in each well for intrawell analysis). However, statistical analysis programs and the resulting decision making do not depend on each individual measurement/comparison error rates, but are dependent on the collective error rate from all of the individual comparisons. When the individual FPRs are integrated over the entire statistical monitoring program, it is referred to as the site-wide false positive rate (SWFPR), which is a better measure of the ability of the entire statistical program to detect false positive observations.

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1.3.2.1 Site-Wide False Positive Rate

For CCR monitoring, detection monitoring events are based on multiple comparisons, which include the seven (7) Appendix III parameters, at each compliance monitoring well. The SWFPR can be calculated based on several input parameters, including the assumed FPR, the number of downgradient monitoring wells (n), the number of parameters, and the number of statistical comparisons events in a given year for the CCR Unit. The Unified Guidance recommends that a statistical evaluation program be designed with an annual, cumulative SWFPR of approximately 10%.

The Unified Guidance recommends measuring statistical power using power curves which display the probability that an individual comparison will detect a concentration increase relative to background results. After determining the statistical method based on the background data, a power curve can be generated in order to determine the statistical power of the compliance monitoring program. The methods and procedures for calculating the SWFPR are described in Section 6.2.2 of the Unified Guidance.

1.3.2.2 Verification Sampling

Verification Sampling is an important aspect of the SAP as it improves statistical power while maintaining the SWFPR. Most statistical evaluations incorporate verification sampling mathematically into their determination of the SWFPR. Verification sampling is typically completed at a 1 of 2 pass strategy. As described above if an initial statistical exceedance is reported, then verification sampling will be performed to confirm the initial exceedance. Verification samples should be collected on a schedule that allows for physical independence of the samples. In a 1 of 2 pass strategy, if the concentration of the verification sample is less than the calculated compliance limit, then no SSI is triggered. If the initial and subsequent verification observation are above the calculated compliance limit, a SSI is triggered.

Due to the time constraints for reporting put forth in the CCR rule, it is suggested that verification sampling not be completed at the next regularly scheduled sampling event, but instead be collected prior to the next sampling event. Verification sampling within 90 days (assuming a 1 of 2 pass verification sampling strategy) will typically allow sufficient time to complete laboratory and statistical analysis in accordance with the timeframes set forth in the CCR Rules.



1.3.3 Statistical Evaluation Methods

As outlined above, the CCR rule list 5 possible methods for statistical evaluation. The different methods that can be employed for CCR monitoring as outlined in §257.93(F) are:

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- §257.93(F)(1) "A parametric analysis of variance followed by multiple comparison procedures to identify statistically significant evidence of contamination. The method must include estimation and testing of the contrasts between each compliance well's mean and the background mean levels for each constituent."
- §257.93(F)(2) "An analysis of variance based on ranks followed by multiple comparison procedures to identify statistically significant evidence of contamination. The method must include estimation and testing of the contrasts between each compliance well's median and the background median levels for each constituent."
- §257.93(F)(3) "A tolerance or prediction interval procedure, in which an interval for each constituent is established from the distribution of the background data and the level of each constituent in each compliance well is compared to the upper tolerance or prediction limit."
- §257.93(F)(4) "A control chart approach that gives control limits for each constituent."
- **§257.93(F)(5)** "Another statistical test method that meets the performance standards of paragraph (g) of this section."

1.3.4 Prediction Intervals

Section §257.93(F)(3) outlines using prediction intervals or tolerance intervals for statistical evaluation. Based on recommendation from the Unified Guidance, prediction limits are the preferred method for calculating detection monitoring compliance limits and will be used to calculate compliance limits for the seven Appendix III constituents. In addition, the Unified Guidance suggests using prediction limits with verification sampling (Chapter 19 of the Unified Guidance), because prediction limits help to maintain low SWFPR while still providing high statistical power. Tolerance intervals, which are a backward looking procedure, should not be used for detection monitoring, but will likely be used in assessment monitoring, as further described in Section 2.0 below. If, at any point in the future, a different statistical method becomes more applicable to the site conditions, this document may be modified to include that method as recommended by the Unified Guidance.

