



40 CFR PART 257 GROUNDWATER MONITORING PLAN

LCPB, Labadie Energy Center

Franklin County, Missouri, USA



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Table of Contents

I.0 INTRODUCTION	
2.0 SITE SETTING	2
2.1 Coal Combustion Residuals (CCR) LCPB Surface Impoundment	2
2.2 Geology	2
2.2.1 Physiographic Setting and Regional Geology	2
2.2.2 Local Geology	2
2.3 Site Hydrogeology	3
2.3.1 Uppermost Aquifer	3
2.3.2 Surface Water and Groundwater Elevations	4
2.3.2.1 CCR Surface Impoundment Water	4
2.3.2.2 Alluvial Aquifer	4
2.3.3 Groundwater Flow Directions	4
2.3.3.1 Horizontal Gradients	6
2.3.3.2 Vertical Gradients	ε
2.3.4 Hydraulic Conductivities	7
2.3.5 Porosity and Effective Porosity	8
3.0 GROUNDWATER MONITORING NETWORK	10
3.1 Monitoring Network Design Criteria	10
3.2 Design of the Groundwater Monitoring System	10
3.2.1 Preferential Migration Pathway Analysis	10
3.3 Groundwater Monitoring Well Placement	11
3.3.1 Background/Upgradient Monitoring Well Locations	11
3.3.2 Downgradient Monitoring Well Locations	11
3.3.3 Groundwater Monitoring Well Screen Intervals	11
1.0 INSTALLATION OF THE GROUNDWATER MONITORING SYSTEM	12
4.1 Drilling Methods and Monitoring Well Constructions	12
4.2 Groundwater Monitoring Well Development	12
4.3 Dedicated Pump Installation	12
4.4 Surveying and Well Registration	13
GROUNDWATER MONITORING PROGRAM	
5.1 Baseline Sampling Events	14
5.2 Detection Monitoring	14
5.2.1 Sampling Constituents and Monitoring Frequency	14
5.2.2 Data Evaluation and Response	14
5.3 Assessment Monitoring	14
5.3.1 Sampling Constituents and Monitoring Frequency	14

i





ii

5	3.2	Data Evaluation and Response	15
	5.3	3.2.1 Responding to a SSL	15
5	3.3	Annual Reporting Requirements	16
6.0	G	ROUNDWATER SAMPLING METHODOLOGY	17
6.1		Equipment Calibration	17
6.2		Monitoring Well Inspection	17
6.3		Water Level Measurement	17
6.4		Monitoring Well Purging	17
6	4.1	Low-Flow Sampling Technique	17
6	4.2	Traditional Purge Techniques	18
6	4.3	Low Yielding Wells	19
6.5		Sample Collection	19
6.6		Equipment Decontamination	19
6.7		Sample Preservation and Handling	19
6.8		Chain-of-Custody Program	20
6	8.1	Sample Labels	20
6	8.2	Sample Seal	20
6	8.3	Field Forms	20
6	8.4	Chain-of-Custody Record	21
6.9		Temperature Control and Sample Transportation	22
7.0	Α	NALYTICAL AND QUALITY CONTROL PROCEDURES	23
7.1		Data Quality Objectives	23
7.2		Quality Assurance/Quality Control Samples	24
7	2.1	Field Equipment Rinsate Blanks	24
7	2.2	Field Duplicates	24
7	2.3	Field Blank	24
7	2.4	Laboratory Quality Control Samples	24
8.0	D	ATA EVALUATION AND STATISTICAL ANALYSIS	26
8.1		Evaluation of Rate and Direction of Groundwater Flow	26
8.2		Data Validation	26
8.3		Statistical Analysis	26
9.0	R	EFERENCES	27



iii

List of Tables

Table 1	Groundwater Level Data
Table 2	Generalized Hydraulic Properties of Uppermost Aquifer
Table 3	CCR Monitoring Well Hydraulic Conductivities
Table 4	Monitoring Well Construction Details
Table 5	Groundwater Quality Monitoring Parameters
Table 6	Analytical Methods and Practical Quantitation Limits

List of Figures

Figure 1	Site Location Topographic Map
Figure 2	Site Location Aerial Map and Monitoring Well Locations
Figure 3	Generalized Cross-Section

List of Appendices

Appendix A Appendix B	CCR Monitoring Well Boring Logs Historic Potentiometric Surface Maps
Appendix C	Potentiometric Surface Maps From Background CCR Sampling Events
Appendix D	Grain Size Distribution
Appendix E	CCR Monitoring Well Construction Diagrams
Appendix F	Well Development Forms
Appendix G	CCR MDNR Well Certification Forms
Appendix H	Statistical Analysis Plan
Appendix I	Example Field Forms

1.0 INTRODUCTION

This Groundwater Monitoring Plan (GMP) presents information on the design of the groundwater monitoring system, groundwater sampling and analysis procedures, and groundwater statistical analysis methods for the Fly Ash Surface Impoundment (LCPB) at Ameren Missouri's (Ameren) Labadie Energy Center (Facility) in Franklin County, Missouri (see location on **Figure 1**). The LCPB is an on-site surface impoundment and manages Coal Combustion Residuals (CCR) from the Facility. The LCPB is approximately 75 acres in size and is located to the south and east of the generating plant.

1

This GMP was developed to meet the requirements of United States Environmental Protection Agency (USEPA) 40 CFR Part 257 "Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities; Final Rule" (the CCR Rule). The CCR Rule requires owners or operators of an existing CCR Surface Impoundment to install a groundwater monitoring system and develop a sampling and analysis program (§§ 257.90 - 257.94). Ameren Missouri has determined that the LCPB Surface Impoundment is subject to the requirements of the CCR Rule. For this GMP, the Labadie Energy Center generating plant is referred to as the LEC and the LEC and its surrounding facilities, including the Surface Impoundment, are referred to as the Facility or Site.

2.0 SITE SETTING

Ameren owns and operates the Facility in Franklin County, Missouri located approximately 35 miles west of downtown St. Louis. **Figure 1** depicts the location of the Facility and property boundaries referenced to local topographic features and the Missouri River. **Figure 2** depicts Facility structures relative to site property boundaries and the Missouri River. The Facility encompasses approximately 2,400 acres and is located within the Missouri River Valley. The Facility is bounded to the north by the Missouri River, to the west by Labadie Creek, to the northeast and east by agricultural land and to the south by a railroad line and bedrock bluffs.

2

The LCPB is bounded to the northwest by the LEC, which is at an elevation of at least 490 feet above mean sea level (MSL). Directly to the west is the Bottom Ash Surface Impoundment (LCPA). To the south of the LCPB are lower elevation agricultural fields ranging from approximately 465 to 475 feet MSL. South of the railroad, bedrock bluffs that rise to an elevation of over 550 feet MSL. Approximately 800 feet east of the LCPB lies the Utility Waste Landfill (UWL), with berm elevations around 488 feet MSL.

2.1 Coal Combustion Residuals (CCR) LCPB Surface Impoundment

The LCPB is located in the floodplain of the Missouri River to the southeast of the LEC and is constructed with perimeter berms at an elevation of approximately 494 feet MSL, which is above the 100-year flood elevation of 484 feet MSL. Historically, fly ash has been managed and stored in this Surface Impoundment. Construction drawings indicate that the base depth of liner in the LCPB extends down to an elevation of approximately 460 feet MSL in the deepest portions of the CCR Unit.

2.2 Geology

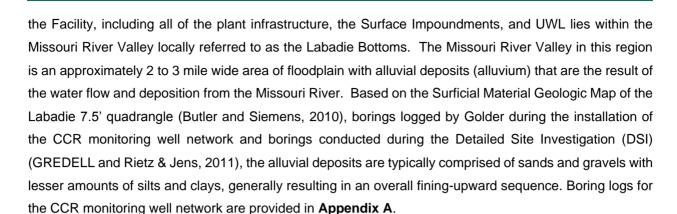
2.2.1 Physiographic Setting and Regional Geology

The Facility area lies along the northeast margin of the Salem Plateau, a subsection of the Ozark Physiographic Province (USGS, 1994). In this region, the Salem Plateau is mainly comprised of Ordovician dolomite, limestone, and sandstone formations. To the northwest of the Labadie Bottoms area, the Salem plateau transitions into the geologically younger Mississippian and Pennsylvanian subsystems that are regionally known as glaciated plains (GREDELL Engineering Resources, Inc. (GREDELL) and Reitz & Jens, Inc. (Reitz & Jens), 2011). The approximate boundary between these two systems is the Missouri River, which is interpreted as being an ice-margin stream during the latest glacial epoch and defined the approximate southernmost progression of glaciation.

2.2.2 Local Geology

The geology immediately surrounding the Facility is composed of two distinctly different geological terrains; (1) floodplain deposits of the Missouri River Valley and (2) older sedimentary bedrock formations. Most of





The depth of the alluvial deposits near the surface impoundment typically range from approximately 90 to 110 feet below ground surface (BGS) (365 to 385 feet MSL) with total depths in the area as deep as 135 feet BGS and becoming shallower towards the bluffs to the south based on site specific borings. Sedimentary bedrock underlies the alluvial deposits.

Bluffs to the south, as well as bedrock underlying the floodplain alluvial deposits, are comprised of relatively flat-lying Ordovician-aged limestones, sandstones and dolomites. In progression from youngest to oldest, these deposits consist of the Plattin Group, Joachim Dolomite, St. Peter Sandstone, Powell Dolomite, and the Cotter/Jefferson City Dolomites (Starbuck, 2010; GREDELL and Reitz & Jens, 2011). In deep wells, the Roubidoux Formation and the underlying Gasconade Dolomite can be found at depths of approximately 530-764 feet BGS (GREDELL and Reitz & Jens, 2011).

2.3 Site Hydrogeology

Site hydrogeology has been characterized based on information obtained from 127 piezometers and borings installed by GREDELL and Reitz & Jens (2011) to support a DSI conducted for the Labadie UWL, the CCR groundwater monitoring wells installations completed by Golder, and 36 monitoring wells installed around the perimeter of the UWL in 2013 and 2014 by Reitz & Jens for state required UWL groundwater monitoring. **Figure 3** provides a generalized north-south depiction of the Nearby LCPA Surface Impoundment referenced to local geology, groundwater, and the Missouri River.

2.3.1 Uppermost Aquifer

The CCR Rule requires that a groundwater monitoring system be completed in the uppermost aquifer around each CCR Surface Impoundment (§257.91(a)). As shown on **Figure 3**, the uppermost aquifer beneath all of the CCR impoundments and landfills is the alluvial deposits consisting of primarily alluvial sands with some silt, clay, and gravel associated with the Missouri River Valley alluvium. This alluvium overlies Ordovician-aged sedimentary bedrock formations. As generally described above, these alluvial



deposits typically exhibit a fining-upward sequence with some silts and clays present within the shallow zone and mostly coarse sands and gravels present at depth.

4

2.3.2 Surface Water and Groundwater Elevations

2.3.2.1 CCR Surface Impoundment Water

The LCPB is a lined pond that typically has a ponded water level approximately 20 plus feet above the surrounding natural groundwater level. Water in the pond is not considered interconnected with the surrounding alluvial aquifer due to the liner system. To the west of the LCPB lies the LCPA which is an unlined Surface Impoundment. LCPA Pond levels in this facility typically range between 18 to 31 feet above the natural groundwater level of the surrounding alluvial aquifer. Data show a mounding effect between water in the LCPA and the surrounding aquifer.

2.3.2.2 Alluvial Aquifer

Groundwater elevations within the alluvial aquifer in the Labadie bottoms area have been obtained in several different studies. As a part of the DSI for the UWL, groundwater elevations were obtained in 100 piezometers located within the alluvial aquifer approximately 800 to 2,000 feet to the east of LCPB from December 2009 to November 2010. These piezometers were all located in the alluvial aquifer and had screen intervals ranging from approximately 428 to 452 feet MSL. Groundwater elevation measurements ranged from approximately 456 to 469 feet MSL during this time period. However, during any single round of groundwater level measurements the aquifer potentiometric surface was relatively flat, with the surface variability in any round of groundwater level measurements ranging from approximately 1 to 4 feet across all of the piezometers. Potentiometric Surface Maps displaying these results are provided in **Appendix B**.

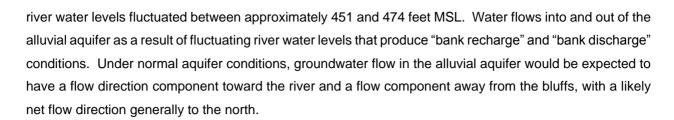
Water level measurements were also collected at 36 monitoring wells during four background sampling events for the UWL from 2013-2014 (GREDELL and Reitz & Jens, 2013a, 2013b, 2013c, and 2014). During this timeframe, groundwater elevations ranged from approximately 448 to 459 feet MSL.

Golder obtained groundwater elevation measurements from March 2016 through May 2017 within the alluvial aquifer for the CCR monitoring wells. For each of the 8 background sampling events (baseline events), groundwater elevations were measured at monitoring wells within a 24-hour timeframe and a potentiometric map was generated from these data (**Appendix C and Table 1**). Groundwater elevations ranged from approximately 453 feet MSL to 467 feet MSL.

2.3.3 Groundwater Flow Directions

Groundwater flow within the alluvial aquifer is dynamic and is influenced by seasonal changes in the water level in the adjacent Missouri River. River water levels measured at the Facility display large seasonal changes in the elevation of the Missouri River water surface. For example, from April 2015 to July 2017,





Although the movement of groundwater within the alluvial aquifer at the Facility is complex, the movement has been characterized by frequent groundwater elevation measurements and the generation of potentiometric surface maps generated by GREDELL, Rietz & Jens and Golder (**Appendix B**, **Appendix C and Table 1**). The potentiometric surface maps display some variability in the groundwater flow direction. These changes in flow direction are related to the level within the adjacent Missouri River.

In addition to the DSI potentiometric surface maps, additional groundwater analysis was also completed as a part of the UWL Construction Permit Application (GREDELL and Rietz and Jens, 2014). These analyses calculated the net groundwater flow velocity and direction from December 2009 until November 2010. During this timeframe, groundwater located near proposed UWL cells 1 & 2 was calculated to have a net annual velocity of approximately 12 feet per year with a bearing of 33 (North-northeast). Groundwater located near UWL cells 3 & 4 was calculated to have a net annual flow velocity of approximately 15 feet per year bearing approximately 67 (East-northeast). The UWL results also displayed that groundwater flow direction was highly variable from month to month depending on Missouri River conditions with overall flow directions ranging from a west-northwesterly direction to a southeasterly direction.

Groundwater flow direction and hydraulic gradient were estimated for the CCR wells using the EPA's Online Tool for Site Assessment (USEPA, 2016). Estimated results from this analysis are provided in **Table 2**. These results indicate that while groundwater flow direction is variable, overall net groundwater flow during the baseline sampling period was generally towards the northwest/north/northeast, flowing from the bluffs toward the river.

Based on the potentiometric surface maps, a general flow direction from the south/southwest (bluffs area) to the north/northeast (Missouri River) under normal river conditions is expected. However, during periods of high river levels, groundwater flow can temporarily reverse and flow southward. During these times of high river stage and temporary flow direction changes, horizontal groundwater gradients generally decrease and little net movement of groundwater to the south occurs.

Horizontal and vertical groundwater flow within the uppermost aquifer has been locally influenced by operation of the adjacent LCPA Surface impoundment. Ponding of water in the LCPA at elevations greater than the static water levels in the underlying alluvial aquifer groundwater create a localized "mounding"





effect, resulting in localized downward gradients and localized radial groundwater flow downward and outward from the impoundment.

6

2.3.3.1 **Horizontal Gradients**

Horizontal groundwater gradients in the alluvial aquifer are typically low and flat. The gradients are very dependent on river water levels (bank recharge and bank discharge conditions described earlier). Horizontal flow gradients calculated for the UWL DSI ranged from 0.000002 to 0.0035 feet/foot. The DSI indicates that the higher gradients were observed closer to the Missouri River and reflect localized river influence and are not representative of site-wide conditions farther from the river. Gradients calculated as a part of the UWL monitoring display similar results to the DSI with groundwater gradients ranging from 0.000002 to 0.00756 feet/foot.

Site-wide horizontal gradients were also calculated for each of the CCR groundwater baseline sampling events and the results of these are displayed on Table 2. The horizontal groundwater gradients are low, ranging from 0.0002 to 0.0006 feet/foot.

A review of the potentiometric surface maps confirms the gradient estimates for a larger scale, but also demonstrates that localized horizontal gradients can be higher especially in areas near the Missouri River.

2.3.3.2 **Vertical Gradients**

A review of downward gradients observed in piezometers was completed by comparing groundwater elevations obtained by GREDELL and Rietz & Jens DSI, as well as by Golder's initial baseline sampling data. This analysis was completed between shallow and intermediate/deep zone piezometer locations where the piezometers are nested (two or more piezometers in close proximity, screened at different elevations). From the review of these data, areas away from the adjacent LCPA show relatively variable vertical gradients that fluctuate between upward and downward with no consistent vertical gradient present between shallow and deeper zones of the alluvial aquifer. Areas adjacent to the LCPA (LMW-1S vs UMW-7D and LMW-2S vs UMW-5D) demonstrate a slight downward gradient. While results vary, overall gradients are typically downward ranging up to 0.4 feet difference between the groundwater levels.

Downward gradients within the nearby LCPA pond and the underlying alluvial groundwater zone are much greater, based on a review of water elevation measurements and the pond gauge levels. This downward gradient changes seasonally based on river levels and fluctuating alluvial aquifer groundwater levels. During high river level conditions, the difference in groundwater elevation between the LCPA pond and the deeper alluvial groundwater zone has been as low as approximately 18 feet during the baseline sampling period. During low river level conditions, the difference in groundwater elevation has been shown to be as much as approximately 31 feet between the deeper alluvial groundwater zone and the LCPA pond.



2.3.4 Hydraulic Conductivities

In-situ hydraulic conductivity tests (slug tests) were conducted as part of the DSI within the shallow portion of the alluvial aquifer in the area of the UWL. The hydraulic conductivity in the area is highly dependent of the geology present within the screening interval of the piezometer. Estimates of the hydraulic conductivity within the aquifer were made using data acquired from slug tests in 25 piezometers. The calculated hydraulic conductivity of the fluvial sediments ranges from 1.01 x 10⁻² to 4.81 x 10⁻² centimeters/second with an average value of 2.49 x 10⁻² centimeters/second. Sandy channel deposits displayed a similar average value of 2.79 x 10⁻² centimeters/second. Generally, there is a tendency toward higher hydraulic conductivity values where the screened interval intersects with relatively coarse-grained sands interpreted as channel deposits. For relatively homogenous flood plain/levee sequences containing fine-grained sediments, calculated values are demonstrably lower. Similarly, in piezometers where the screen interval intersects finer-grained, clayey backswamp/cut-off deposits, the DSI indicates lower hydraulic conductivity values were measured.

7

Groundwater flow velocities were calculated as a part of the DSI using these hydraulic conductivity values, hydraulic gradients, and an estimated value for effective porosity (Table 8 of the DSI). The DSI suggests a representative range of prevailing groundwater movement at the Site is between 0.1 and 10 feet per year, depending on hydraulic conductivity and effective porosity.

Golder also performed rising head hydraulic conductivity tests on the 12 newly installed CCR monitoring wells used to monitor the shallow alluvial aquifer, in order to estimate the hydraulic conductivities in February to April, 2016. The tests were conducted using a pneumatic slug (Hi-K slug) and a downhole pressure transducer. The results of Golder's hydraulic conductivity testing estimated the geometric mean of hydraulic conductivity to be approximately 1.8 x 10⁻² cm/sec for CCR groundwater monitoring wells screened in the shallow alluvial aquifer. Golder's findings for hydraulic conductivity values are summarized below in **Table 3** and are consistent with the conductivities calculated in the DSI.

Estimated groundwater flow velocities were calculated using the CCR monitoring well hydraulic conductivity, hydraulic gradients and an estimated value for effective porosity (**Table 2**). Using these values, groundwater flow velocities are estimated to range between 0.04 and 0.14 feet per day and average approximately 19 feet per year.