Prediction interval methods can be used for parametric and non-parametric datasets as well as for intrawell or interwell statistical analysis. Prediction limits use background data from either background monitoring wells for interwell analysis or from historical data for intrawell analysis calculate a concentration that represents an upper limit of expected future concentrations for a particular population. In contrast to tolerance limits, prediction intervals are a forward looking, predictive analysis, which incorporate uncertainty in future measurements, and are thus the most appropriate method for detection monitoring programs. Typically, a one-sided upper prediction limit is used to evaluate detection monitoring observations. Observations must be lower than the prediction limit (or within the upper and lower prediction limits for pH) to be considered "in control". Parametric methods are generally preferred over non-parametric methods, because they result in lower SWFPRs and higher statistical power.





For detection monitoring, if parametric testing is required, the procedures outlined in Section 19.3.1 of the Unified Guidance should be used to calculate prediction limits for the statistical analysis. If non-parametric testing is required, the procedures outlined in Section 19.4.1 of the Unified Guidance should be used to calculate prediction limits. Most groundwater statistical software includes algorithms for calculating either parametric or non-parametric prediction limits.

1.3.5 Double Quantification Rule

In situations where the entire background dataset is reported as ND or Estimated (J-flag), the Double Quantification Rule (DQR) will be used to supplement the prediction limit analyses. Generally, the Appendix III constituents occur at detectable concentrations in natural groundwater; however, if ND results are encountered for a given constituent, the DQR can be implemented. A demonstration that this statistical evaluation is as least as effective as any other test and results as described in §257.93(f)(5) can be made. The DQR is recommended by the Unified Guidance as a supplement to prediction limits because it reduces the number of non-detects used for statistical analysis and provides a lower SWFPR while maintaining statistical power.

Under the DQR, a SSI is triggered if a compliance well observation is higher than the reporting limit (RL)/PQL in either (1) both a detection monitoring sample and its verification resample, or (2) two consecutive sampling events in a program were resampling is not utilized.

1.4 Responding to SSIs

If the statistical evaluation for an Appendix III analyte triggers a SSI, the data must be evaluated to determine if the cause of the SSI is due to a release from the CCR Unit or from an alternative source. Possible alternative sources may include laboratory causes, sampling causes, statistical evaluation causes, or natural variation. If the SSI can be attributed to one of these sources and the SSI was not caused by the CCR Unit, an alternate source demonstration (ASD) can be completed. An ASD must be certified by a qualified professional engineer and completed in writing within 90 days of completing the statistical evaluation for a particular sampling event. If the SSI cannot be attributed to an alternative source and is from the CCR Unit, then Assessment Monitoring is triggered.

1.5 Updating Background Values

The Unified Guidance suggests that updating statistical limits should only be completed after a minimum of 4 to 8 new measurements are available (i.e., every 2 to 4 years of semiannual monitoring, assuming no verification sampling). The periodic update of background, during which additional data are incorporated into the background, improves statistical power and accuracy by providing a more conservative estimate of the true background population. Prior to incorporating new data into the background dataset, a test should be performed to demonstrate that the "new data" are from the same statistical population as the existing





background results. Below are three methods that can be used in determining if the "new" data should be included in the background:

- Time Series Graphs As described in Section 1.1.2.1, time series graphs can be used as a qualitative test to assist with the determination whether a new group of data match the historical data or if there is a concentration trend that could be indicative of a release or evolving groundwater conditions.
- Box-Whisker plots can also be used to determine whether or not the datasets are similar.
- Mann-Whitney (or Wilcoxon Rank) Test Used to evaluate the ranked medians of both the historical and new dataset populations. An α of 0.05 should be used for this evaluation. After calculation, if the Mann-Whitney statistic does not exceed the critical point, the test assumes that the two data populations have equal medians, and therefore are likely similar.

Ultimately, the Mann-Whitney (Wilcoxon Rank Sum) Test is the statistical test that is used to determine whether new observations should be included in the background dataset. It is important to note that a difference in background datasets does not automatically prevent the new data from being used; however, if differences are noted, a review of the new data will be conducted to determine if the noted difference is a result of a change in the natural conditions of the groundwater or if it is the result of a potential release from the CCR Unit. If the new data are included in the background dataset, the prediction limits will be recalculated, as described in Section 1.3.4 above.





2.0 ASSESSMENT MONITORING STATISTICAL EVALUATION

This section discusses the procedures, methods, and processes that will be implemented as part of the assessment monitoring statistical evaluation, if required. Assessment monitoring will be initiated if a SSI is triggered during detection monitoring. As per the CCR Rule in Section §257.95(b), assessment monitoring must be initiated within 90 days of identifying an SSI (not the sample event which provided the data that resulted in the SSI). This 90-day period includes sampling the groundwater monitoring network for the Appendix IV constituents. Following the initial sampling event for all Appendix IV constituents, the monitoring network is then sampled again within 90 days of receiving the results from the initial Appendix IV sampling event. Following these initial assessment monitoring events, assessment monitoring is performed on a semiannual basis. During one of the two semiannual events, the full list of Appendix IV constituents must be tested. During the second assessment monitoring event of each year, only the Appendix IV constituents that are detected during the previous semiannual event are required to be Assessment monitoring is terminated if concentrations for all Appendix III and Appendix IV monitored. constituents in all compliance wells are statistically lower than background for two consecutive sampling events (§257.95(e)). The following sections discuss the procedures, methods, and processes that will be implemented as part of the assessment monitoring statistical evaluation. As discussed in Section 1.1 of this document, many of the statistical comparisons used in assessment monitoring require various analyses to be completed prior to the data being accepted into the statistical evaluation. Before using the results from assessment monitoring, the steps outlined in Sections 1.1 and 1.2 will be completed. Please refer to those sections for descriptions on the methods and techniques required to complete these analyses.

2.1 Establishing a Ground Water Protection Standard (GWPS)

Following the removal of outliers and the performance of general statistics described in Sections 1.1 and 1.2, GWPS will be developed for use in the assessment monitoring program. The GWPS is a key element to the assessment monitoring process. GWPS must be generated for each of the detected Appendix IV analytes. If interwell methods are utilized (preferred method), a site-wide GWPS will be generated for each analyte based on Appendix IV results reported for background/hydraulically upgradient wells. If intrawell methods are utilized, a well specific GWPS will be generated for each analyte.

For Appendix IV parameters that have a maximum contaminant level (MCL), as established by the United States Environmental Protection Agency, the GWPS is set equal to the MCL. For those constituents whose background concentration are greater than the MCL, the GWPS will be calculated from the background data. Finally, for those constituents that do not have an established MCL, the GWPS will be calculated. Several analytes (cobalt, lead, lithium, and molybdenum) do not have MCLs established and therefore the GWPS must be calculated based on their background concentrations.



2.1.1 Maximum Contaminant Level (MCL) Based GWPS

Many of the Appendix IV analytes have USEPA MCL levels. As specified in the CCR Rule in Section §257.95(b), the GWPS must either be the MCL, or a limit based on background data, whichever is greater. This section describes the methods to be used for statistical analysis when the MCL is to be used as the GWPS.

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For Assessment Monitoring, the Unified Guidance recommends the confidence interval method to evaluate for potential exceedances, which are referred to as "statistically significant levels" (SSLs) (Chapter 21, Unified Guidance). Using confidence intervals, SSLs are identified by comparing the calculated confidence interval against the GWPS. A confidence interval statistically defines the upper and lower bounds of a specified population within a stipulated level of significance. Confidence intervals are required to be calculated based on a minimum of 4 independent observations, but a more representative confidence interval can be developed when all of the available data are utilized.

The specific type of confidence interval should be based the attributes of the data being analyzed, including: (1) the data distribution, (2) the detection frequency, and (3) potential trends in the data. Table 1 below is based on Table 4-4 from the Electric Power Research Institute's *Groundwater Monitoring Guidance for the Coal Combustion Residual Rule* (2015), which displays the criteria for selecting an appropriate confidence interval. The method and procedure for calculating the Upper Confidence Limit (UCL) and Lower Confidence Limit (LCL) is provided in the section reference from the Unified Guidance, which is listed in the last column of Table 1, below.