Table 3: CCR Monitoring Well Hydraulic Conductivities

				Estimated Hydraulic					
	Total Depth	Well Screen Interval	Well Screen interval	Conductivity	Estimated Hydraulic				
Well ID	(feet BTOC)	(feet BTOC)	(feet MSL)	(feet/day)	Conductivity (cm/sec)				
LCPB Fly Ash Surface Impoundment Monitoring Wells									
LMW-1S	25.75	15.6 - 25.4	444.7 - 454.5	97	3.4E-02				
LMW-2S	56.07	50.9 - 55.7	441.0 - 445.8	31	1.1E-02				
LMW-3S	71.80	61.6 - 71.4	421.2 - 431.0	37	1.3E-02				
LMW-4S	34.83	24.6 - 34.4	438.5 - 448.3	76	2.7E-02				
LMW-5S	23.96	13.8 - 23.6	445.2 - 455.0	56	2.0E-02				
LMW-6S	25.09	14.9 - 24.7	444.9 - 454.7	56	2.0E-02				
LMW-7S	25.27	15.1 - 24.9	443.6 - 453.4	41	1.4E-02				
LMW-8S	25.20	15.0 - 24.8	442.4 - 452.2	56	2.0E-02				
Background	l Monitoring W	/ells							
BMW-1S	33.03	22.8 - 32.6	440.9 - 450.7	128	4.5E-02				
BMW-2S	30.17	20.0 - 29.8	444.8 - 454.6	112	4.0E-02				
UWL Monit	oring Wells								
MW-26*	23.00	12.8 - 22.6	446.6 - 456.4	79	2.8E-02				
TMW-1*	21.58	11.3 - 21.1	448.2 - 458.0	79	2.8E-02				
TMW-2	27.77	17.6 - 27.4	443.0 - 452.8	56	2.0E-02				
TMW-3	27.61	17.4 - 27.2	442.2 - 452.0	78	2.7E-02				

8

Notes

- 1. feet MSL feet above mean sea level
- 2. cm/sec centimeters per second
- 3. Rising head tests were completed by Golder Associates on February 18, and April 19, 2016 using a Pneumatic Hi-K Slug®
- 4. feet BTOC feet below top of casing
- 5. * Hydraulic conductivity values represent average hydraulic conductivity for channel deposits from the UWL DSI.

2.3.5 Porosity and Effective Porosity

Porosities were estimated based on the grain size distributions of an aquifer soil sample collected during monitoring well drilling. A representative grain size distribution was collected from the screen interval at LMW-1S using the ASTM D6912 Method B and the results are provided in **Appendix D**. The sample from LMW-1S was similar in field classification to other well drilling samples and the results indicate that the screened interval of the alluvial aquifer are mostly comprised of sand (at least 90%) with lesser amounts of gravel, silt and clay. Also, the typical grain size of the sand ranges from fine to medium sand. Textbook values of porosities for sands and sand/gravel mixes range from 25-50% (Fetter, 2000 and Freeze and Cherry, 1979) and fine sands typically range from 29-46%, whereas coarse sands typically range from 26-43% (Das, 2008). An average porosity of 35% is estimated for the alluvial aquifer based on the site data.

Effective porosity is the porosity that is available for fluid flow. Studies completed in unconsolidated sediments have determined that water molecules pass through all pores and the effective porosity is





approximately equal to the total porosity (Fetter, 2000). Therefore, the effective porosity of the alluvial aquifer is also estimated to be 35%.

3.0 GROUNDWATER MONITORING NETWORK

3.1 Monitoring Network Design Criteria

§257.91 of the CCR Rule sets out the requirements for development of a groundwater monitoring system for both new and existing CCR landfills and Surface Impoundments. The performance standard in the CCR Rule (§257.91(a)) states that the groundwater monitoring system must consist of a sufficient number of wells at appropriate locations to yield groundwater samples in the uppermost aquifer that accurately represent:

10

- The quality of background groundwater
- The quality of groundwater passing the waste boundary of the CCR unit

3.2 Design of the Groundwater Monitoring System

The detection monitoring well network for the Facility is depicted on **Figure 2**. The network consists of 10 monitoring wells screened in the uppermost aquifer for the purpose of monitoring the LCPB Surface Impoundment. The monitoring well network includes 2 background groundwater monitoring wells (BMW-1S and BMW-2S) that are located approximately 2 miles west of the surface Impoundment in areas unaffected by CCR disposal. Eight (8) of the groundwater monitoring wells are placed ringing the LCPB and are considered to be the downgradient wells. The groundwater monitoring well locations were selected based on site-specific information presented in section 2.0 of this document, as well as the preferential migration pathway analysis below.

3.2.1 Preferential Migration Pathway Analysis

After detailed review of the information outlined in section 2.0 of this document, a preferential migration pathway for potential groundwater impacts coming from the Surface Impoundment was determined. The LCPB has a bottom elevation of approximately 460 feet MSL. Potential constituent migration pathways are likely to be downward then laterally in the direction of groundwater flow in the shallow alluvial aquifer. Groundwater flow within the alluvial aquifer can also be variable depending on levels within the Missouri River and can flow in a variety of directions. Groundwater monitoring wells were placed around the unit in order to capture flow in variable directions. Based on water level readings, the groundwater in the shallow alluvial aquifer can range from approximately 448 to 469 feet MSL. In order to place monitoring well screens within the migration pathway from the unit, monitoring wells were installed with screen interval elevations that range below the seasonal low groundwater levels so that the well screen is submerged below the water table surface to allow for groundwater sampling.



3.3 Groundwater Monitoring Well Placement

3.3.1 Background/Upgradient Monitoring Well Locations

As described above, the flow of groundwater in the alluvial aquifer is generally from the bluffs area located south of the site toward the Missouri River to the northwest/north/northeast, however, alluvial aquifer flow is locally influenced by water levels in the nearby LCPA and the Missouri River level. The CCR Rule (§257.91(a)(1)) requires that background groundwater samples from the uppermost aquifer "Accurately represent the quality of background groundwater that has not been affected by leakage from a CCR unit."

11

As shown in **Figure 2**, the background monitoring wells BMW-1S and BMW-2S are west of the LCPB at a location approximately 2,000 to 3,000 feet from the Missouri River. These wells provide background groundwater quality representative of upgradient Missouri River influences on the alluvial aquifer.

3.3.2 Downgradient Monitoring Well Locations

As discussed above, downgradient monitoring wells are located ringing the LCPB to monitor potential migration pathways. **Figure 2** shows that the downgradient well network consists of 8 groundwater monitoring wells (LMW-1S, LMW-2S, LMW-3S, LMW-4S, LMW-5S, LMW-6S, LMW-7S, and LMW-8S) around the LCPB at locations that are located as close to the waste boundary as practical.

3.3.3 Groundwater Monitoring Well Screen Intervals

The system of monitoring wells ringing the Surface Impoundment is screened in the alluvial aquifer zone near the base elevation of CCR. Details on the construction of the groundwater monitoring wells are provided in **Table 4** and **Appendix E**. Screen intervals were range from approximately 430 to 455 feet MSL in sandy alluvial deposits.



4.0 INSTALLATION OF THE GROUNDWATER MONITORING SYSTEM

The CCR Rule Groundwater Monitoring System for the LCPB was installed in November 2015 and February 2016 as described in the following subsections.

12

4.1 Drilling Methods and Monitoring Well Constructions

Cascade Drilling LP installed the monitoring wells using a rotosonic drill rig (Mini Sonic CDD 1415) under direct supervision of a Golder Geologist or Engineer. Continuous soil core samples were obtained at each well borehole location and were logged in the field by Golder. Soils were classified according to the Unified Soil Classification System. Boring logs and well construction diagrams are provided in **Appendix A**, and **Appendix E**, respectively.

Groundwater monitoring wells were installed in accordance with Missouri Department of Natural Resources (MDNR) Well Construction Rules (10 CSR 23-4.060 Construction Standards for Monitoring Wells). All groundwater monitoring wells were installed with 2-inch diameter PVC well riser pipe and 10-foot long, 0.010-inch machine slotted well screens. Wells were installed with a sand filter pack, bentonite seal, and annular space in accordance with MDNR Well Construction Rules. Details on the construction of the groundwater monitoring wells are provided in **Table 4** and **Appendix E**.

Monitoring wells were completed with an aluminum protective cover with a locking lid that extends approximately 2 to 3 feet above ground surface and a small concrete pad. Yellow protective posts (concrete filled steel bollards) have been installed around each monitoring well.

4.2 Groundwater Monitoring Well Development

After well construction, a Golder geologist or engineer developed groundwater monitoring wells using surging and purging techniques. During development, field parameters (pH, conductivity, temperature, and turbidity) were recorded and development was complete once a minimum of three well-bore volumes of water were purged, turbidity was typically less than 20 nephelometric turbidity units (NTU) or ± 10% and consecutive measurements of field parameter values were within 10 percent difference. Groundwater monitoring wells were developed using an inertial pump with a surge block ring attached to a foot valve to surge and purge the well. Well development forms are attached in **Appendix F**.

4.3 Dedicated Pump Installation

A dedicated pump was installed in each groundwater monitoring well after development and hydraulic conductivity testing. The dedicated pumps provide a consistent, repeatable sampling method to reduce likelihood of cross-contamination, reduce water sample turbidity, and expedite sampling. For the purposes of this groundwater monitoring network, low-flow QED brand PVC MicroPurge bladder pumps with Dura-Flex Teflon bladders were installed in each well.





4.4 Surveying and Well Registration

Zahner and Associates, Inc., a Professional Land Surveyor licensed in Missouri, surveyed the location and top of casing elevation of the monitoring wells. A drawing showing the location of the groundwater monitoring wells is shown in **Figure 2** and a summary of survey information is provided in **Table 4**. Upon completion of monitoring well installation and surveying, MDNR Well Construction Registration Forms were prepared for each well and submitted to MDNR. Copies of these forms are provided in **Appendix G**.

5.0 GROUNDWATER MONITORING PROGRAM

The groundwater monitoring program for the LCPB Surface Impoundment is described in the following sections.

14

5.1 Baseline Sampling Events

In accordance with section 257.94(b) of the CCR Rule, before starting detection monitoring, eight baseline (or background) samples were collected for all Appendix III and Appendix IV parameters at all downgradient and upgradient/background monitoring wells prior to October 17, 2017. These samples establish initial baseline datasets that are used for the statistical evaluation of groundwater results.

5.2 Detection Monitoring

The Detection Monitoring Program is defined in the CCR Rule in section 257.94 and the following sections outline the procedures for the detection monitoring program.

5.2.1 Sampling Constituents and Monitoring Frequency

Detection monitoring should be completed at a minimum of semi-annually (approximately every 6 months) for all Appendix III constituents (**Table 5**), unless a demonstration that the need for an alternative monitoring schedule is required. **Table 6** lists the analytical methods and practical quantitation limits used for the monitoring program.

5.2.2 Data Evaluation and Response

As required in the CCR Rule, a statistical evaluation of the groundwater data must be completed within 90 days of receiving data from the laboratory. The data will be analyzed using the methods and procedures outlined in the statistical analysis plan (**Appendix H**).

5.3 Assessment Monitoring

Assessment monitoring is outlined in section 257.95 of the CCR Rule and is initiated after a confirmed SSI has been identified and no alternate source demonstration has been completed. In accordance with the CCR Rule, a notification must be prepared and placed within the Facility operating record and on the publically available website stating that an Assessment Monitoring program has been initiated. The purpose of Assessment Monitoring is to determine whether or not groundwater concentrations are at a Statistically Significant Level (SSL) compared to Groundwater Protection Standards (GWPS). Detection Monitoring sampling continues during Assessment Monitoring.

5.3.1 Sampling Constituents and Monitoring Frequency

As outlined in section 257.95 of the CCR rule, Assessment Monitoring groundwater sampling must begin within 90 days of a confirmed SSI determination. Sampling must be completed at all monitoring wells used





in the detection monitoring program, for all Appendix IV analytes (**Table 5**). Within 90 days of receiving data from this initial Assessment Monitoring sampling event, a second sampling event must be completed analyzing the Appendix IV constituents detected in groundwater during the initial sampling event.

Following this initial phase of the Assessment Monitoring Program, the CCR Rule requires sampling of the full list of Appendix IV constituents on an annual basis (Annual Assessment Event). During the other semi-annual Assessment Sampling Event, only those Appendix IV constituents that are detected during the annual sampling event are to be analyzed and reported. Additionally, verification resampling will be performed within 90 days of receiving data from the laboratory for all detected Appendix IV constituents for each event.

5.3.2 Data Evaluation and Response

As required in the CCR Rule, a statistical evaluation of the groundwater data must be completed within 90 days of receiving data from the laboratory. The data will be analyzed using the methods and procedures outlined in the Statistical Analysis Plan (**Appendix H**).

A GWPS is required for each Appendix IV constituent and must be included in the annual report. The GWPS will be either the MCL or a value based on background data, whichever is higher. The generation of the GWPS is discussed in more detail in the Statistical Analysis Plan (**Appendix H**). Statistical analysis must be completed within 90 days of receiving data from the laboratory. The statistical analysis will determine if any constituents are SSLs greater than the GWPS.

In order to discontinue Assessment Monitoring and return to Detection Monitoring, the concentration of all Appendix III and Appendix IV constituents for all compliance wells must be at levels statistically lower than background levels for two consecutive sampling events (257.95(e)). If any constituent is present at a statistical level above background levels, but below the GWPS, then Assessment Monitoring continues.

5.3.2.1 Responding to a SSL

If the Assessment Monitoring statistical evaluations demonstrate that a SSL has been triggered, then the owner/operator of the CCR unit must complete the following four actions as described in 257.95(g):

- 1. Prepare a notification identifying the constituents in Appendix IV that have exceeded a CCR Unit specific GWPS. This notification must be placed in the facility operating record within 30 days of identifying the SSL (257.95(g)) and 257.105(h)). Additionally, within 30 days of placing the notification in the operating record, the notification must be posted to the internet site (257.107(h)).
- 2. Define the character and extent of the release and any relevant site conditions that may affect the corrective action remedy that is ultimately selected. The characterization must be sufficient to support a complete and accurate assessment of the corrective measures necessary to effectively clean up releases from the CCR Unit and must include at least the following: (No timeframe is specified in the CCR Rule for this action)



A. Installation of additional monitoring wells that are necessary to define the contaminant plume

16

- B. Collect data on the nature and estimated quantity of the material released
- C. Install and sample at least one additional monitoring well at the facility boundary in the direction of the contaminant plume migration
- 3. Notify off-site property owners if the contamination plume has migrated offsite on to their property within 30 days of this determination.
- 4. If possible, provide an alternate source demonstration that determines that the SSL is not caused by a release at the facility within 90 days of completing the statistical evaluation. If no alternate source demonstration can be made and the plume is determined to have originated from the CCR Unit, then proceed to corrective action steps in the CCR Rule.
 - D. If no alternate source demonstration is made, and the CCR Unit is an unlined surface impoundment, the closure or retrofit must be initiated.

Actions 1-3 must be completed regardless of whether or not an alternate source demonstration can be made.

5.3.3 Annual Reporting Requirements

In addition to the periodical reporting listed above, an annual groundwater monitoring report will be prepared according to the requirements of 40 CFR §257.90(e). At a minimum, the annual groundwater monitoring report will contain the following information:

- The current status of the groundwater monitoring program
- A projection of key activities planned for the upcoming year
- A map showing the CCR unit and all background (or upgradient) and downgradient monitoring wells included in this monitoring plan
- A discussion of any monitoring wells that were installed or decommissioned during the preceding year or any other changes made to the groundwater monitoring system
- Analytical results from groundwater sampling
- The monitoring data obtained under §§ 257.90 through 257.98, including a summary of the number of groundwater samples that were collected for analysis for each background and downgradient well, the dates the samples were collected, and whether the sample was required by the detection monitoring or assessment monitoring programs
- A narrative discussion of any transition between monitoring programs (e.g., the date and circumstances for transitioning from detection monitoring to assessment monitoring in addition to identifying the constituent(s) detected at a statistically significant increase over background levels)
- If required, an alternate source demonstration that is certified by a professional engineer
- If required, a demonstration that an alternate sampling frequency is needed
- If assessment monitoring is required, a listing of GWPS for each Appendix IV constituent



6.0 GROUNDWATER SAMPLING METHODOLOGY

Sampling will be performed in accordance with generally accepted practices within the industry and with the provisions of Missouri regulations. The following sections provide details regarding procedures that will be used to collect groundwater samples. Although this section provides reference to specific forms, the use of other equivalent forms to record the necessary data is permissible.

17

6.1 Equipment Calibration

Equipment used to record field water quality parameters will be calibrated each day prior to use following manufacturers' recommendations. Calibration solutions for standardization materials will be freshly prepared or from non-expired stock. In the absence of manufacturer or regulatory guidance, field equipment should be calibrated to within +/- 10 percent of the standard (or 0.1 standard units for pH meters). Equipment that fails calibration may not be used. Calibration records will be maintained. A sample field Instrument Calibration Form is included in **Appendix I**.

6.2 Monitoring Well Inspection

Prior to performing any water purging or sampling, each monitoring well will be inspected to assess its integrity. The condition of each monitoring well will be evaluated for any physical damage or other breach of integrity. The security of each monitoring well will be assessed in order to confirm that no outside source constituents have been introduced to the monitoring well.

6.3 Water Level Measurement

To meet the requirements of §257.93(c), water level measurements will be taken at all monitoring wells and prior to the start of any groundwater purging. These measurements will be taken within a 24 hour period and will be recorded on the Record of Water Level Readings form or Groundwater Sample Collection Form (included in **Appendix I**). Static water levels will be measured in each monitoring well prior to purging using an electric meter accurate to 0.01 foot. The measuring probe will be rinsed with distilled or deionized water before and after use at each well.

6.4 Monitoring Well Purging

Prior to collecting samples, each monitoring well will be purged. Purging will be accomplished using either:

- Low-flow (a.k.a., minimal drawdown, or Micropurge) techniques
- Traditional purging techniques where at least three well volumes are evacuated before samples are collected

6.4.1 Low-Flow Sampling Technique

Low-flow groundwater sampling procedures will be used for purging and sampling monitoring wells that are equipped with dedicated pumps and will sustain a pumping rate of at least 100 milliliters per minute (ml/min).





Water will be purged from these wells at low rates in order to minimize drawdown in the well during purging and sampling. Depth to water measurements and field water quality parameters (temperature, pH, turbidity, and conductivity) recorded during purging will be used as criteria to determine when purging has been completed. Sample collection will be initiated immediately after purging at each well.

During water purging, wells will be pumped at rates that minimize drawdown in the well. Purging rates in the range of 100-500 ml/min typically will be used; however, higher rates may be used if sustained by the well. Stabilization of the water column will be considered achieved when three consecutive water level measurements vary by 0.3-foot or less at a pumping rate of no less than 100 ml/min (USEPA, 2010).

At a minimum, field water quality parameter measurements of temperature, pH, turbidity, and conductivity, will be measured during purging at each well. Prior to collecting the initial set of field water quality parameters, the water in the sampling pump and discharge tubing (i.e., pump system volume) remaining from the previous sampling event will be removed.

After evacuating the water in the pump system, collecting field measurements will begin. Depth to water measurements and field water quality parameter measurements will be made during purging. If a field meter equipped with a flow cell is used, an amount of water equal to the volume of the flow cell should be allowed to pass through the flow cell between individual field stabilization measurements. Stabilization will be attained and purging considered complete when three consecutive measurements of each field parameter vary within the following limits:

- ± 0.2 for pH
- ± 3% for Conductivity
- ± 10% for Temperature
- Less than 10 nephelometric turbidity units (NTU) or ± 10% for Turbidity

All data gathered during monitoring well purging will be recorded on a form, an example of which is included in **Appendix I**.

6.4.2 Traditional Purge Techniques

If low-flow sampling is not performed, wells will be purged a minimum of 3 well volumes before collecting a sample. Purging procedures will generally follow those for low-flow sampling including measurement of the field parameters listed above with two exceptions:

- Higher flow rate may be used during purging
- Purging is completed after a minimum of 3 well volumes have been removed (see below)



Even where low-flow sampling is not performed, the sampling goals are to:

- Stabilize field parameters (listed in previous section) prior to collecting samples
- Minimize drawdown in the well

When traditional purge techniques are used, field stabilization measurements will be collected at the beginning of purging and between each well volume purged. The stability criteria will be those described above for low-flow sampling.

19

6.4.3 Low Yielding Wells

If a monitoring well purges dry, it will be allowed to recover up to 24 hours before samples are collected. No additional purging will be performed after initially purging the monitoring well dry. If recharge is insufficient to fill all necessary sample bottles, samplers will note this on the field form, and fill as many sample bottles as possible.

6.5 Sample Collection

Sampling should take place immediately after purging is complete. Samples will be transferred directly from field sampling equipment into containers supplied by the analytical laboratory appropriate for the constituents being monitored as listed in **Table 6**. Sample containers will be kept closed until the time each set of sample containers is filled.

6.6 Equipment Decontamination

All non-dedicated field equipment that is used for purging or sample collection shall be cleaned with a phosphate-free detergent and triple-rinsed, inside and out, with deionized or distilled water prior to use and between each monitoring well. Decontamination water shall be disposed of at an Ameren approved location. Any disposable tubing used with non-dedicated pumps should be discarded after use at each monitoring well. Clean latex gloves will be worn by sampling personnel during monitoring well purging and sample collection.