Table 2- Confidence Interval Method Selection

Data Distribution	Non-detect Frequency	Data Trend	Confidence Interval Method
Normal	Low	Stable	Confidence Interval Around Normal Mean (Section 21.1.1)
Transformed Normal (Log-Normal)	Low	Stable	Confidence Interval Around Lognormal Arithmetic Mean (Section 21.1.3)
Non-normal	N/A	Stable	Nonparametric Confidence Interval Around Median (Section 21.2)
Cannot Be Determined	High	Stable	Nonparametric Confidence Interval Around Median (Section 21.2)
Residuals After Subtracting Trend are Normal (with equal variance)	Low	Trend	Confidence Band Around Linear Regression (Section 21.3.1)
Residuals after Subtracting Trend are Non-Normal	Low	Trend	Confidence Band Around Theil-Sen Line (Section 21.3.2)

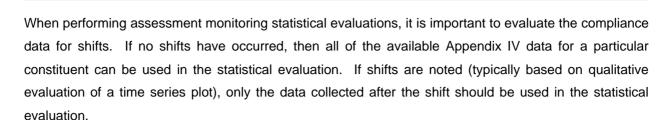
14

In an assessment monitoring program the LCL is of prime interest. If the LCL exceeds the GWPS, there is statistical evidence that a SSL has been triggered. An initial SSL should be confirmed by verification sampling. If only the UCL exceeds the GWPS while the LCL is below the GWPS, the test is considered inconclusive and the Unified Guidance recommends that this situation be interpreted as "in compliance". If both the UCL and the LCL are below the GPWS, the data are also "in compliance" with the GWPS.

It is important to note that a slightly different set of criteria are used to determine whether assessment monitoring can be terminated. Additional discussion of the criteria used for exiting assessment monitoring and returning to detection monitoring is provided below in Section 2.2.

During Assessment Monitoring, a per test FPR (α) of 0.05 will be used as an initial error level for calculating the two-tailed confidence intervals for the compliance wells (which actually means 2.5% FPR per tail). In some cases based on recommendations from the Unified Guidance, it is appropriate to adjust the FPR of the confidence interval based on the number of data points available as well as the distribution of the data being evaluated. If deemed necessary based on recommendations from the Unified Guidance, an approach is provided in Section 22 of the Unified Guidance for determining an appropriate per test FPR based on the data characteristics.





2.1.2 Non-MCL Based GWPS

Background or historical concentration limits should be assessed using the following techniques for all Appendix IV analytes. These concentration limits should then be compared with the MCL, if available, and the higher of these two values will be used as the GWPS.

The Unified Guidance provides two acceptable approaches for establishing a non-MCL based GWPS (unless all values are ND, in which case the Double Quantification Rule as described above in Section 1.3.5 should be used). The two methods include the tolerance interval approach or the prediction interval approach.

2.1.2.1 Tolerance Interval Approach

If the background dataset is normally or transformed normally distributed, the Unified Guidance recommends Tolerance Intervals over the Prediction Intervals for establishing a GWPS. The GWPS should be based on a 95 percent coverage/95 percent confidence tolerance interval. If the background data are non-normal (even after transformation), then a large number of background observations are required to calculate a non-parametric tolerance interval (typically a minimum of 60 background observations are required to meet these requirements). If there is an insufficient number of background observations to calculate a non-parametric tolerance interval, then a non-parametric Prediction Interval approach should be used, as described in Section 2.1.2.2 below.

The Upper Tolerance Limit (UTL) is calculated for each detected Appendix VI constituent. Tolerance Limits, as outlined in the Unified Guidance (Section 17.2), are a concentration limit that is designed to contain a pre-specified percentage of the dataset population. Two coefficients associated tolerance intervals are (1) the specified population proportion and (2) the statistical confidence. The coverage coefficient (γ), which is used to contain the population portion, and the tolerance coefficient (or confidence level (1- α)), which is used to set the confidence of the test. Typically, the UTL is calculated to have a coverage and confidence of 95%. When an MCL does not exist or the background concentrations are greater than the MCL, the calculated UTL for each constituent is used as the GWPS. The confidence interval for each compliance well is then compared with the GWPS.

In order to calculate a valid confidence interval, a minimum of four data points are necessary for each of the detected Appendix IV constituents in each compliance monitoring well (or four "new" assessment



monitoring observations in each well when intrawell statistical methods are employed). Using the Tolerance Interval Approach, a statistically significant level (SSL) is triggered when calculated lower confidence limit (LCL) for each compliance well is greater than the GWPS.