6.7 Sample Preservation and Handling

In accordance with §257.93 of the CCR Rule, groundwater samples collected as part of the monitoring program will not be filtered prior to analysis. Once groundwater samples have been collected and preserved in laboratory supplied containers, they will be packed into insulated, ice-filled coolers to be maintained at a temperature as close as possible to 4 degrees Celsius. Groundwater samples will be collected in the designated size and type of containers required for specific parameters. Sample containers will be filled in such a manner as not to lose preservatives by spilling or overfilling. Samples will be delivered to the laboratory or sent via overnight courier following chain-of-custody procedures.



6.8 Chain-of-Custody Program

The chain-of-custody (COC) program will allow for tracing sample possession and handling from the time of field collection through laboratory analysis. The COC program includes sample labels, sample seals, field Groundwater Sample Collection Forms, and COC record. A sample Chain-of-Custody (COC) form is provided in **Appendix I**.

20

Each sample will be assigned a unique sample identification number to be recorded on the sample label. The sample identification number for all samples will be designated differently based on the nature of the samples. Each sample identification number and description will be recorded on the field Groundwater Sample Collection Form and on the COC document.

6.8.1 Sample Labels

Sample labels sufficiently durable to remain legible when wet will contain the following information, written with indelible ink:

- Site and sample identification number
- Monitoring well number or other location
- Date and time of collection
- Name of collector
- Parameters to be analyzed
- Preservative, if applicable

6.8.2 Sample Seal

The shipping container will be sealed to prevent the samples from being disturbed during transport to the laboratory.

6.8.3 Field Forms

All field information must be completely and accurately documented to become part of the final report for the groundwater monitoring event. Example field forms are included in **Appendix I**. The field forms will document the following information:

- Identification of the monitoring well
- Sample identification number
- Field meter calibration information
- Static water level depth
- Purge volume
- Time monitoring well was purged
- Date and time of collection



- Parameters requested for analysis
- Preservative used
- Field water quality parameter measurements
- Field observations on sampling event
- Name of collector(s)
- Weather conditions including air temperature and precipitation

6.8.4 Chain-of-Custody Record

The COC record is required for tracing sample possession from time of collection to time of receipt at the laboratory. The National Enforcement Investigations Center (NEIC) of USEPA considers a sample to be in custody under any of the following conditions:

21

- It is in the individual's possession
- It is in the individual's view after being in his possession
- It was in the individual's possession and he locked it up
- It is in a designated secure area

All environmental samples will be handled under strict COC procedures beginning in the field. The field team leader will be the field sample custodian and will be responsible for ensuring that COC procedures are followed. A COC record will accompany each individual shipment. The record will contain the following information:

- Sample destination and transporter
- Sample identification numbers
- Signature of collector
- Date and time of collection
- Sample type
- Identification of monitoring well
- Number of sample containers in shipping container
- Parameters requested for analysis
- Signature of person(s) involved in the chain of possession
- Inclusive dates of possession

A copy of the completed COC form will be placed in a water resistant bag and accompany the shipment and will be returned to the shipper after the shipping container reaches its destination. The COC record will also be used as the analysis request sheet. When shipping by courier, the courier does not sign the COC record: copies of shipping forms are retained to document custody.





6.9 Temperature Control and Sample Transportation

After collection, sample preservation, and labeling, sample containers will be placed in coolers containing water-ice with the goal of reducing the groundwater samples to a temperature of approximately 4°C or less. All samples included in the shipping container will be packed in such a manner to minimize the potential for container breakage. Samples will be either hand-delivered or shipped via commercial carrier to the certified analytical laboratory. Custody seals will be placed on the shipping containers if a third party courier is used.

7.0 ANALYTICAL AND QUALITY CONTROL PROCEDURES

7.1 Data Quality Objectives

As part of the evaluation component of the Quality Assurance (QA) program, analytical results will be evaluated for precision, accuracy, representativeness, completeness, and comparability (PARCC). These are defined as follows:

 Precision is the agreement or reproducibility among individual measurements of the same property, usually made under the same conditions

23

- Accuracy is the degree of agreement of a measurement with the true or accepted value
- Representativeness is the degree to which a measurement accurately and precisely represents a characteristic of a population, parameter, or variations at a sampling point, a process condition, or an environmental condition
- Completeness is a measure of the amount of valid data obtained from a measurement system compared with the amount that was expected to be obtained under correct normal conditions
- Comparability is an expression of the confidence with which one data set can be compared with another data set in regard to the same property

The accuracy, precision and representativeness of data will be functions of the sample origin, analytical procedures and the specific sample matrices. Quality Control (QC) practices for the evaluation of these data quality indicators include the use of accepted analytical procedures, adherence to hold time, and analysis of QC samples (e.g., blanks, replicates, spikes, calibration standards and reference standards).

Quantitative QA objectives for precision and accuracy, along with sensitivity (detection limits) are established in accordance with the specific analytical methodologies, historical data, laboratory method validation studies, and laboratory experience with similar samples. The Representativeness of the analytical data is a function of the procedures used to process the samples.

Completeness is a qualitative characteristic which is defined as the fraction of valid data obtained from a measurement system (e.g., sampling and analysis) compared to that which was planned. Completeness can be less than 100 percent due to poor sample recovery, sample damage, or disqualification of results which are outside of control limits due to laboratory error or matrix-specific interferences. Completeness is documented by including sufficient information in the laboratory reports to allow the data user to assess the quality of the results. The overall completeness goal for each task is difficult to determine prior to data acquisition. For this project, all reasonable attempts will be made to attain 90% completeness or better (laboratory).

Comparability is a qualitative characteristic which allows for comparison of analytical results with those obtained by other laboratories. This may be accomplished through the use of standard accepted





methodologies, traceability of standards to the National Bureau of Standards (NBS) or USEPA sources, use of appropriate levels of quality control, reporting results in consistent, standard units of measure, and participation in inter-laboratory studies designed to evaluate laboratory performance.

Data quality and the standard commercial report package will be evaluated with respect to PARCC criteria using the laboratory's QA practices, use of standard analytical methods, certifications, participation in interlaboratory studies, temperature control, adherence to hold times, and COC documentation (also called Data Validation).

7.2 Quality Assurance/Quality Control Samples

This section describes the various Quality Assurance/Quality Control (QA/QC) samples that will be collected in the field and analyzed in the laboratory and the frequency at which they will be performed.

7.2.1 Field Equipment Rinsate Blanks

In cases where sampling equipment is not dedicated or disposable, an equipment rinsate blank will be collected. The equipment rinsate blanks are prepared in the field using laboratory-supplied analyte-free water. The water is poured over and through each type of sampling equipment following decontamination and submitted to the laboratory for analysis of target constituents. **One rinsate blank will be collected for every 10 samples.**

7.2.2 Field Duplicates

Field duplicates are collected by sampling the same location twice, but the field duplicate is assigned a unique sample identification number. Samplers will document which location is used for the duplicate sample. One field duplicate will be collected for every 10 samples.

7.2.3 Field Blank

Field blanks are collected in the field using laboratory-supplied analyte-free water. The water is poured directly into the supplied sample containers in the field and submitted to the laboratory for analysis of target constituents. One field blank will be collected for every 10 samples.

7.2.4 Laboratory Quality Control Samples

The laboratory will have an established QC check program using procedural (method) blanks, laboratory control spikes, matrix spikes, and duplicates. Details of the internal QC checks used by the laboratory will be found in the laboratory QAP and the published analytical methods. These QC samples will be used to determine if results may have been affected by field activities or procedures used in sample transportation or if matrix interferences are an issue. One (1) Matrix Spike (MS)/ Matrix Spike Duplicate (MSD) set (i.e. one sample plus one MS, and one MSD sample at one location) will be collected per 20 samples. MS/MSD samples will have a naming convention as follows:



25



Sample: L-LMW-1SMS: L-LMW-1S-MSMSD: L-LMW-1S-MSD

8.0 DATA EVALUATION AND STATISTICAL ANALYSIS

The following sections describe the evaluation and analysis procedures that are followed upon receipt of the analytical report.

26

8.1 Evaluation of Rate and Direction of Groundwater Flow

Groundwater elevations will be determined for each sampling event and will be used to develop a groundwater elevation contour map that will be submitted with reports. The direction of groundwater flow will be determined from up-and downgradient relationships as depicted on the potentiometric surface map. Based on these maps, groundwater flow velocities will be estimated for each event.

8.2 Data Validation

Before the data are used for statistical analysis, they will be evaluated by examining the quality control data accompanying the data report from the laboratory. Relevant quality control data could include measures of accuracy (percent recovery), precision (relative percent difference, RPD), and sample contamination (blank determinations). Data that fail any of these checks will be flagged for further evaluation. A Data Quality Review (DQR) may be initiated with the laboratory for any anomalous data.

8.3 Statistical Analysis

Upon completion of the data validation, the data will be submitted for statistical analysis in compliance with 40 CFR §257.93. The detailed statistical analysis plan for the Facility will be included in **Appendix H**.



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27

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TABLES

Groundwater Level Data LCPB Surface Impoundment

Labadie Energy Center, Franklin County, MO

	Top of Ground Background Event 1 Background Event 1 Casing Surface 3/22/2016 5/3/2016			Background Event 3 Background Event 4 7/11/2016 9/8/2016		Background Event 5 11/11/2016		Background Event 6 1/16/2017		Background Event 7 3/1/2017		Background Event 8 5/31/2017								
Well ID	Northing	Easting	Feet MSL ⁴	Feet MSL ⁴	DTW ²	GWE ³	DTW ²	GWE ³	DTW ²	GWE ³	DTW ²	GWE ³	DTW ²	GWE ³	DTW ²	GWE ³	DTW ²	GWE ³	DTW ²	GWE ³
LMW-1S	990727.7	726039.1	470.06	468.1	11.10	458.96	8.33	461.73	8.14	461.92	11.43	458.63	12.13	457.93	14.75	455.31	15.21	454.85	4.22	465.84
LMW-2S	992017.5	725074.2	496.64	494.9	38.34	458.30	34.49	462.15	35.06	461.58	38.54	458.10	39.74	456.90	42.10	454.54	42.42	454.22	30.81	465.83
LMW-3S	993254.3	725081.6	492.56	490.5	34.74	457.82	30.79	461.77	31.41	461.15	35.04	457.52	36.24	456.32	38.60	453.96	38.88	453.68	27.08	465.48
LMW-4S	994194.9	725624.1	472.88	470.7	15.23	457.65	12.60	460.28	11.93	460.95	15.44	457.44	16.55	456.33	19.22	453.66	19.45	453.43	7.61	465.27
LMW-5S	994201.6	726366.8	468.75	466.9	10.99	457.76	8.75	460.00	7.80	460.95	11.24	457.51	12.13	456.62	14.90	453.85	15.22	453.53	3.59	465.16
LMW-6S	993320.2	726391.4	469.56	467.2	11.57	457.99	8.99	460.57	8.50	461.06	11.92	457.64	12.80	456.76	15.40	454.16	15.83	453.73	4.39	465.17
LMW-7S	992330.1	726371.1	468.43	466.7	10.30	458.13	7.26	461.17	7.25	461.18	10.64	457.79	11.53	456.90	14.11	454.32	14.50	453.93	3.15	465.28
LMW-8S	991371.2	726351.3	467.24	465.2	8.85	458.39	5.84	461.40	5.84	461.40	9.14	458.10	10.00	457.24	12.60	454.64	13.04	454.20	1.88	465.36
BMW-1S	988310.0	715131.6	473.49	471.2	16.40	457.09	9.40	464.09	11.89	461.60	16.30	457.19	18.26	455.23	20.53	452.96	19.74	453.75	6.61	466.88
BMW-2S	987210.1	715104.3	474.56	472.5	17.15	457.41	11.77	462.79	12.44	462.12	16.83	457.73	18.84	455.72	21.32	453.24	20.64	453.92	7.42	467.14
Missouri River	995047.6	723234.9	NA	NA	NA	454.26	NA	464.69	NA	458.15	NA	453.85	NA	451.84	NA	450.11	NA	451.37	NA	464.22

Notes:

- 1.) Groundwater monitoring wells surveyed by Zahner & Associates, Inc. on January 13 and February 11, 2016.
- 2.) DTW Depth to water measured in feet below top of casing.
- 3.) GWE Groundwater elevation measured in feet above mean sea level.
- 4.) MSL Feet above mean sea level.
- 5.) Horizontal Datum: State Plane Coordinates NAD83 (2000) Missouri East Zone feet.
- 6.) Vertical Datum: NAVD88 feet.
- 7.) NA Not Applicable.
- 8.) Missouri River level obtained from United States Geological Survey (USGS) gauge 06935550.

Prepared JSI Check JS/RJF

Reviewed MNH

Generalized Hydraulic Properties of Uppermost Aquifer LCPB Surface Impoundment Labadie Energy Center, Franklin County, MO

	LCPB Compliance Wells										
(LMW-1S, LMW-2S, LMW-3S, LMW-4S, LMW-5S, LMW-6S, LMW-7S, and LMW-8S)											
		Average	Estimated		Mean		Estimated				
Baseline	Baseline	Groundwater	Hydraulic	Hydraulic	Hydraulic	Estimated	Groundwater				
Sampling	Sampling	flow Direction	Gradient	Conductivity	Conductivity	Effective	Velocity				
Event	Event Date	(Azimuth)	(Feet/Foot)	(Feet/Day)	(cm/sec)	Porosity	(Feet/Day)				
1	3/22/2016	350.0	0.0003	52.93	1.9E-02	0.35	0.05				
2	5/3/2016	59.2	0.0009	52.93	1.9E-02	0.35	0.14				
3	7/11/2016	27.5	0.0003	52.93	1.9E-02	0.35	0.04				
4	9/8/2016	359.6	0.0003	52.93	1.9E-02	0.35	0.05				
5	11/11/2016	323.8	0.0004	52.93	1.9E-02	0.35	0.07				
6	1/16/2017	351.0	0.0004	52.93	1.9E-02	0.35	0.06				
7	3/1/2017	3.7	0.0003	52.93	1.9E-02	0.35	0.05				
8	5/31/2017	61.5	0.0003	52.93	1.9E-02	0.35	0.05				

Estimated Results (USEPA Tool)					
Resultant					
Groundwater Flow	20				
Direction (Azimuth)					
Estimated Annual Net					
Groundwater	19				
Movement (Feet/Year)					

Prepared By: JS Checked By: JSI Reviewed By: MNH

Notes:

- 1. Azimuth and Hydraulic Gradient calculated using the United States Environmental protection agency (USEPA) On-Line Tools for Site Assessment Calculation for Hydraulic Gradient (magnitude and direction) available at https://www3.epa.gov/ceampubl/learn2model/part-two/onsite/gradient4plus-ns.html.
- 2. Hydraulic conductivity value is the geometric mean of slug test results for the LCPB compliance wells.
- 3. An effective porosity of 0.35 was used based on grain size distributions and published values (Fetter 2000, Cohen 1953, and Johnson 1967).
- 4. Azimuth is measured clockwise in degrees from north.
- 5. cm/sec centimeters per second.

Monitoring Well Construction Details LCPB Surface Impoundment Labadie Energy Center, Franklin County, MO

		Location ⁴		Top of Casing Elevation	Ground Surface Elevation	Top of Screen	Bottom of Screen	Base of Well	Total Depth
Well ID	Date Installed	Northing	Easting	(FT MSL) ⁵	(FT MSL) ⁵	(FT MSL) ⁵	(FT MSL) ⁵	(FT MSL) ⁵	(FT BGS) ⁵
LMW-1S	11/20/2015	990727.7	726039.1	470.06	468.1	454.5	444.7	444.3	23.8
LMW-2S	11/23/2015	992017.5	725074.2	496.64	494.9	445.8	441.0	440.6	54.3
LMW-3S	2/2/2016	993254.3	725081.6	492.56	490.5	431.0	421.2	420.8	69.7
LMW-4S	11/18/2015	994194.9	725624.1	472.88	470.7	448.3	438.5	438.1	32.7
LMW-5S	11/18/2015	994201.6	726366.8	468.75	466.9	455.0	445.2	444.8	22.1
LMW-6S	11/20/2015	993320.2	726391.4	469.56	467.2	454.7	444.9	444.5	22.8
LMW-7S	11/20/2015	992330.1	726371.1	468.43	466.7	453.4	443.6	443.2	23.5
LMW-8S	11/20/2015	991371.2	726351.3	467.24	465.2	452.2	442.4	442.0	23.2
BMW-1S	2/1/2016	988310.0	715131.6	473.49	471.2	450.7	440.9	440.5	30.7
BMW-2S	2/2/2016	987210.1	715104.3	474.56	472.5	454.6	444.8	444.4	28.1

Notes:

- 1.) All elevations and coordinates were surveyed on January 13, 2016 and February 11, 2016 by Zahner and Associates, Inc.
- 2.) FT MSL = Feet Above Mean Sea Level.
- 3.) FT BGS = Feet Below Ground Surface.
- 4.) Horizontal Datum: State Plane Coordinates NAD83 (2000) Missouri East Zone Feet.
- 5.) Vertical Datum: NAVD88 Feet.

Prepared By: JS Checked By: JSI/MSG Reviewed By:MNH

Groundwater Quality Monitoring Parameters LCPB Surface Impoundment Labadie Energy Center, Franklin County, MO

	Monitoring Parameter	Background ²	Detection ³	Assessment ⁴
Field Parameters	Temperature, pH, Conductivity and Dissolved Oxygen	Х	Х	Х
	Boron	X	Χ	Х
	Calcium	Х	Х	Х
	Chloride	Х	Х	Х
Appendix III ¹	Fluoride	Х	Х	Х
	Sulfate	Х	Х	Х
	рН	Х	Х	Х
	Total Dissolved Solids (TDS)	Х	Х	Х
	Antimony	X		Х
	Arsenic	Х		Х
	Barium	Х		Х
	Beryllium	Х		Х
	Cadmium	Х		Х
	Chromium	X		Х
	Cobalt	Х		Х
Appendix IV ¹	Fluoride	X		Х
• •	Lead	Х		Х
	Lithium	X		Х
	Mercury	Х		Х
	Molybdenum	Х		Х
	Selenium	Х		Х
	Thallium	Х		Х
	Radium 226 & 228	Х		Х

Notes:

- 1.) Analyte lists match requirements for monitoring from USEPA Rule 40 CFR parts 257 and 261.
- 2.) Background will be completed by October 2017 until at least 8 samples are collected.
- 3.) Approximately 6 months will separate each semi-annual sampling event.
- 4.) If necessary, assessment monitoring will be performed in accordance with USEPA Rule.