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Tolerance limits can be completed using both parametric (Section 17.2.1 of Unified Guidance) or nonparametric methods (Section 17.2.2 of Unified Guidance). However, as described above, the nonparametric method requires at least 60 background (or historical) measurements in order to achieve 95% confidence with 95% coverage. Tolerance Intervals can be calculated using most groundwater statistical software packages.

2.1.2.2 **Prediction Interval Approach**

If Tolerance Intervals cannot be used to calculate the GWPS (based on recommendation from the Unified Guidance, such as non-parametric datasets, ect.), then a Prediction Interval method should be used. This method is very similar to Section 1.3.4 of this document, however, for assessment monitoring, the Unified Guidance suggests using a prediction interval about a future mean for normally/transfomred-normally distributed datasets or a prediction interval about a future median for datasets with a high percent of ND or non-normally distributed data.

When using prediction intervals to calculate for a GWPS, a one-sided prediction interval is calculated using background (or historical) datasets based on a specified number of future comparisons - four future comparisons is typical. The Upper Prediction Limit that is calculated as a product of this method then becomes the GWPS, and is compared against the confidence interval for the compliance data, as described in Section 2.1.2.1, above. As also described above, if the LCL is greater than the calculated prediction limit then an SSL is triggered.

2.2 **Returning to Background Detection Monitoring**

As specified in 257.95(e) of the CCR Rule, in order to return to detection monitoring, the concentration of all constituents listed in Appendix III and Appendix IV must be shown to be at or below calculated "background (or historical) values" for two consecutive semiannual sampling events. This determination of background values is based on the statistical evaluation procedure established for detection monitoring. Therefore, if prediction limits (with the double quantification rule for analytes with all non-detects) are used for detection monitoring, prediction limits should be calculated and used for all Appendix III and IV analytes to determine when the monitoring program can return to Detection Monitoring. It is important to remember that Appendix IV constituents are only required to be sampled annually with only those Appendix IV constituents that are detected during the previous semiannual event being required to be analyzed during the second semiannual event of a given year. If statistical results demonstrate that concentrations for all constituents are below background levels for a particular event, all Appendix IV constituents should be sampled during the next event in order to achieve this goal of returning to Detection Monitoring. If this



statistical evaluation demonstrates that any of the Appendix III or Appendix IV are at a concentration above background levels, but no SSLs have been triggered, then the CCR unit will remain in assessment monitoring (257.95(f)).

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2.3 Response to a SSL

If the assessment monitoring statistical evaluation demonstrates that a SSL has been triggered, then the owner/operator of the CCR unit must complete the following four actions as described in 257.95(g):

- 1. Prepare a notification identifying the constituents in Appendix IV that have exceeded a CCR Unit specific GWPS. This notification must be placed in the facilities operating record within 30 days of identifying the SSL
- 2. Define the nature and extent of the release and any relevant site conditions that may affect the corrective action remedy that is ultimately selected. The characterization must be sufficient to support a complete and accurate assessment of the corrective measures necessary to effectively clean up releases from the CCR Unit and must include at least the following:
 - A. Installation of additional monitoring wells that are necessary to define the contaminant plume,
 - B. Collect data on the nature and estimated quantity of the material released,
 - C. Install and sample at least one additional monitoring well at the facility boundary in the direction of the contaminant plume migration,
- 3. Notify off-site property owners if the contamination plume has migrated offsite on to their property, and
- 4. If possible, provide an alternative source demonstration that determines that the SSL is not caused by a release at the facility within 90 days of completing the statistical evaluation. If no alternative source demonstration can be made and the plume is determined to have come from the CCR Unit then initiate corrective action.

Actions 1-3 must be completed regardless of whether or not an alternate source demonstration can be made.

2.4 **Updating Background Values**

The background for Assessment Monitoring Parameters should be updated using the same methods and techniques described in Section 1.5 for updating detection monitoring background data.



3.0 REFERENCES

EPRI. 2015. Groundwater Monitoring Guidance for the Coal Combustion Residual Rule. Electric Power Research Institute. November.