Prepared By: JS Checked By: MWD Reviewed By: MNH

Analytical Methods and Practical Quantitation Limits LCPB Surface Impoundment Labadie Energy Center, Franklin County, MO

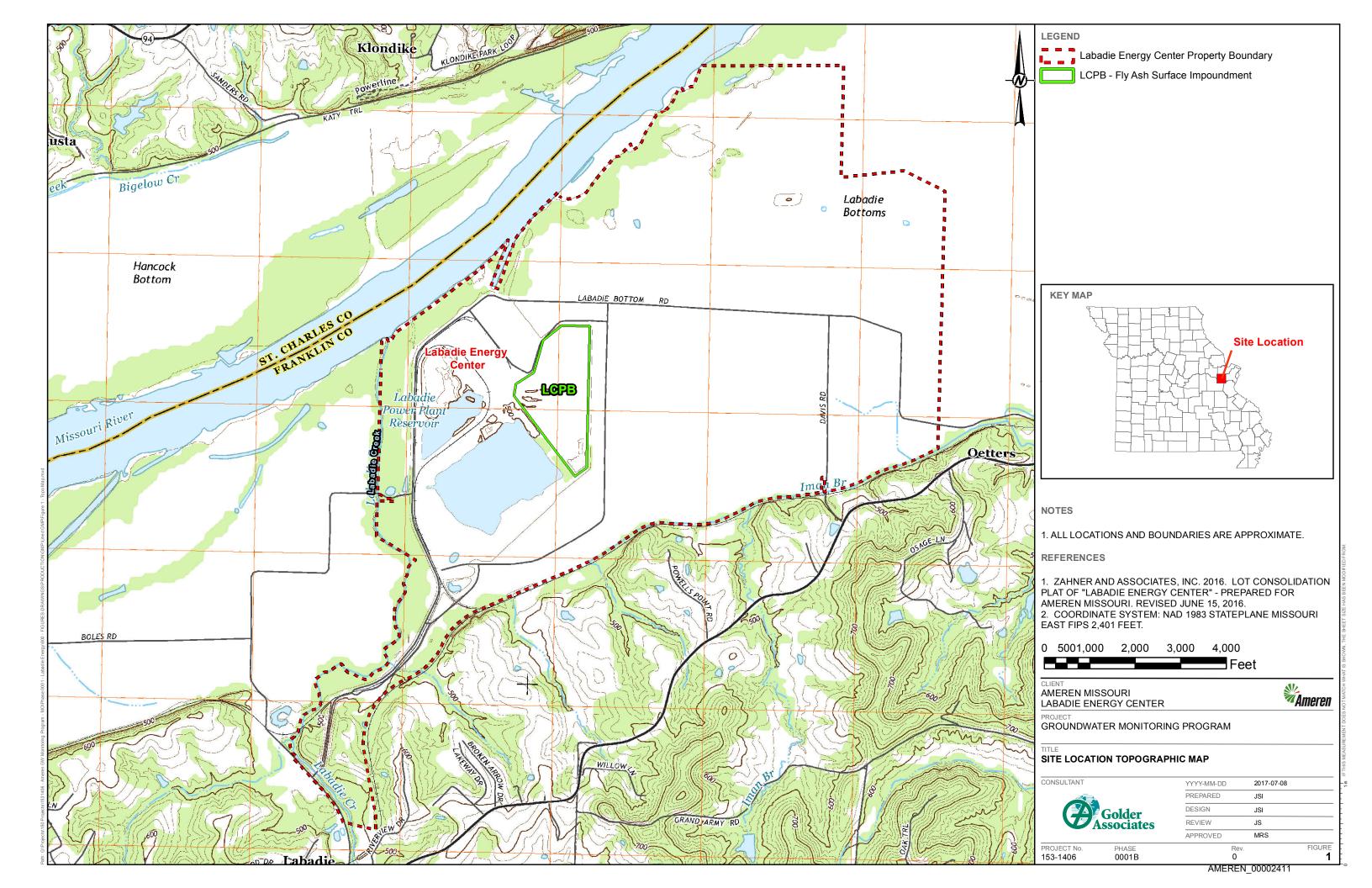
Analyte	Method Reference	Preservative	Hold Times	PQL (μg/L)	MCL (mg/L)
Appendix III - Detection Moni	itoring		_		
Boron	SW-846 6010/MCAWW 200.7	HNO3	6 months	20.0	NA
Calcium	SW-846 6010/MCAWW 200.7	HNO3	6 months	500.0	NA
Chloride	EPA 300.0/325.5/MCAWW 300/SW846 9251/9056	NA	28 days	500.0	NA
Fluoride	EPA 300.0, 300.1	NA	28 days	-	4
рН	4500 H+B-2000	NA	NA	-	NA
Sulfate	EPA 300.0/SW846 300	NA	28 days	2000.0	NA
Total Dissolved Solids (TDS)	2540 C-1997/SM18-20 2540 C	NA	7 days	10000.0	NA
Appendix IV - Assessment Mo	onitoring	•		•	
Antimony	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.006
Arsenic	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.01
Barium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	2.0	2
Beryllium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.004
Cadmium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	0.5	0.005
Chromium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.5	0.1
Cobalt	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	4.0	NP
Fluoride	EPA 300.0	N/A	28 days	-	4
Lead	SW-846 6020	HNO3	6 months	0.005	0.015
Lithium	SW-846 6010	HNO3	6 months	-	NA
Mercury	SW-846 7470	HNO3	28 days	-	0.002
Molybdenum	SW-846 6010	HNO3	6 months	-	NP
Selenium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	1.0	0.05
Thallium	SW-846 6010/6020/MCAWW 200.7/200.8	HNO3	6 months	0.2	0.002
Radium 226 & 228	SW-846 903.1/SM 6500 904	-	-	1.0 (pCi/L)	5.0 (pCi/L)

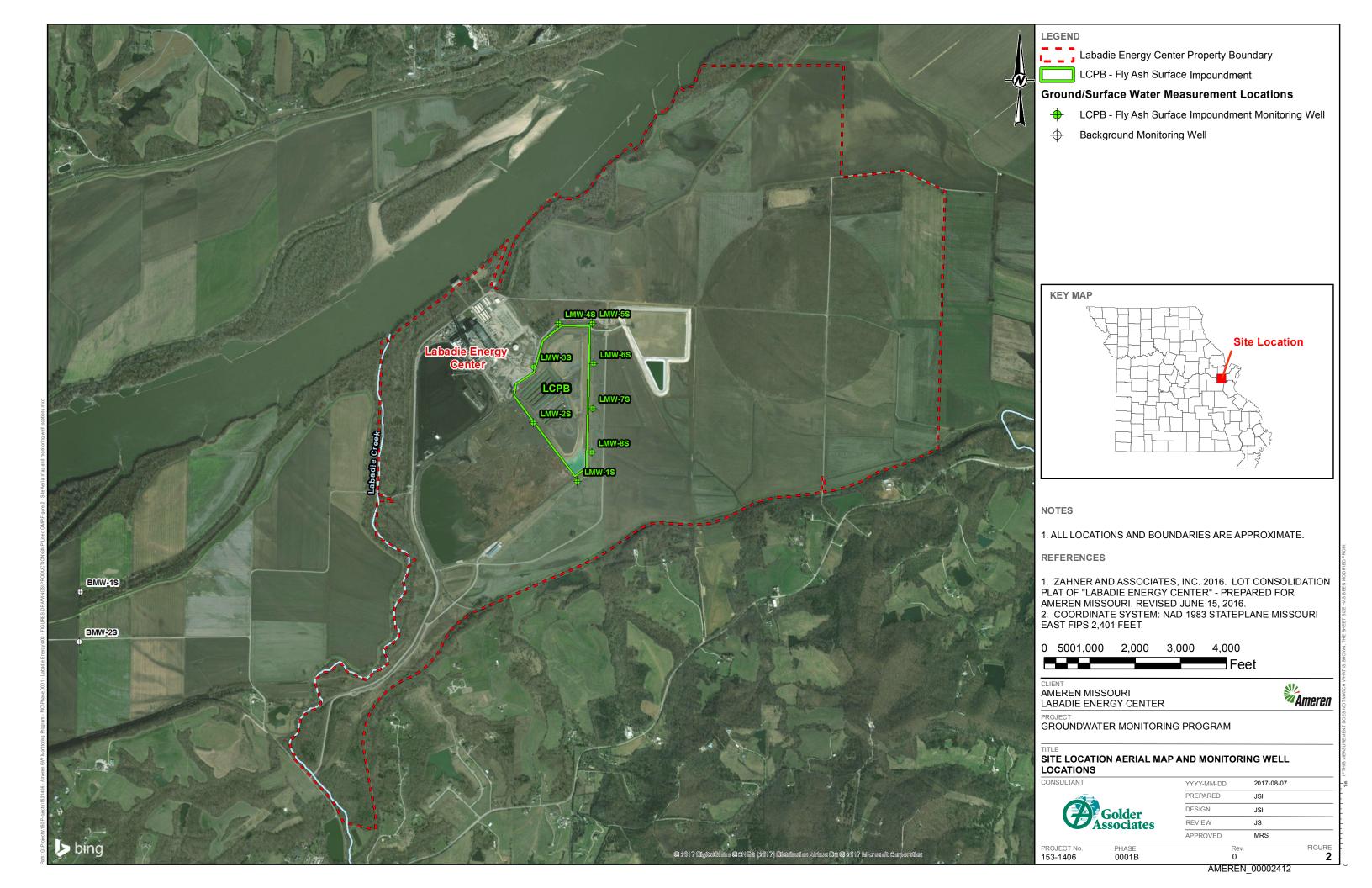
Notes:

- 1.) NA not applicable.
- 2.) Analyte lists matches requirements for detection and assessment monitoring from United States Environmental Protection Agency (USEPA) Rule 40 CFR parts 257 and 261.
- 3.) SW-846 denotes Test Methods for Evaluating Solid Waste, Physical- Chemical Methods, EPA publication SW-846, 3rd edition, and subsequent updates.
- 4.) MCAWW denotes Methods for the Chemical Analysis of Water and Wastes (MCAWW), United States Environmental Protection Agency (USEPA) published in the 1983.
- 5.) EPA 300 denotes Methods for the Determination of Organic Compounds in Drinking Water Environmental Monitoring Systems Laboratory, Office of Research and Development, USEPA, Cincinnati, Ohio 45268. EPA-300/4-88/039, December 1988 (Revised July 1991).
- 6.) SM18-20 denotes Standard Methods for the Examination of Water and Wastewater, 18th, 19th, and 20th Editions, published by the American Public Health Association, Water Environment Federation, and the American Water Works Association.
- 7.) Other industry-used or agency-approved methods may be used provided that they produce the necessary level of precision and accuracy for data use and reporting.
- 8.) Updates to the methods listed here are approved for use.
- 9.) PQL Practical Quantitation Limit.
- 10.) MCL Maximum Contaminant Level from USEPA 2014 Edition of the Drinking Water Standards and Health Advisories. October 2014. http://water.epa.gov/drink/contaminants/index.cfm.
- 11.) Dash (-) Indicates no information available.
- 12.) μg/L Micrograms per liter.
- 13.) pCi/L Picocuries per liter.
- 14.) NP Not Promulgated.
- 15.) mg/L Milligrams per liter.

Prepared By: JS Checked By: MWD Reviewed By: MRS

FIGURES





Generalized Cross-Section 700 700 675 675 650 650 625 625 Typical Monitoring Well 600 600 Groundwater Level (Varies) 575 575 Labadie Energy Center 550 550 Overview Map Property Boundary - LCPA Surface Missouri River 525 525 Impoundment Coal Pile 500 500 475 475 CCR 450 450 425 425 Alluvial Aquifer 375 375 350 350 325 325 300 300 Bedrock 275 275 Aquifer 250 250 225 1000 1500 2000 2500 3000 3500 4000 4500 5000 5500 6000 6500 7000 7500 8000 8500 9000 9500 10000 10500 North South Distance (feet) NOT TO SCALE **REFERENCES** NOTES 1.) ALL LOCATIONS AND BOUNDARIES ARE APPROXIMATE. 1.) AMEREN, 2011. AMEREN MISSOURI LABADIE ENERGY **Ameren** AMEREN MISSOURI GROUNDWATER MONITORING PROGRAM 2.) CROSS-SECTION IS NOT TO SCALE AND IS ONLY A VISUAL CENTER, LABADIE PROPERTY CONTROL MAP, NOVEMBER 2011 LABADIE ENERGY CENTER REPRESENTATION OF THE SUBSURFACE GEOLOGY AND 2.) GREDELL ENGINEERING RESOURCES, INC., AND REITZ & FEATURES. JENS. 2011. DETAILED SITE INVESTIGATION REPORT FOR: CONSULTANT YYYY-MM-DD 3.) MSL - MEAN SEA LEVEL. AMEREN MISSOURI LABADIE POWER PLANT PROPOSED **GENERALIZED CROSS-SECTION** DESIGNED JSI UTILITY WASTE DISPOSAL AREA FRANKLIN COUNTY, MISSOURI. PREPARED JSI REVIEWED FIGURE 3 153-1406 0001 APPROVED AMEREN_00002413

APPENDIX A CCR MONITORING WELL BORING LOGS

RECORD OF BOREHOLE LMW-1S SHEET 1 of 1 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 468.09 DRILLING INIE 11/05. 0 GGIIG DRILLING DATE: 11/20/2015 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 990,727.65 E: 726,039.06 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-1.0) FILL - (SW) SAND, fine to coarse sub-rounded sand, trace gravel; dusky yellowish brown (10YR 2/2); non-cohesive, dry, loose sw (1.0-5.0) (ML) SILT, non-plastic fines, some fine sand, some organics (roots), trace gravel; brownish gray (5YR 4/1) to medium dark gray (N4); non-cohesive, dry, compact 1 SO ML - 5 (5.0-10.0) (CL) SILTY CLAY, medium plasticity fines, some fine sand; brownish gray (5YR 4/1); cohesive, w<PL, stiff SO CL 10 (10.0-13.0) (SP-SM) SAND, fine sand, some non-plastic (10.0) Hole collapsed to 8.0 feet below ground surface. Measured field recovery is more than estimated actual recovery due to hole collapse. Measured field recovery: 7.8/10.0, Estimated actual recovery: fines; dark yellowish brown (10YR 4/2); non-cohesive, moist, compact SP-SM 5.8/10.0. Sonic 6 (13.0-15.0) (SM) SILTY SAND, fine sand, some non-plastic fines; dark yellowish brown (10YR 4/2); non-cohesive, wet, compact SM 5.8 10.0 - 15 3 SO (15.0-25.0) (SP) SAND, fine to medium sub-rounded (15.0-25.0) Soil description based off of sand, trace sub-rounded gravel, trace non-plastic fines; dark yellowish brown (10YR 4/2) to medium gray (N5); laboratory grain size analysis. non-cohesive, wet, compact 20 SW 10/9/1 CO.GDT GLDR SO LEC LOGS.GPJ - 25 END OF BORING AT 25.0 FT BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION BOREHOLE MWD RECORD OF GOLDER STL LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

PR	OJECT	RECOR : Ameren CCR GW Monitoring : NUMBER: 153-1406.0001B : Labadie Energy Center RECOR DRILLING METI DRILL RIG: Mir	HOD: 6" So E: 11/22/20	onic 115	DATU AZIMI	JM: NAVD UTH: N/A	88	01751 F	SHEET 1 of 2 ELEVATION: 494.89 INCLINATION: -90
		SOIL/ROCK PROF		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	000.	RDINATES: N: 992,017.51 E SAMPLES			. 720,071.21
DEPTH (feet)	BORING METHOD	DESCRIPTION	USCS	GRAPHIC LOG	ELEVATION DEPTH	N NUMBER	TYPE	REC ATT	REMARKS
0 -	<u> </u>	(0.0-5.0) Hydrovac			(ft)			 	(0.0-5.0) Hydrovac material. No samples
									collected.
			NA			NA	NA	<u>0.0</u> 5.0	
					489.9				
- 5		(5.0-10.0) (ML) SILT, non-plastic fines, some fine sand, dusky yellowish brown (10YR 2/2); non-cohesive, dry, loose			5.0				
-			ML			2	SO	<u>5.0</u> 5.0	
- - 10					484.9				
_ 10		(10.0-15.0) No Recovery			10.0				Run #2, No recovery, sample appears to have washed out of bit.
-			NA			3	so	<u>0.0</u> 5.0	
_ 15	Sonic				479.9				_
	9.9	(15.0-20.0) (ML) SILT, non-plastic fines, trace fine sand, trace sub-rounded gravel; dusky yellowish brown (10YR 2/2); non-cohesive, dry, loose			15.0				
			ML			4	so	<u>5.0</u> 5.0	
-									
- 20		(20.0-27.5) (ML) SILT, non-plastic fines, some fine sand; moderate brown (5YR 3/4); non-cohesive, dry, compact			474.9 20.0				-
50									
Z Z						5	so	<u>3.9</u> 5.0	
25			ML						_
		(27.5-32.1) (SM) SILTY SAND, fine poorly graded sand,			467.4 27.5	- 6	so	<u>4.5</u> 5.0	
- 20 - 25 - 25 - 25 - 25 - 25 - 25 - 25		non-plastic fines; greenish black (5GY 2/1); non-cohesive, dry, compact	SM						
30		Log continued on next page							-
SCA DRI	LLING	1 in = 3.8 ft G CONTRACTOR: Cascade		CHEC	ED: JS KED: JSI		_		Golder Associates
	LLEK	: J. Drabek		KEVIE	WED: P	JJ/IVINH			ASSOCIATES

RECORD OF BOREHOLE LMW-2S SHEET 2 of 2 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 494.89 DRILLING METHOD: 0 Sonic
DRILLING DATE: 11/22/2015
DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 992,017.51 E: 725,074.21 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS NUMBER DESCRIPTION TYPE USCS DEPTH (ft) - 30 (27.5-32.1) (SM) SILTY SAND, fine poorly graded sand, non-plastic fines; greenish black (5GY 2/1); non-cohesive, dry, compact *(Continued)* SM (32.1-38.0) (ML) sandy SILT, non-plastic to low plasticity fines, fine sand; dark yellowish brown (10YR 4/2); non-cohesive, moist, compact 10.0 10.0 - 35 7 SO ML Water Level 36.31
 Water Level 36.31 ft bgs 3/14/2016 (38.0-40.0) (SM) SILTY SAND, poorly graded fine sand, non-plastic fines; dark yellowish brown (10YR 4/2); non-cohesive, moist, compact SM 40 (40.0-44.0) (SP) SAND, fine sand, non-plastic fines pockets; moderate yellowish brown (10YR 5/4); non-cohesive, moist, compact SP Sonic 6 (44.0-55.0) (SP) SAND, fine sand, trace non-plastic fines; medium dark gray (N5); non-cohesive, moist, 10.0 10.0 - 45 8 SO SP - 50 (50.0) Pause drilling overnight. Continue drilling @0730 on 11/23/2015 RECORD OF BOREHOLE MWD LEC LOGS.GPJ GLDR_CO.GDT 10/9/1 9 SO - 55 END OF BORING AT 55.0 FT BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION GOLDER STL LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE LMW-3S SHEET 1 of 3 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 490.5 DRILLING INIE 1110D. 0 GGIIIG DRILLING DATE: 2/2/2016 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 993,254.34 E: 725,081.60 SAMPLES SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS BORING NUMBER DESCRIPTION USCS TYPE DEPTH - 0 Run #1, Sample appears to be compacted while being extruded into sample bags. Measured field recovery: 3.2/5.0 Estimated actual recovery: 4.9/5.0. (0.0-0.5) TOPSOIL - (ML) sandy SILT, non-plastic fines, ML fine to medium sub-angular sand; dark yellowish brown (10YR 4/2); non-cohesive, moist, loose (0.5-19.5) FILL - (SP) SAND, fine to medium sub-rounded sand, trace non-plastic fines and trace medium plasticity fines pockets; moderate yellowish brown (10YR 5/4); non-cohesive, moist, loose 1 SO 485.5 - 5 (5.0) SAA (Same As Above) except, trace fine Run #2, Sample appears to be compacted while being extruded into sample bags. Measured field recovery: 3.5/5.0 Estimated actual recovery: 5.0/5.0. sub-rounded gravel SO 480.5 10 SP Run #3, Driller gets no recovery when attempting to sample 10.0 to 15.0 feet. Driller then attempts to try 10 foot run from 10.0 to 20.0. Run #3, Driller makes multiple attempts at (10.0) SAA except, some coarse sand; dry 10.0 10 foot run, eventually gets sample to surface but it is very mixed up due to multiple sample attempts. Sonic 7.3 10.0 - 15 3 SO 6 (19.5-21.0) (ML) sandy SILT, non-plastic fines; trace medium plasticity fines pockets, fine sand; medium gray 20 10/9/ ML (N5); non-cohesive, wet, loose CO.GDT (21.0-23.7) (ML) sandy CLAYEY SILT, low plasticity fines, fine to coarse sub-rounded to sub-angular sand, trace sub-angular gravel; medium gray (N5); cohesive, ML GLDR LEC LOGS.GPJ (23.7-40.0) (SC) CLAYEY SAND, fine sand, medium plasticity fines, some non-plastic fines, trace sub-angular gravels; medium gray (N5); non-cohesive, moist, compact 6.7 10.0 - 25 SO BOREHOLE MWD SC RECORD OF 460.5 Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JSI/JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE LMW-3S SHEET 2 of 3 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 490.5 DRILLING DATE: 2/2/2016
DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 993,254.34 E: 725,081.60 SOIL/ROCK PROFILE SAMPLES **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) (23.7-40.0) (SC) CLAYEY SAND, fine sand, medium plasticity fines, some non-plastic fines, trace sub-angular gravels; medium gray (N5); non-cohesive, moist, compact (Continued) - 30 30.0 (30.0) SAA except, wet ft bgs 3/14/2016 7.4 10.0 - 35 SC 5 SO 40 (40.0-47.1) (SC) CLAYEY SAND, fine sand, some (40.447.1) (30) CEATET SAND, IIII saint, Some mon-plastic fines, some medium plasticity fines pockets (~3 inches in diameter, approximately every 2 ft), trace sub-angular gravel; medium gray (N5); non-cohesive, wet, compact SC Sonic 445.5 - 45 6 SO (45.0) SAA except, light olive gray (5Y 5/2) 6 (47.1-54.5) (CL) sandy SILTY CLAY, medium plasticity fines, some non-plastic fines, fine sand; medium dark gray (N4); cohesive, w~PL, firm - 50 10/9/1 CL CO.GDT GLDR LEC LOGS.GPJ (54.5-57.9) (CL) SILTY CLAY, medium to high plasticity, some fine sand; medium dark gray (N4); cohesive, 7.1 10.0 - 55 7 SO BOREHOLE MWD CL (57.9-60.0) (SC) CLAYEY SAND, fine to medium sub-rounded sand, medium plasticity fines; medium gray Run #7, Medium plasticity fines could be fall in from above formation caused by drill rig RECORD OF (N5); non-cohesive, wet, compact vibrations SC 430.5 Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JSI/JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE LMW-3S SHEET 3 of 3 DRILLING METHOD: 6" Sonic DRILLING DATE: 2/2/2016 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DATUM: NAVD88 ELEVATION: 490.5 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 993,254.34 E: 725,081.60 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 60 (60.0-70.0) (SW) SAND, fine to coarse sub-rounded sand, some fine to coarse sub-rounded gravels; trace non-plastic fines; medium gray (N5); non-cohesive, wet, compact 60.0 Run #8, Sample appears to be compacted while being extruded into sample bags. Measured field recovery: 5.5/10.0 Estimated actual recovery: 8.7/10.0. Sonic <u>8.7</u> 10.0 - 65 SW 8 SO - 70 END OF BORING AT 70.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG LMW-3S. - 75 GOLDER STL RECORD OF BOREHOLE MWD LEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 80 - 85 LOGGED: JSI/JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE LMW-4S SHEET 1 of 2 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 470.74 DRILLING INIE 11/05. 0 GGIIG DRILLING DATE: 11/18/2015 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 994,194.85 E: 725,624.12 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS NUMBER DESCRIPTION TYPE USCS DEPTH (ft) - 0 (0.0-1.0) TOPSOIL - (CL) SILTY CLAY, medium plasticity fines, some fine sand, some organics (roots), trace gravel; dark yellowish brown (10YR 4/2); cohesive, w-PL, soft CL (1.0-2.7) (CL) SILTY CLAY, low to medium plasticity CL fines, trace fine sand; dark yellowish brown (10YR 4/2); cohesive, w~PL, soft 468.0 1 SO (2.7-3.0) (GW) GRAVEL, fine to coarse sub-angular gravel, some fine to medium sand, some non-plastic fines; grayish orange (5Y 8/4); non-cohesive, moist, GW 467.7 (3.0-7.7) (ML) CLAYEY SILT, low plasticity fines, some fine sand; brownish gray (5YR 4/1); cohesive, w<PL, soft 465.7 - 5 (5.0) SAA (Same As Above) except, some sub-angular МН 463.0 7.7 (7.7-20.0) (SP) SAND, fine sand; light brownish gray (5YR 6/1) to grayish orange (10YR 7/11); non-cohesive, 10 Run #3, Sample appears to be compacted while being extruded into sample bags. Measured field recovery: 2.4/5.0 Estimated actual recovery: 3.4/5.0. Run #3, Driller notes mosture is due to drilling fluid and not actual formation moisture. 3.4 5.0 SO 3 SP Sonic 455.7 - 15 (15.0) SAA except, fine to medium sub-rounded sand; 6 moist SO 20 10/9/1 (20.0-33.0) (SW) SAND, fine to coarse sub-rounded sand, trace fine gravel; light brownish gray (5YR 6/1) to medium gray (N5); non-cohesive, wet, compact CO.GDT GLDR LEC LOGS.GPJ 9.5 10.0 - 25 SW 5 SO BOREHOLE MWD RECORD OF Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JSI/JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE LMW-4S SHEET 2 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 11/18/2015 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DATUM: NAVD88 ELEVATION: 470.74 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 994,194.85 E: 725,624.12 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 30 Run #6, No recovery due to loose sands being pushed out of way as the bit advances. Poor recovery could also be due to washing out of sands as the sampler is retrieved. Driller notes material felt same as above. (SW) SAND was found in drill bit after run. (20.0-33.0) (SW) SAND, fine to coarse sub-rounded sand, trace fine gravel; light brownish gray (5YR 6/1) to medium gray (N5); non-cohesive, wet, compact (Continued) Sonic <u>0.0</u> 3.0 SW SO 6 END OF BORING AT 33.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION - 35 40 - 45 GOLDER STL RECORD OF BOREHOLE MWD LEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 50 - 55 LOGGED: JSI/JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

RECORD OF BOREHOLE LMW-5S SHEET 1 of 1 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 466.86 DRILLING METHOD: 0 Some DRILLING DATE: 11/18/2015 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 994,201.59 E: 726,366.81 SOIL/ROCK PROFILE SAMPLES **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-1.0) TOPSOIL - (CL) SILTY CLAY, medium plasticity fines, some fine sand; dark yellowish brown (10YR 4/2); cohesive, w~PL, soft CL (1.0-2.7) (CL) SILTY CLAY, medium plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2); CL cohesive, w~PL, soft 3.7 5.0 1 SO (2.7-6.0) (ML) CLAYEY SILT, low plasticity fines, some fine sand; brownish gray (5YR 4/1); cohesive, w<PL, soft ML - 5 (6.0-11.5) (ML) sandy SILT, non-plastic fines, fine sand; brownish gray (5YR 4/1); non-cohesive, compact, moist Water Level 8.65 ft
 ML bgs 3/14/2016 10 Run #3, Excess recovery collected in sample bag due to clay swelling. Measured field recovery: 6.0/5.0 Estimated actual recovery: 5.0/5.0. (11.5-13.5) (SP & ML) SAND & SILT, fine sand, Sonic non-plastic fines; light brownish gray (5YR 6/1); non-cohesive, moist, compact SO & ML 3 (13.5-25.0) (SP) SAND, fine to medium sub-rounded sand; light brownish gray (5YR 6/1) to pale yellowish brown (10YR 6/2); non-cohesive, moist, compact - 15 SP - 20 SO 10/9/1 CO.GDT LEC LOGS.GPJ GLDR - 25 END OF BORING AT 25.0 FEET BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION RECORD OF BOREHOLE MWD GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JSI/JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE LMW-6S SHEET 1 of 1 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 467.23 DRILLING METHOD: 0 Some DRILLING DATE: 11/20/2015 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 993,320.17 E: 726,391.38 SOIL/ROCK PROFILE SAMPLES **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 0 (0.0-4.0) (CL) SILTY CLAY, medium plasticity fines; dark yellowish brown (10YR 4/2); cohesive, w<PL, stiff CL 1 SO 463.2 4.0 (4.0-5.0) (ML) sandy CLAYEY SILT, medium plasticity fines, fine sand; dark yellowish brown (10YR 4/2); ML cohesive, w<PL, stiff - 5 (5.0-8.2) (SM) SILTY SAND, fine sand, non-plastic fines; dark yellowish brown (10YR 4/2); non-cohesive, moist, SM (8.2-10.0) (ML) CLAYEY SILT, medium plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2); cohesive, w<PL, stiff bgs 3/14/2016 ML 10 (10.0-21.7) (SP) SAND, fine sand; dark yellowish brown (10YR 4/2); non-cohesive, moist, compact Sonic SO 3 6 452.2 - 15 (15.0) SAA (Same As Above) except, dark yellowish brown (10YR 4/2) to medium gray (N5) SP - 20 SO 10/9/1 CO.GDT (21.7-25.0) (SW) SAND, fine to coarse sub-rounded sand, trace sub-rounded gravel; medium dark gray (N4); LEC LOGS.GPJ GLDR non-cohesive, wet, compact SW - 25 END OF BORING AT 25.0 FT BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION RECORD OF BOREHOLE MWD GOLDER STL LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE LMW-7S SHEET 1 of 1 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 466.69 DRILLING METHOD: 0 Some DRILLING DATE: 11/20/2015 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 992,330.13 E: 726,371.14 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 0 (0.0-5.0) (CL) SILTY CLAY, medium plasticity fines, trace fine sand, trace organic material; dark yellowish brown (10YR 4/2); cohesive, w~PL, stiff CL 1 SO - 5 (5.0-7.5) (CL) SILTY CLAY, medium plasticity fines, some fine sand; moderate yellowish brown (10YR 5/4); cohesive, w~PL, firm CL 2 (7.5-22.0) (SP) SAND, fine sand; moderate yellowish Water Level 8.16 ft brown (10YR 5/4); non-cohesive, moist, compact bgs 3/14/2016 456.7 10 (10.0) SAA (Same As Above) except, trace fines 10.0 Sonic SO 3 6 SP 451.7 - 15 (15.0) SAA except, medium gray (N5) GOLDER STL RECORD OF BOREHOLE MWD LEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 20 SO (22.0-25.0) (SW) SAND, fine to coarse sand; medium gray (N5); non-cohesive, wet, compact SW - 25 END OF BORING AT 25.0 FT BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION LOGGED: JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

RECORD OF BOREHOLE LMW-8S SHEET 1 of 1 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 465.24 DRILLING METHOD: 0 Some DRILLING DATE: 11/20/2015 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 991,371.23 E: 726,351.28 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER TYPE USCS DEPTH - 0 (0.0-4.6) (CL) SILTY CLAY, medium plasticity fines, trace fine sand; dark yellowish brown (10YR 4/2); cohesive, w~PL, firm CL 2.0 5.0 1 SO (4.6-10.0) (SP) SAND, fine sand; moderate yellowish - 5 brown (10YR 5/4); non-cohesive, dry, loose bgs 3/14/2016 SP 10 (10.0-13.0) (SM) SILTY SAND, fine sand, non-plastic fines; moderate yellowish brown (10YR 5/4); non-cohesive, moist, compact SM SO 3 (13.0-23.2) Soil description based off of laboratory grain size analysis. (13.0-23.2) (SP-SM) SAND, fine to medium sand, some non-plastic fines; moderate yellowish brown (10YR 5/4); non-cohesive, moist, compact - 15 SP 8.0 8.2 SO GOLDER STL RECORD OF BOREHOLE MWD LEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 20 END OF BORING AT 23.2 FT BELOW GROUND SURFACE.
FOR WELL DETAILS, SEE WELL CONSTRUCTION - 25 LOGGED: JSI/JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

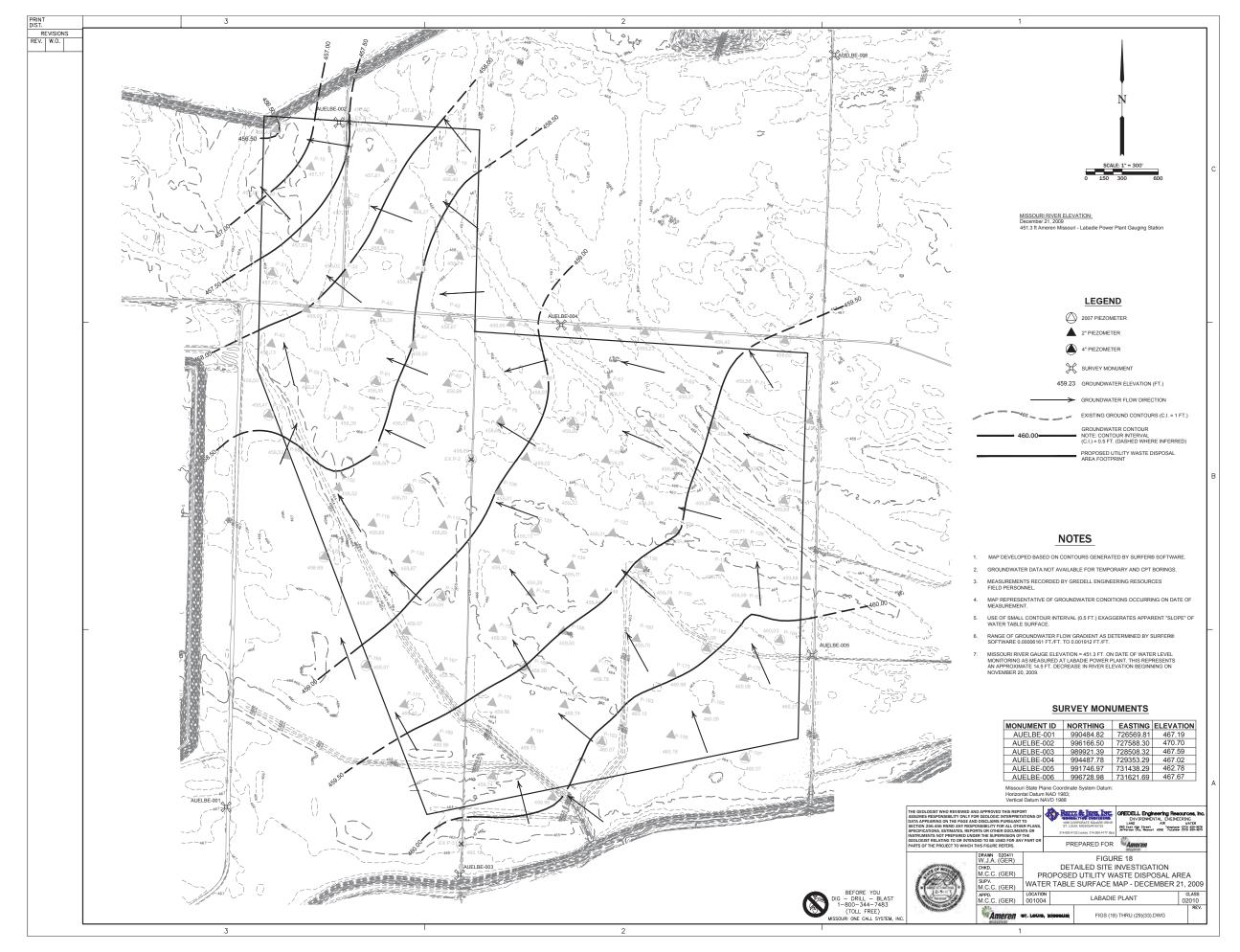
RECORD OF BOREHOLE BMW-1S SHEET 1 of 2 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DATUM: NAVD88 ELEVATION: 471.17 DRILLING INE 1110D. 0 GGIIIG DRILLING DATE: 2/1/2016 DRILL RIG: Mini Sonic (CDD1415) AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 988,310.02 E: 715,131.61 SAMPLES **BORING METHOD** SOIL/ROCK PROFILE DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT NUMBER DESCRIPTION TYPE USCS DEPTH - 0 (0.0-6.5) (ML) CLAYEY SILT, low to medium plasticity fines, some organics (roots), some fine sand; brownish gray (5YR 4/1); cohesive, w<PL, firm 2.1 5.0 1 SO ML 466.2 - 5 (5.0) SAA (Same As Above) except, no organics (6.5-9.3) (CL) SILTY CLAY, medium plasticity fines trace fine sand, trace iron staining; brownish gray (5YR 4/1) mottled with dark yellowish orange (10YR 6/6) and moderate yellowish brown (10YR 5/4); cohesive, w~PL, SO CL (9.3-10.0) (SP-SM) SAND, fine sand, some non-plastic fines; brownish gray (5YR 4/1); non-cohesive, moist, 9.3 SP-SM 10 compact (10.0-17.9) (SM) SILTY SAND, fine sand, low to non-plastic fines; brownish gray (5YR 4/1); non-cohesive, wet, compact SM ft bgs 3/14/2016 Sonic - 15 3 SO 6 454.9 16.3 (16.3) SAA except, color to medium gray (N5) (17.9-18.6) (CL) SILTY CLAY, medium plasticity, some fine sand; medium gray (N5); cohesive, w-PL, firm (18.6-30.7) (SP) SAND, fine sand, trace non-plastic CL 452.6 fines; medium gray (N5); non-cohesive, wet, compact 20 10/9/1 Run #4, Sample appears to be compacted while being extruded into sample bags. Measured field recovery: 4.2/10.71 Estimated actual recovery: 7.3/10.71. CO.GDT GLDR LEC LOGS.GPJ SP 7.3 10.7 so - 25 4 (25.0) SAA except, trace subrounded gravels, some medium grained subrounded sand 25.0 BOREHOLE MWD RECORD OF Log continued on next page GOLDER STL SCALE: 1 in = 3.8 ft LOGGED: JSI/JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

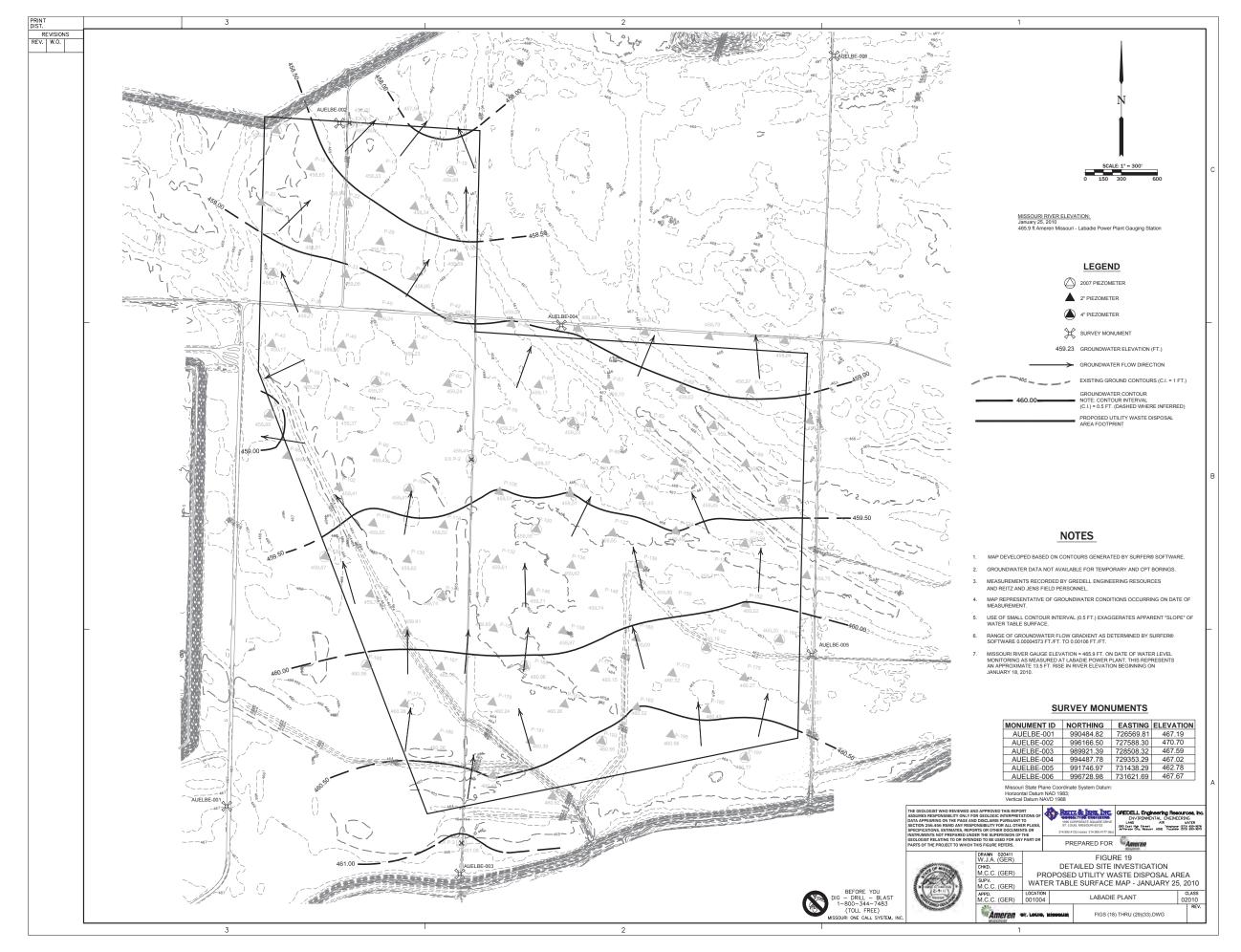
	RECORD OF BOREHOLE BMW-1S SHEET 2 of 2										
	PROJECT LOCATION		Ameren CCR GW Monitoring NUMBER: 153-1406.0001B : Labadie Energy Center DRILLING METHOD: 6" Soi DRILLING DATE: 2/1/2016 DRILL RIG: Mini Sonic (CDI			AZIMUTH: N/A				ELEVATION: 471.17 INCLINATION: -90 :: 715,131.61	
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	DEPTH (feet)	BORING METHOD	DESCRIPTION		USCS	GRAPHIC LOG	ELEVATION	NUMBER	TYPE	REC	REMARKS
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	_		SURFACE. FOR WELL DETAILS, SEE WELL CO LOG BMW-1S.				00.7				-
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L RECC	60										_
SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade DRILLER: J. Drabek LOGGED: JSI/JS CHECKED: JSI REVIEWED: PJJ/MNH								Golder Associates			