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- USEPA. 2009. Statistical Analysis of Groundwater Monitoring Data at RCRA Facilities, Unified Guidance.

 Office of Resource Conservation and Recovery Program Implementation and Information Division.

 March
- USEPA. 2015. Federal Register. Volume 80. No. 74. Friday April 17, 2015. Part II. Environmental Protection Agency. 40 CFR Parts 257 and 261. Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule/ [EPA-HQ-RCRA-2009-0640; FRL-9919-44-OSWER]. RIN-2050-AE81. April.



APPENDIX I EXAMPLE FIELD FORMS

Sheet	of
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	11000	Cities								
Project	Ref:									
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/lonitore	d By:			Date			Time			
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Develo	opmen	it / Purgir	ng Disc	charge	e Data					
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tart Purg	ing			Date			Time			
top Purg	ing			Date			Time			
Monitoring	9									
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft TOC)	Appearance of Water and Comme

Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft TOC)	Appearance of Water and Comments

GROUNDWATER SAMPLE COLLECTION FORM



Teflon

Hand Pump

Project Ref: _						Project No. :	
WEATHER CO	ONDITI	<u>IONS</u>					
Temperatur	re			_Weather			
Sample Loc					_ Sample No		
Sample Da							
-							
		Water Lev	el Before Purging	j:			
					 		
		Appearance	e of Sample:				
FIELD MEASU	JREME	<u>ENTS</u>					
<u>Para</u>	<u>ameter</u>	<u>Units</u>	<u>Measurement</u>	<u>Measurement</u>	Measurement	Measurement	<u>Sample</u>
	Time	hhmm					
Volume Disc	•	•		· 			
Snoo	•	Standard					
Spec. CondS/CM Turbidity NTU							
Tempe	•						
Dissolved O							
Redox Po	tential	+/- mV					
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LABORATOR	Y CON	<u>ITAINERS</u>					
Sub-			Analysis Requeste	d	Type and Size of	Filtered	Type of
Sample		-			Sample Container	(Yes or No)	Preservative
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2							
3							
4							
5							
6							
7							
8							
REMARKS:							
NA = Not appli	icable						
SAMPLING ME		··					
		PVC/PE	Perist	altic Pump	Air-Lift Pump		
		Stainless St		ersible Pump	Other		

Golder	ABOVE G	ROUND MONITORING	G WELL CONST	RUCTION LOG
PROJECT NAME:		Р	ROJECT NUMBER	:
SITE NAME:		L	OCATION:	
CLIENT:		S	URFACE ELEVATION	ON:
GEOLOGIST:		NORTHING:		EASTING:
DRILLER:		STATIC WATER LEVEL:		COMPLETION DATE:
DRILLING COMPANY:		D	RILLING METHOD	S:
STICK UP:		PROTECTION OF TYPE OF SCREE SIZE OF AMOUNT	FECTIVE CASING (yes IRAVEL OR SAND HOLE ID SURFACE ELEVATION FER OF RISER PIPE (in.) FER OF BOREHOLE (in.) RETE SEAL DEPTH (ft. b) IND AMOUNT OF ANNUAL FER SAND PACK DEPTH (ft. b) FESCREEN DEPTH (ft. b) OF SCREEN: IN SLOT SIZE (in.): IN SLOT SIZE (in.): IN OF SAND:	DN:
TOTAL DEPTH OF BOREHOLE (ft. bgs):		вотто	M OF WELL DEPTH (ft. M OF FILTER PACK (ft.	bgs):
ADDITIONAL NOTES:				
CHECKED BY:				PREPARED BY:



RECORD OF WATER LEVEL READINGS

Project N	lame:			Location:			Project No.:			
Borehole No.	Date	Time	Measuring Device / Serial No.	Measurement Point (M.P)	Water Level Below M.P.	Correction To Survey Mark	Survey Mark Elevation	Water Level Elevation	Ву	Comments

Sheet ___ of ___



Project Name:			Project No:								
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Instrument Details											
Instrument Name											
Serial No.											
Model No.											
Calibration Details											
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Calibration Standard											
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Calibration:	Date	Time	Calibration Standard Units:	Instrument Reading Units:							
				+							
Comments:											