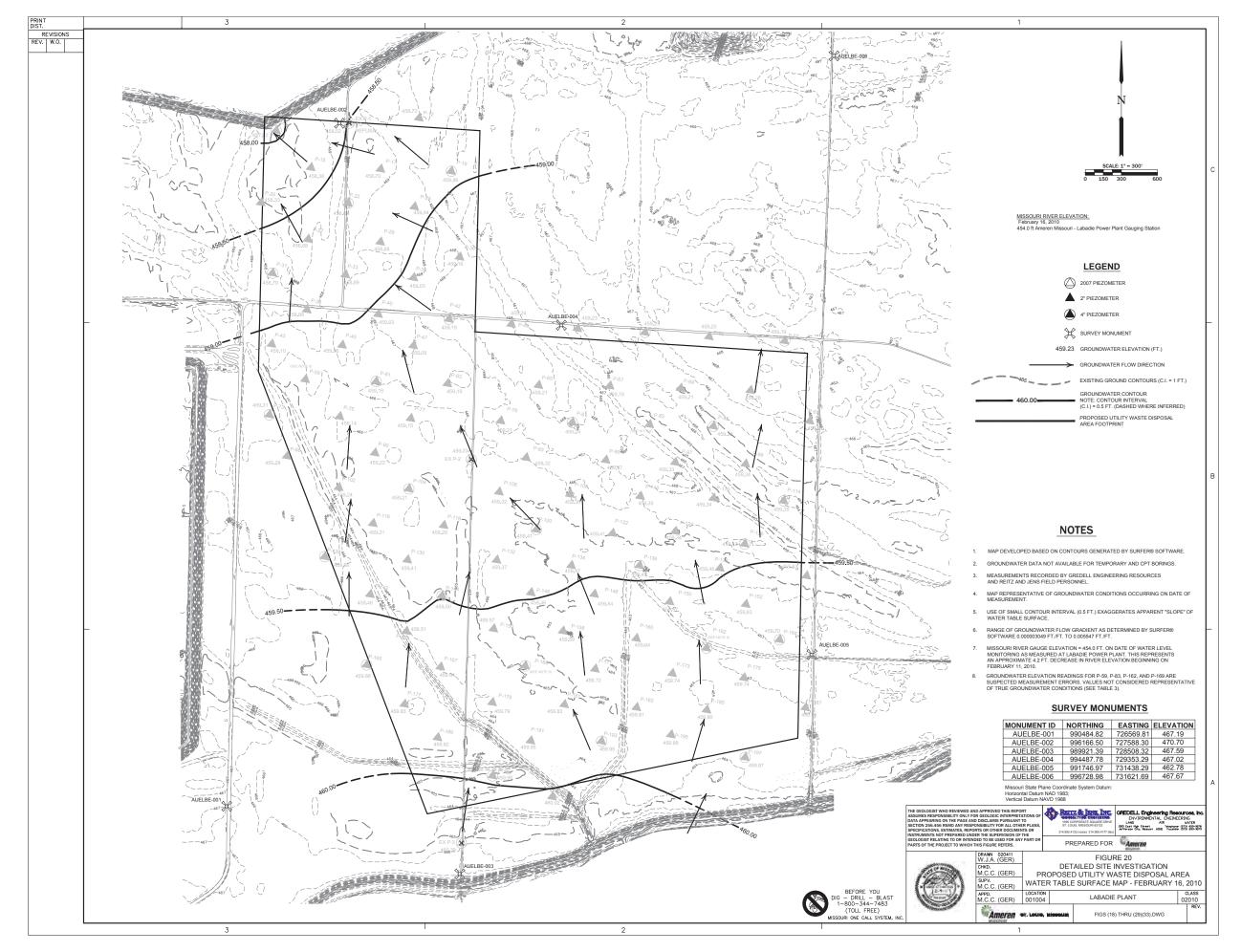
RECORD OF BOREHOLE BMW-2S SHEET 1 of 2 DRILLING METHOD: 6" Sonic DRILLING DATE: 2/2/2016 DRILL RIG: Mini Sonic (CDD1415) PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOÇATION: Labadie Energy Center DATUM: NAVD88 ELEVATION: 472.48 AZIMUTH: N/A INCLINATION: -90 COORDINATES: N: 987,210.08 E: 715,104.29 SAMPLES SOIL/ROCK PROFILE **BORING METHOD** DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS REC ATT DESCRIPTION NUMBER TYPE USCS DEPTH (ft) - 0 (0.0-4.0) (ML) CLAYEY SILT, low plasticity fines, some fine to coarse sub-angular sand, some organics (roots); brownish gray (5YR 4/1); cohesive, w<PL, firm ML 2.3 5.0 1 SO Run #1, Sand in last foot of run appears to have washed out. 468.5 4.0 $\overline{(4.0\text{--}30.0)}\ \overline{(\text{SP)}\ \text{SAND}}, \ \overline{\text{fine sand}}, \ \overline{\text{trace non-plastic fines}}; \\ \overline{\text{moderate yellowish brown (10YR 5/4); non-cohesive,}}$ dry, loose - 5 - 10 SO 3 Sonic 457.5 - 15 ft bgs 3/14/2016 (15.0) SAA (Same As Above) except, wet, fine to 6 medium sub-rounded sand SP 4 SO GOLDER STL RECORD OF BOREHOLE MWD LEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 20 450.5 22.0 (22.0-27.0) SAA except, trace coarse sand 447.5 25.0 - 25 so 5 (25.0) SAA except, mottled dark yellowish orange (10YR 6/6) and dark yellowish brown (10YR 4/2) 444.5 28.0 (28.0) SAA except, color to light olive gray (5Y 5/2) 442.5 - 30 Log continued on next page SCALE: 1 in = 3.8 ft LOGGED: JSI/JS DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH **Associates**

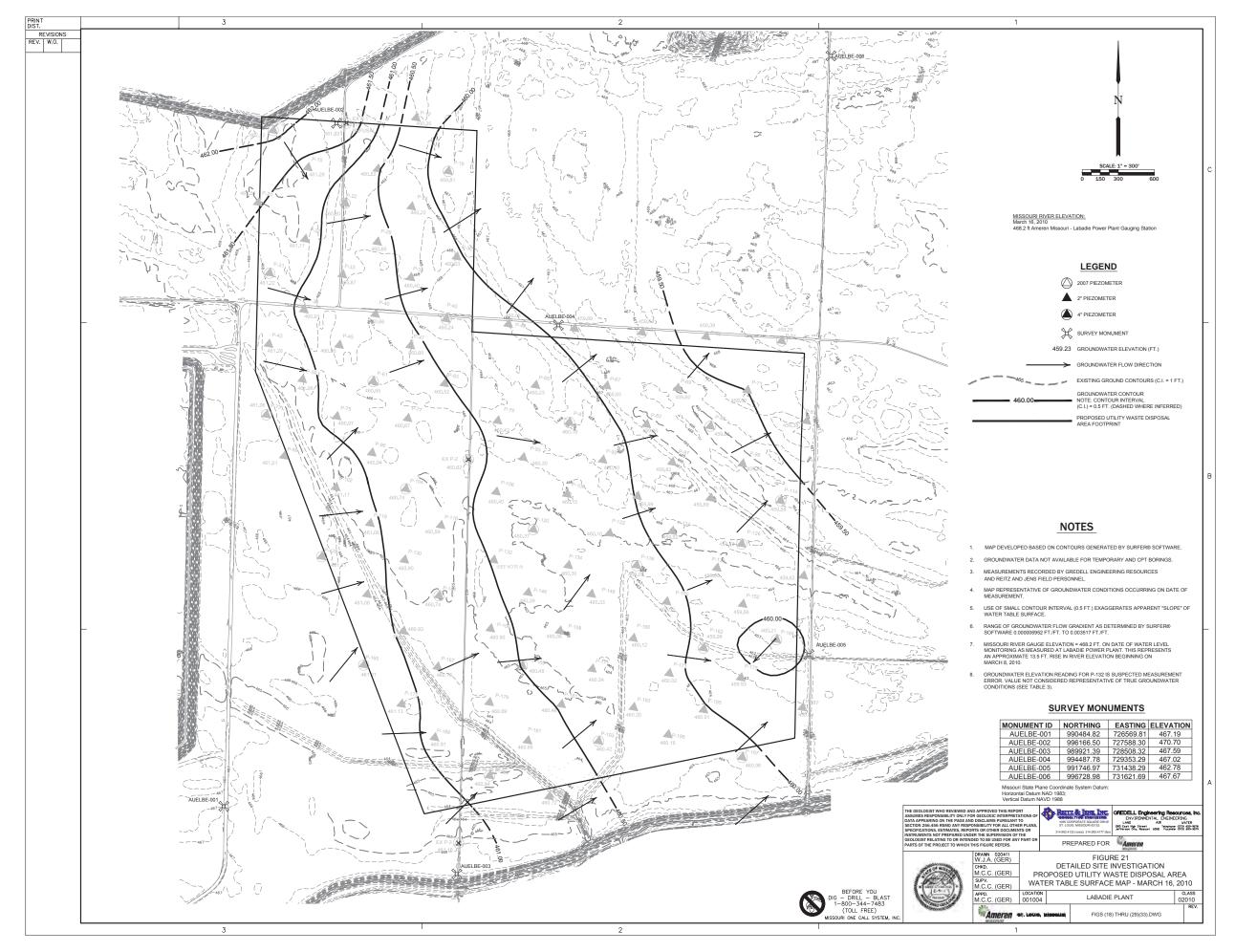
RECORD OF BOREHOLE BMW-2S SHEET 2 of 2 PROJECT: Ameren CCR GW Monitoring PROJECT NUMBER: 153-1406.0001B LOCATION: Labadie Energy Center DRILLING METHOD: 6" Sonic DRILLING DATE: 2/2/2016 DRILL RIG: Mini Sonic (CDD1415) DATUM: NAVD88 ELEVATION: 472.48
AZIMUTH: N/A INCLINATION: -90
COORDINATES: N: 987,210.08 E: 715,104.29 BORING METHOD SOIL/ROCK PROFILE SAMPLES DEPTH (feet) GRAPHIC LOG ELEVATION REMARKS DESCRIPTION NUMBER USCS TYPE DEPTH (ft) - 30 END OF BORING AT 30.0 FT BELOW GROUND SURFACE. FOR WELL DETAILS, SEE WELL CONSTRUCTION LOG BMW-2S. 30.0 - 35 - 40 - 45 GOLDER STL RECORD OF BOREHOLE MWD LEC LOGS.GPJ GLDR_CO.GDT 10/9/17 - 50 - 55 LOGGED: JSI/JS SCALE: 1 in = 3.8 ft DRILLING CONTRACTOR: Cascade CHECKED: JSI Golder DRILLER: J. Drabek REVIEWED: PJJ/MNH Associates