Chain of Custody Record >>> Select a Laboratory <<< #N/A #N/A #N/A Regulatory Program: DW NPDES RCRA Other: #N/A COC No: **Client Contact** Project Manager: Site Contact: Date: Tel/Fax: Carrier: COCs Your Company Name here Lab Contact: of Address **Analysis Turnaround Time** Sampler: For Lab Use Only: WORKING DAYS City/State/Zip CALENDAR DAYS Walk-in Client: Phone (xxx) xxx-xxxx TAT if different from Below FAX Lab Sampling: (xxx) xxx-xxxx 2 weeks Project Name: 1 week Site: Job / SDG No.: 2 days P O # 1 day Sample Type Sample Sample # of (C=Comp, Sample Identification Date Time G=Grab) Matrix Cont. Sample Specific Notes: Preservation Used: 1= Ice, 2= HCI; 3= H2SO4; 4=HNO3; 5=NaOH; 6= Other Possible Hazard Identification: Sample Disposal (A fee may be assessed if samples are retained longer than 1 month) Are any samples from a listed EPA Hazardous Waste? Please List any EPA Waste Codes for the sample in the Comments Section if the lab is to dispose of the sample. Unknown Poison B Return to Client Archive for___ Non-Hazard Flammable Disposal by Lab Months Special Instructions/QC Requirements & Comments: **Custody Seals Intact:** Cooler Temp. (°C): Obs'd: Corr'd: Therm ID No.: Custody Seal No .: Yes No. Relinquished by: Date/Time: Received by: Company: Company: Date/Time: Relinguished by: Date/Time: Date/Time: Received by: Company: Company:

Date/Time:

Company:

Received in Laboratory by:

Company:

Relinquished by:

Date/Time:

Golder Associates

Field Boring Log

DEPTH HOLE PROJ. NO DEPTH SOIL DRILL GA INSP.		PROJECT DRILLING METHOD		BORING NO
DEPTH ROCK CORE WEATHER _		DRILLING COMPANY		SURFACE ELEV.
ABANDONMENT		DRILL RIG	DRILLER	DATUM
DEPTHS///		SAMPLER HAMMER TYPE	WT DROP	STARTED/
WATER LEVEL CAVE-IN DATE-TIME DEPTHS / /	NOTE /	HOLE LOCATION		COMPLETED/
(DELAYED) WATER LEVEL CAVE-IN DATE-TIME	NOTE			TIME DATE

SAMPLE TYPES	<u>ABBREVIATIONS</u>	ORDER OF DESCRIPTION	NON-COHESIVE SOILS	COHESIVE SOILS
A.S. AUGER SAMPLE C.S. CHUNK SAMPLE BL BLACK BLACK D.O. DRIVE OPEN (SPT) D.S. DENISON SAMPLE F.S. FOIL SAMPLE CIN CAVE-IN P.S. PITCHER SAMPLE S.C. SOIL CORE T.D. THIN-WALLED, OPEN T.P. THIN-WALLED, PISTON W.S. WASH SAMPLE W.S. WASH SAMPLE FL FINE FL FRAGMENTS TRACK TRACK TRACK TOTAL ANG ANGULAR BLACK BL	OG ORANGE WL WATER LEVEL ORG ORGANIC WH WEIGHT OF HAMMEI	SE SOLIC ROUP SYMBOL	RELATIVE DENSITY BLOWS	VERY SOFT

* NOTE SIZE	FRAG FRAGMENTS PP POO IGL GRAVEL PL PLA	STIC LI	IMIT Y	WR WEI	_OW	КОВО	H L 15	i) MOISTUR b) DENSITY	/CONSISTE	NCY	'			WET WITH FREE WATER W > PL CAN ROLL THREAD <2 mm					
ELEV.				SAMPLE				STITUE			HAVI								
DEPTH	LITHOLOGY	NO.	TYPE	DEPTH SPT N	/ BLOWS	REC ATT	GL PROPORTI	SD ON; SIZE, SHAPE PLASTICITY	CL/SI , GRADING;	CO or	MOIST. or W	DENS./	uscs	SAMPLE	DESCRIPTION	AND	DRILLING	NOTES	
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