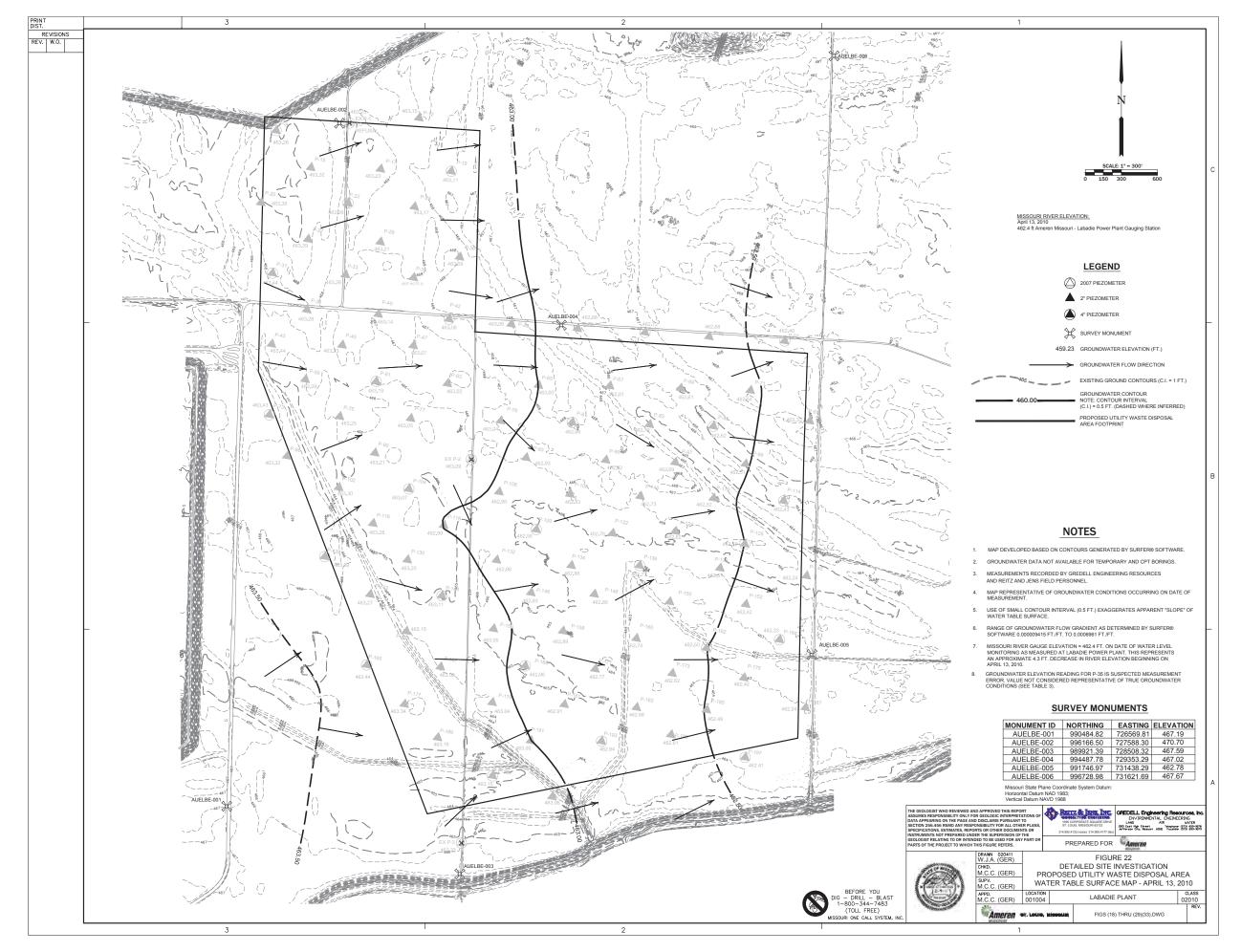
APPENDIX B HISTORIC POTENTIOMETRIC SURFACE MAPS

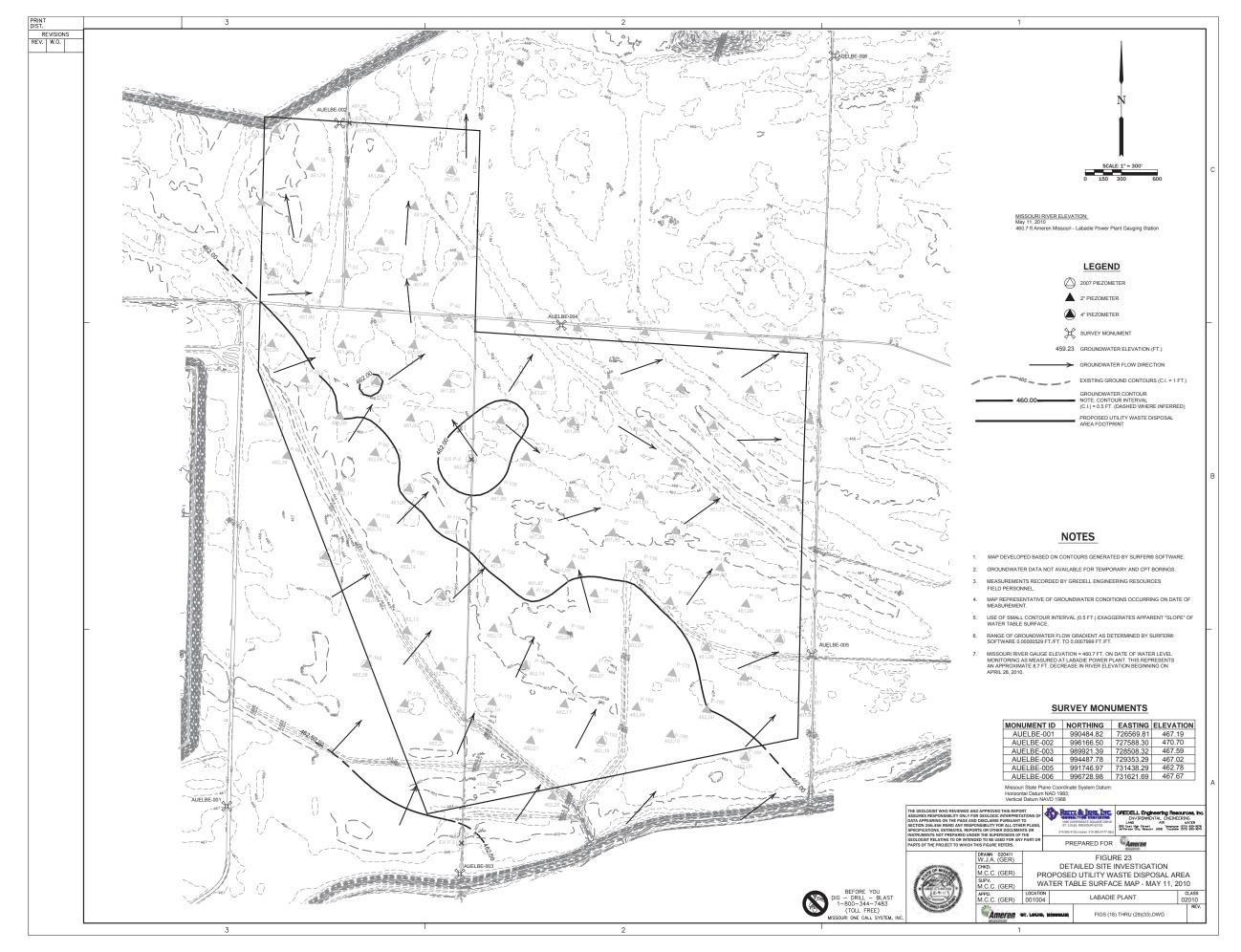


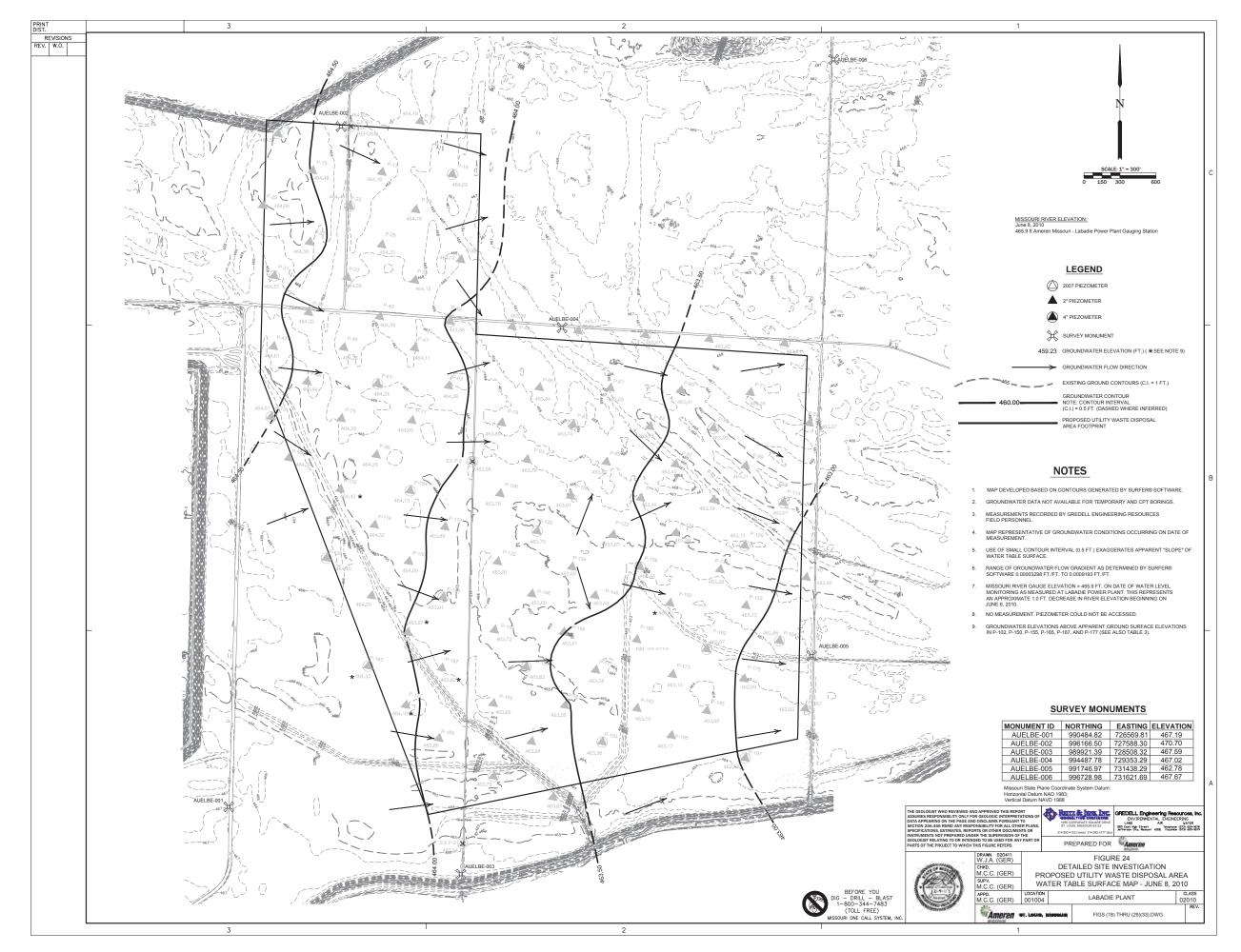


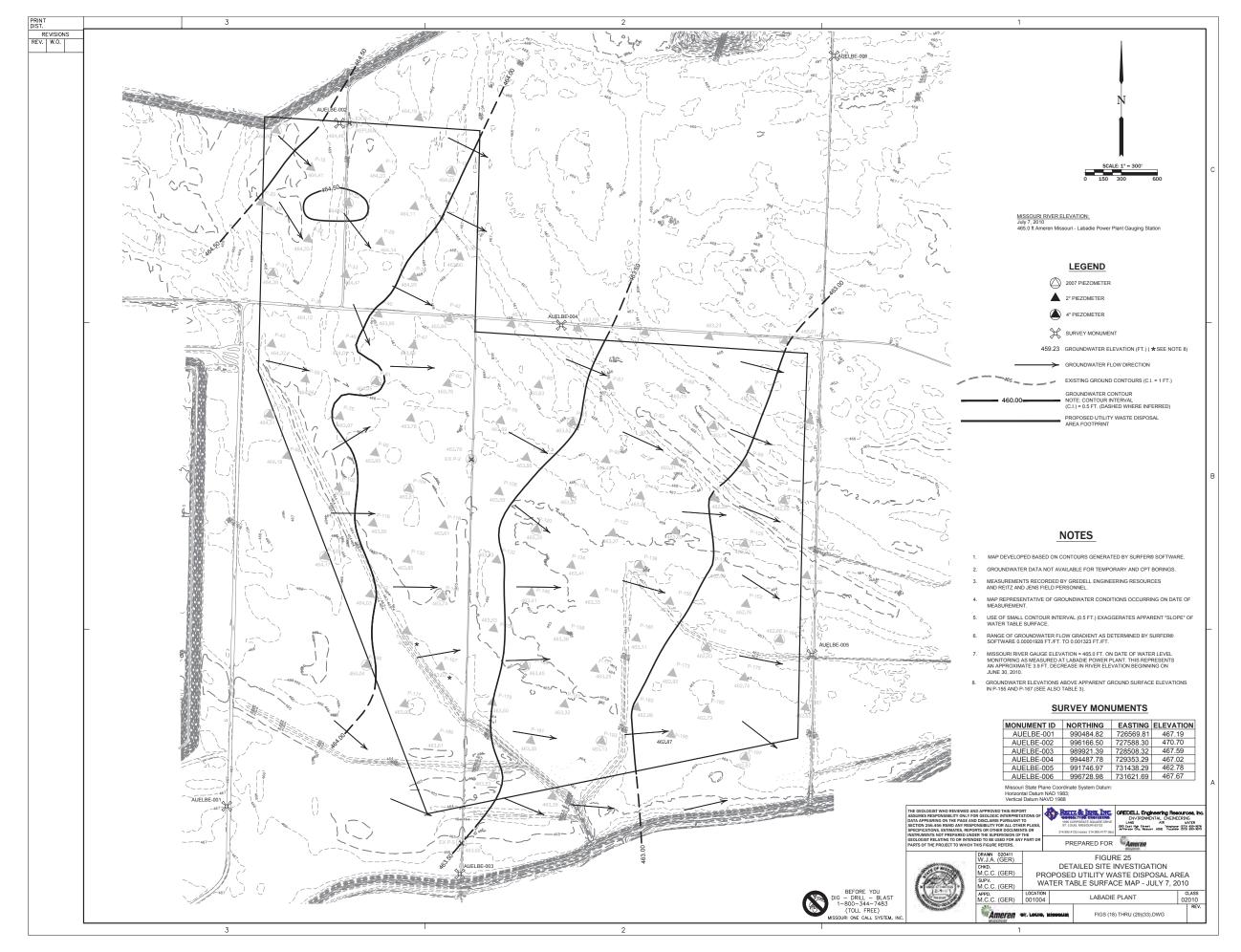


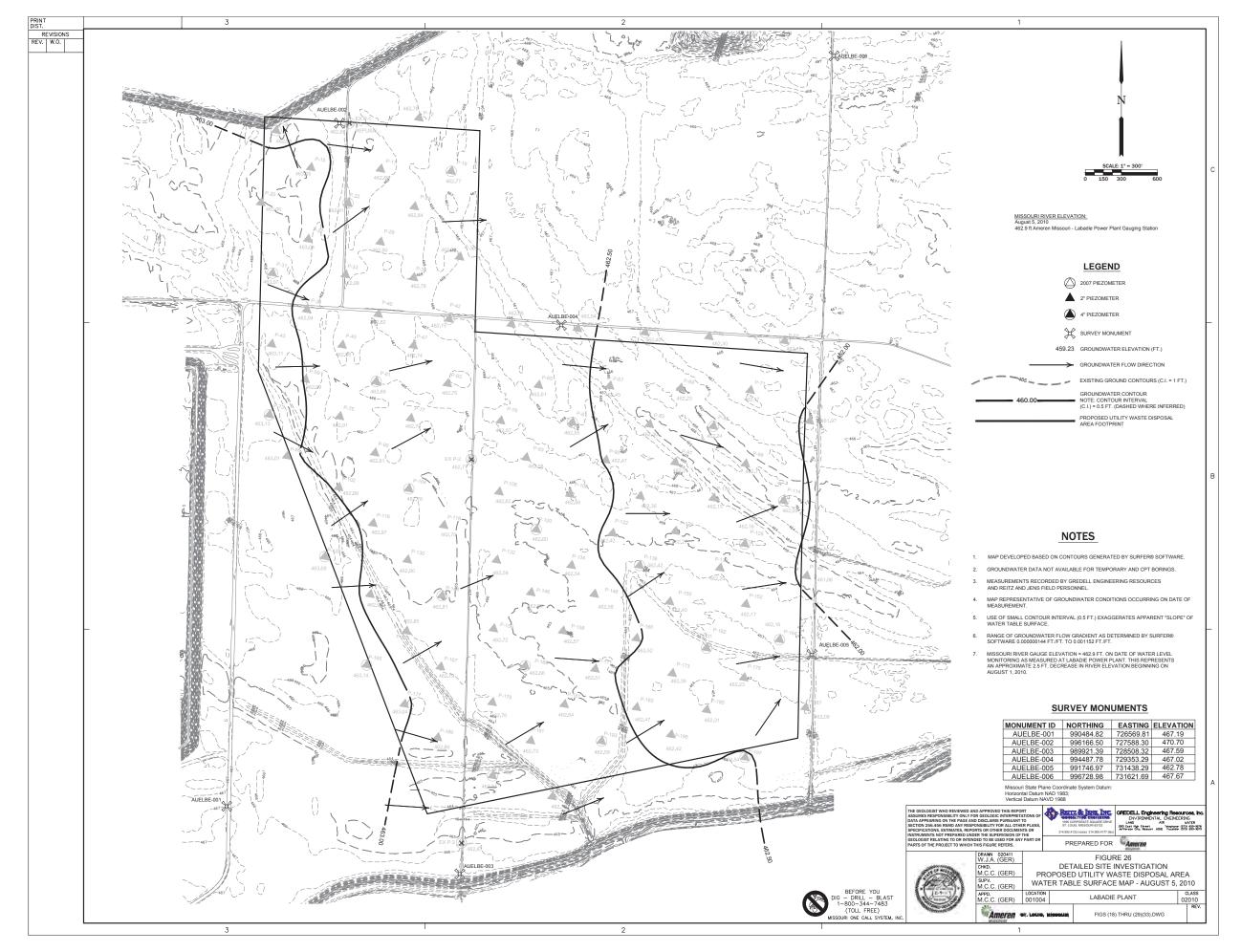


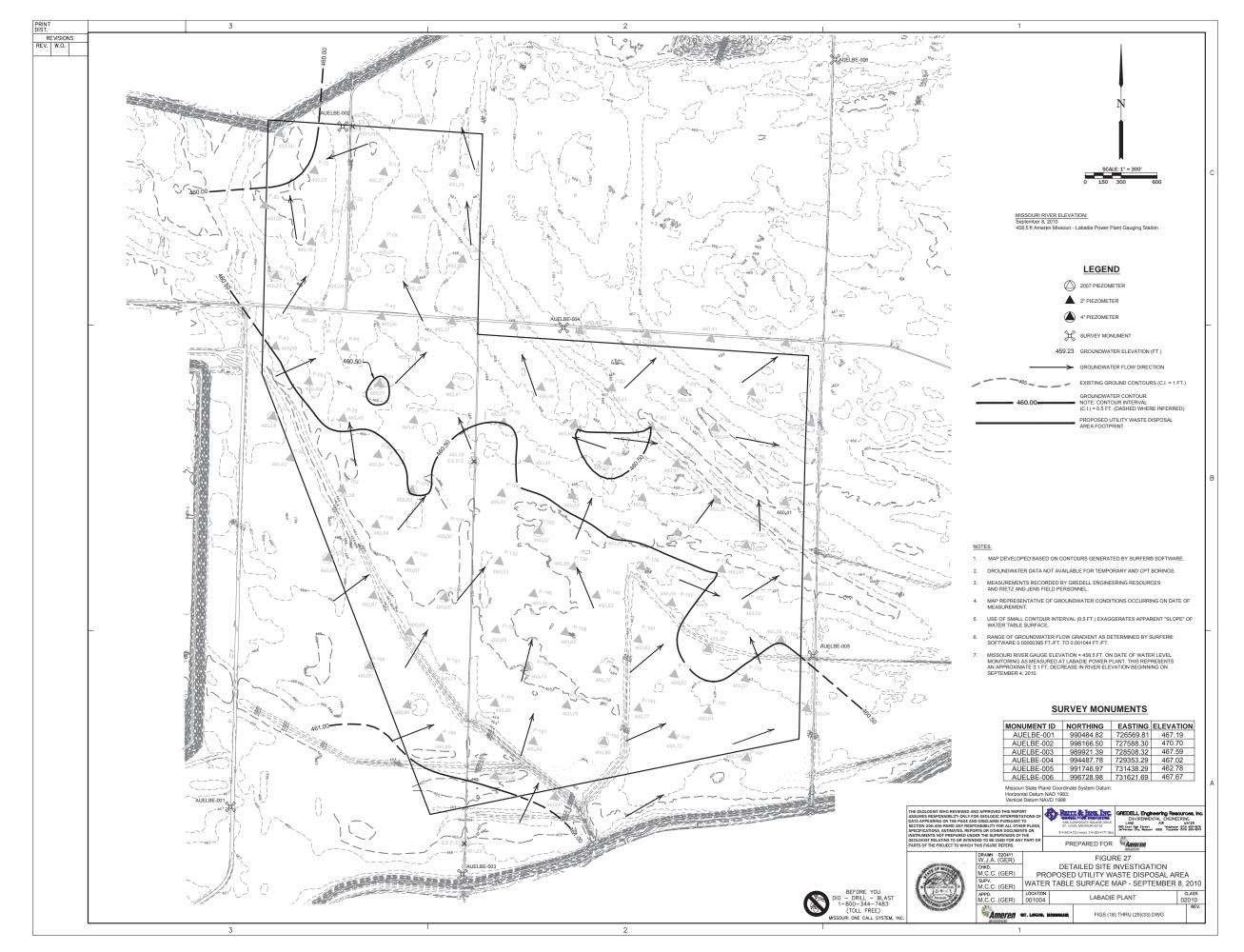


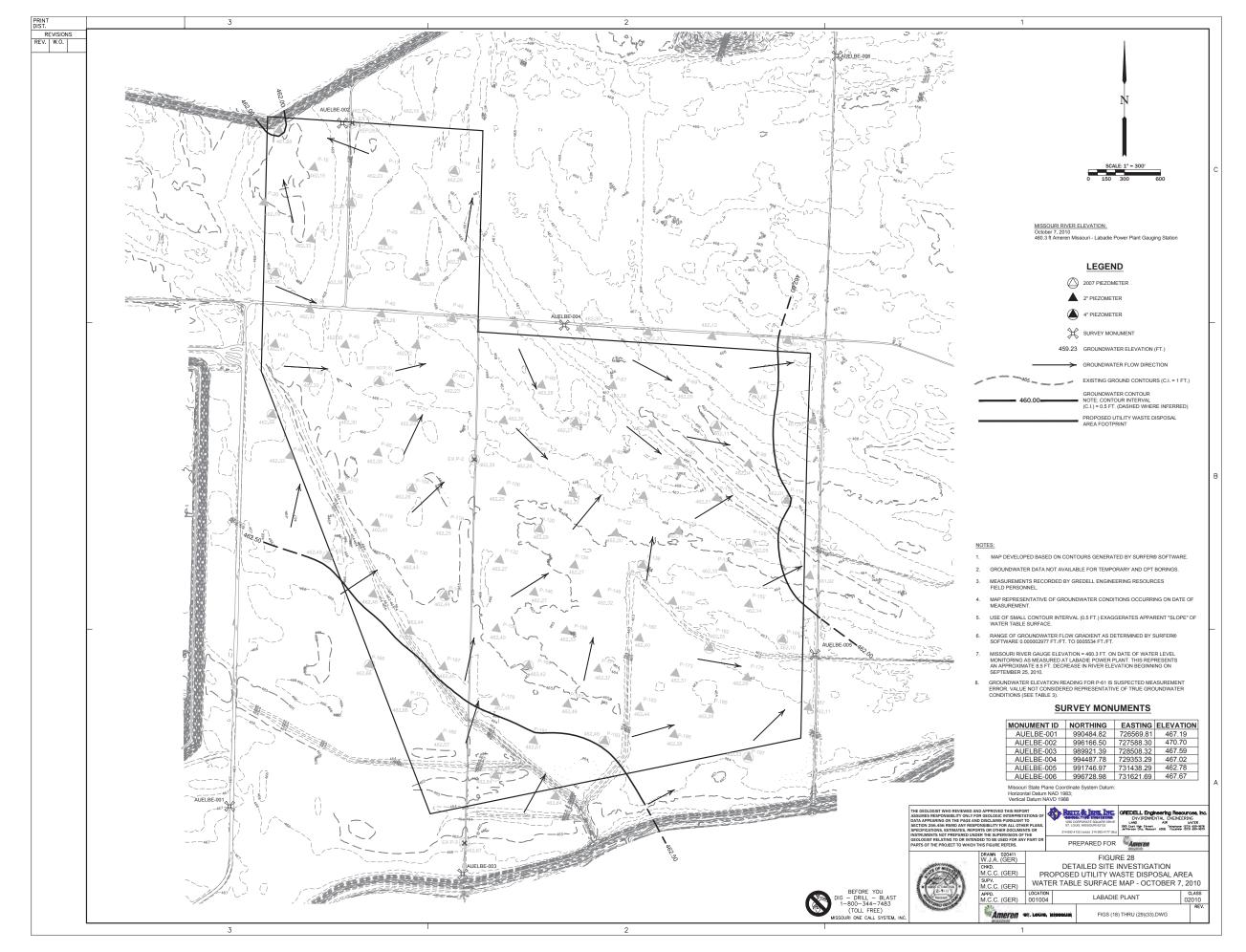


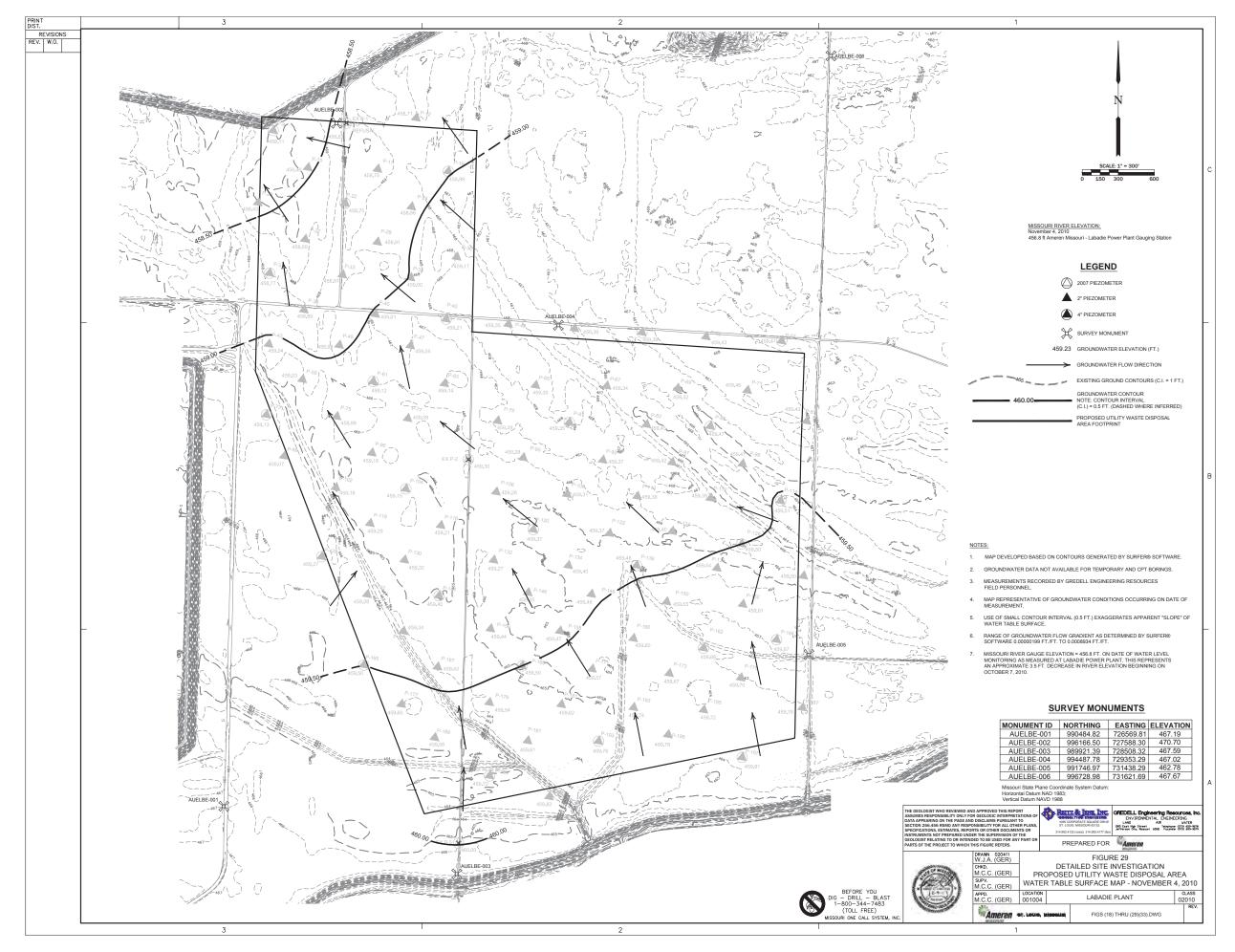


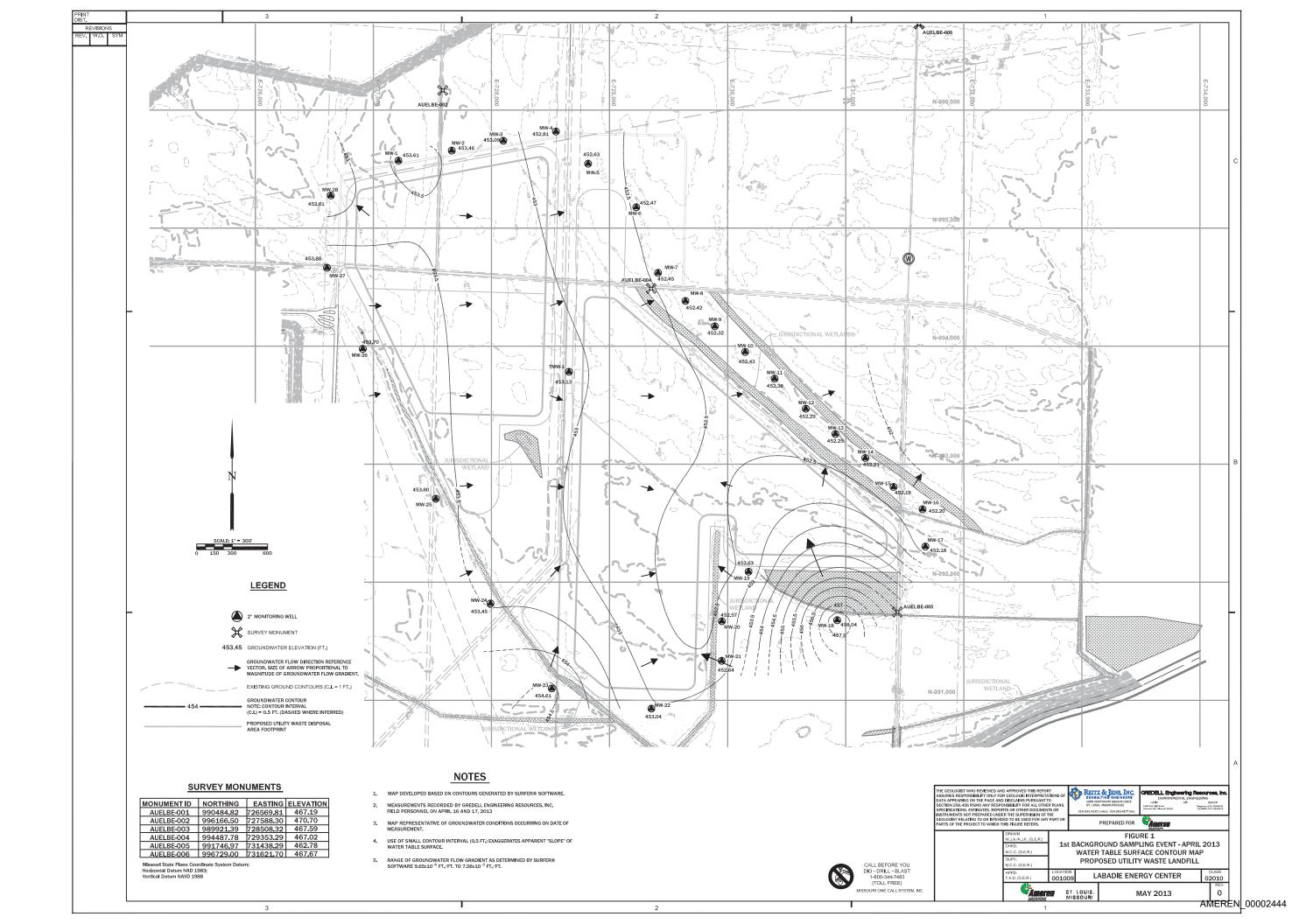


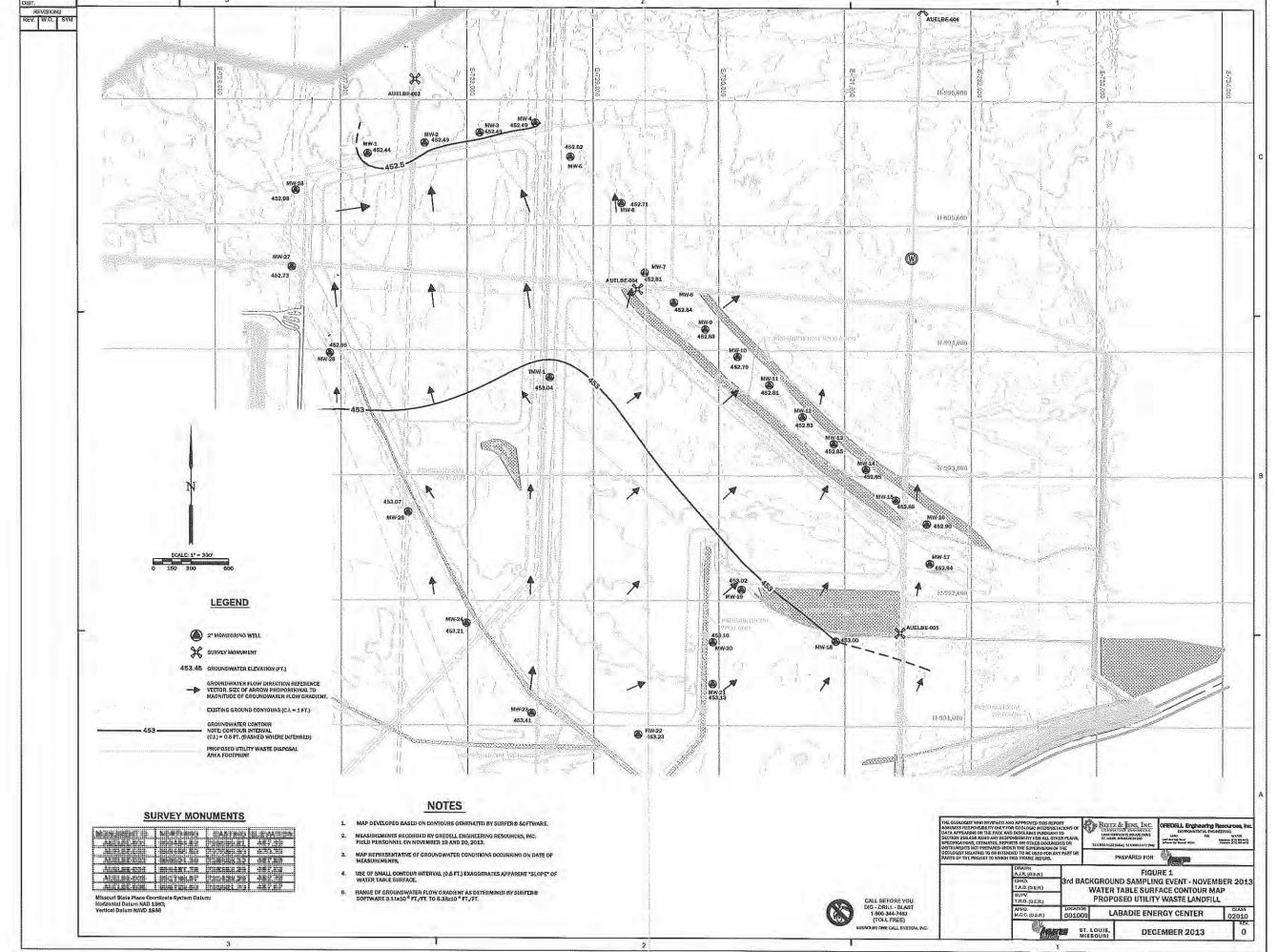


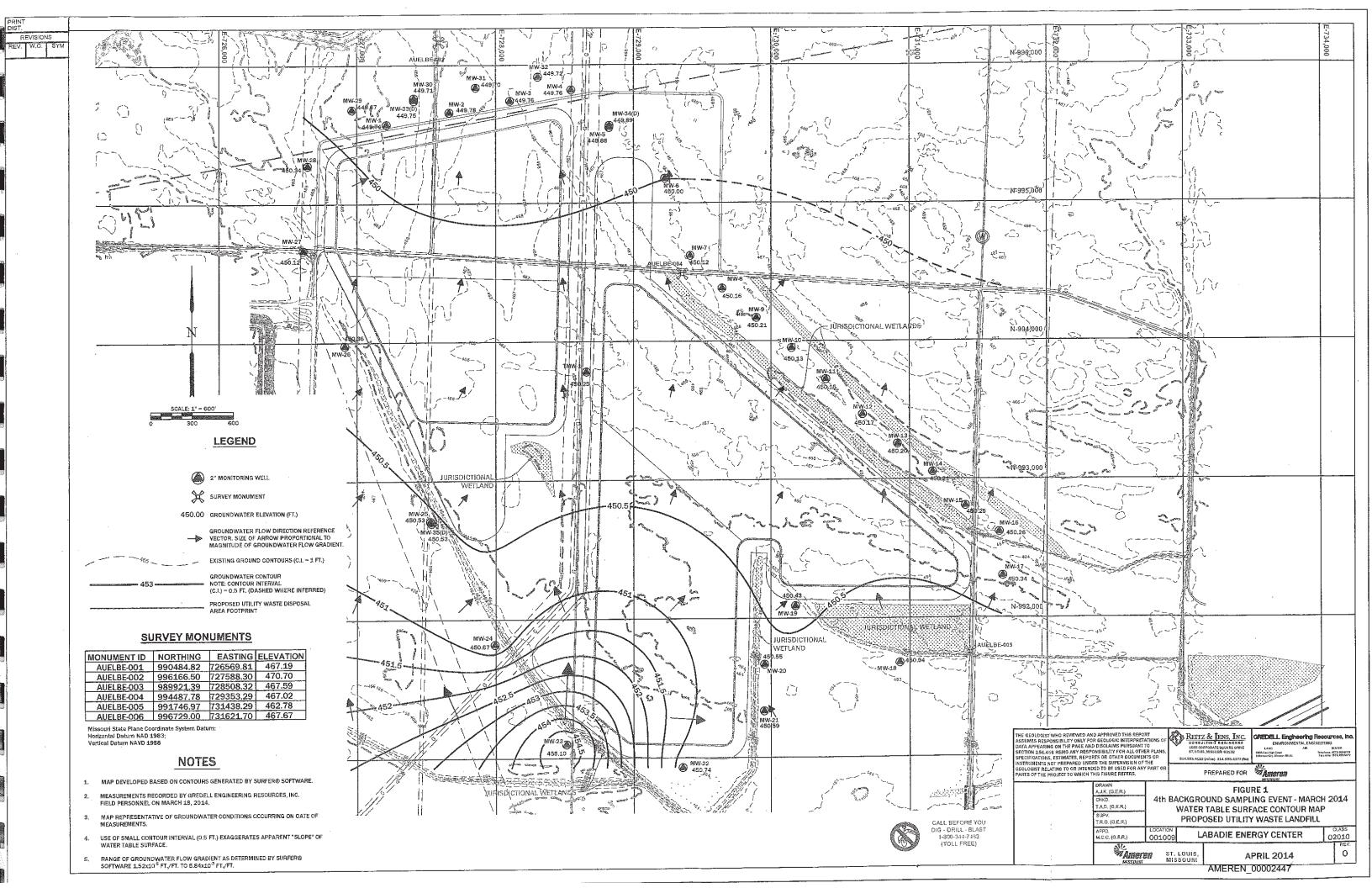




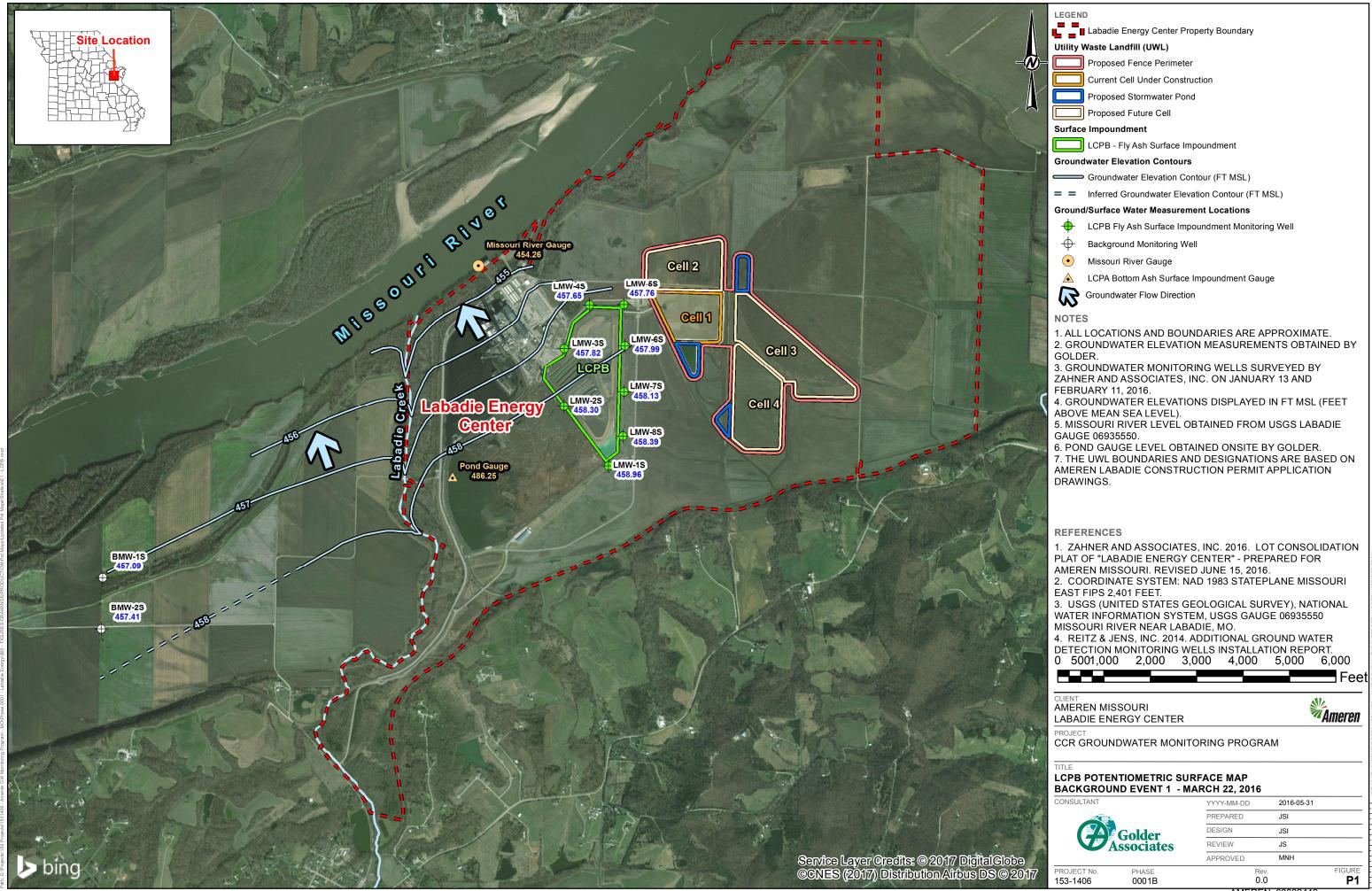


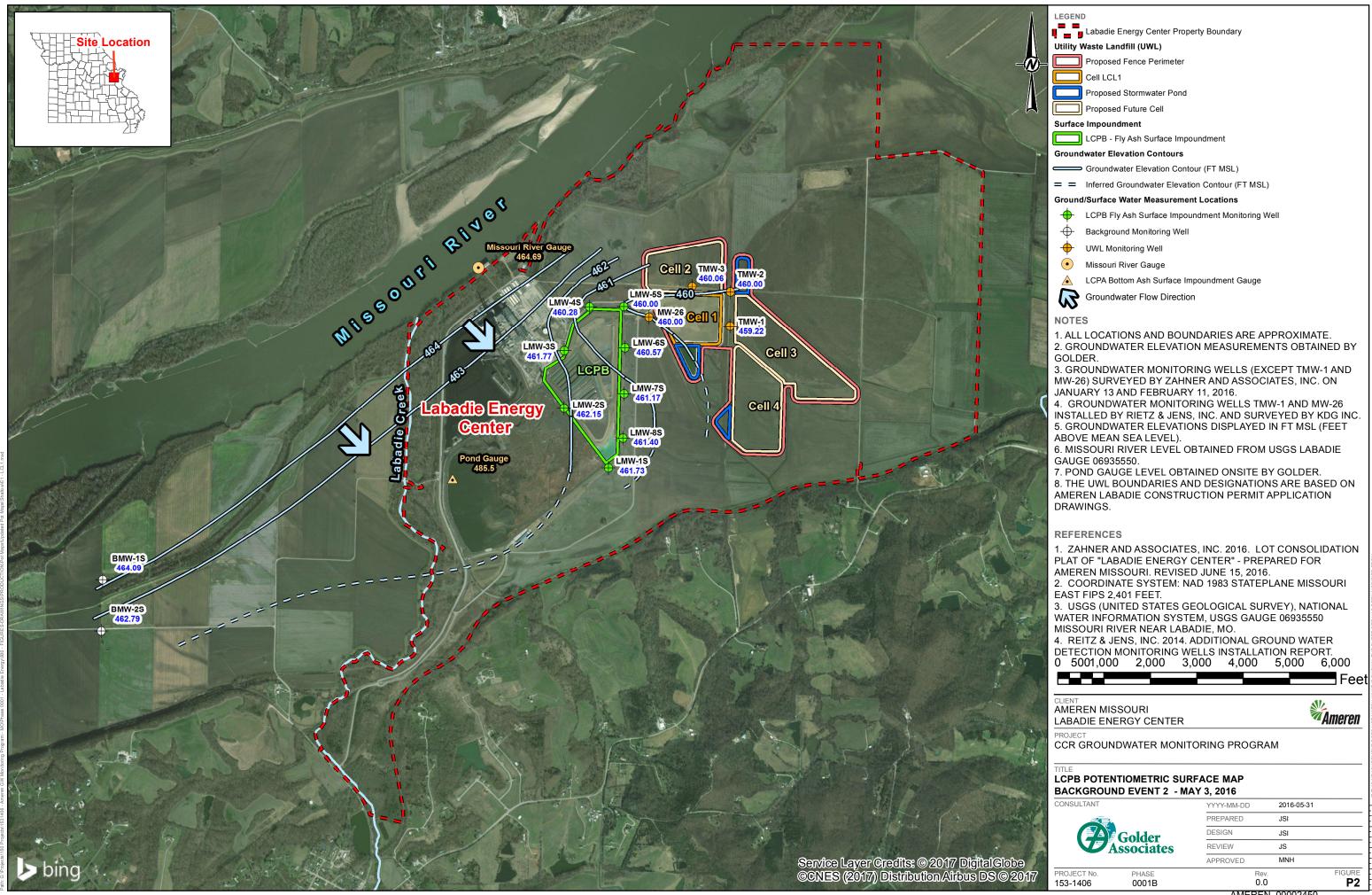




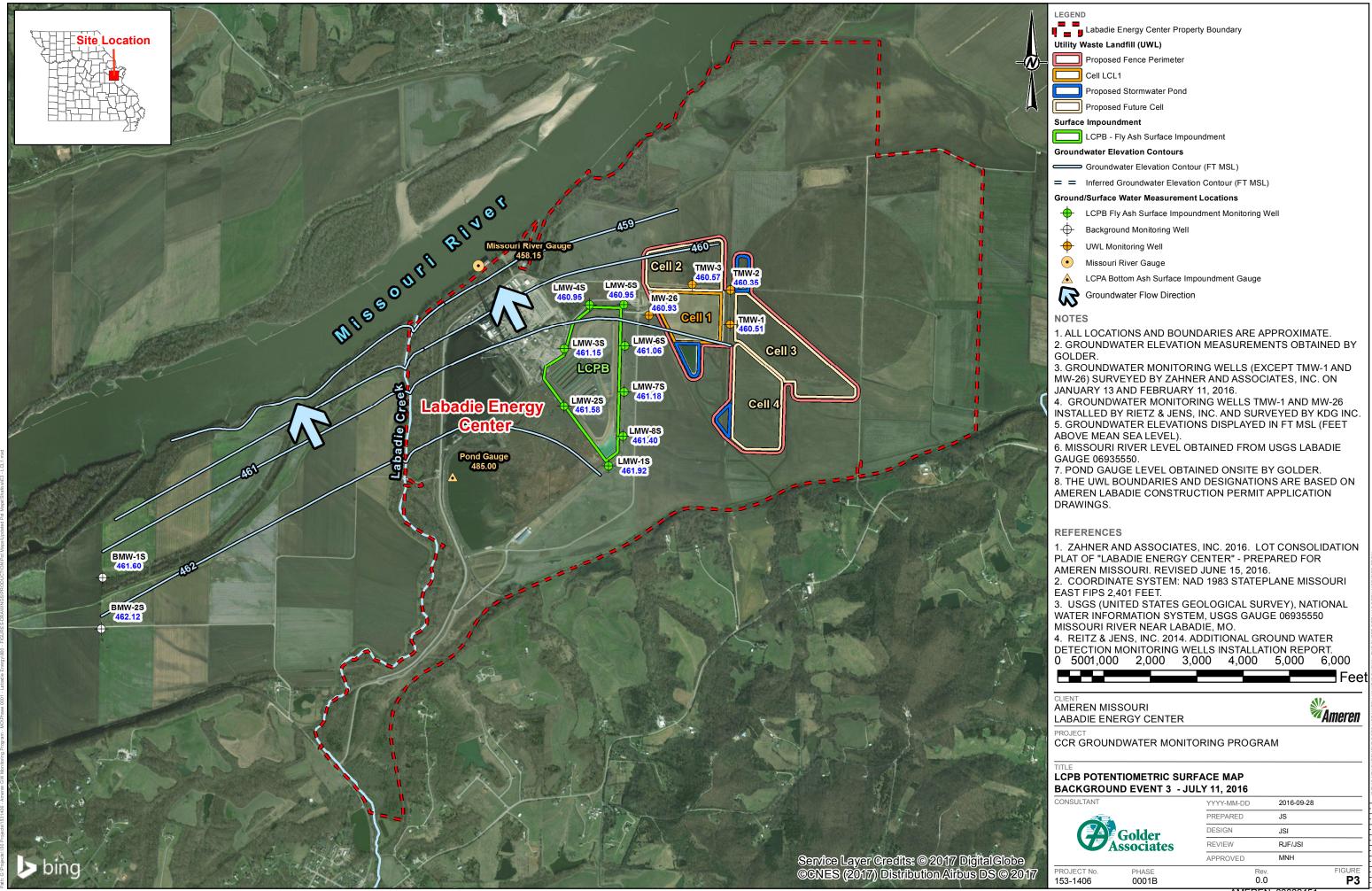


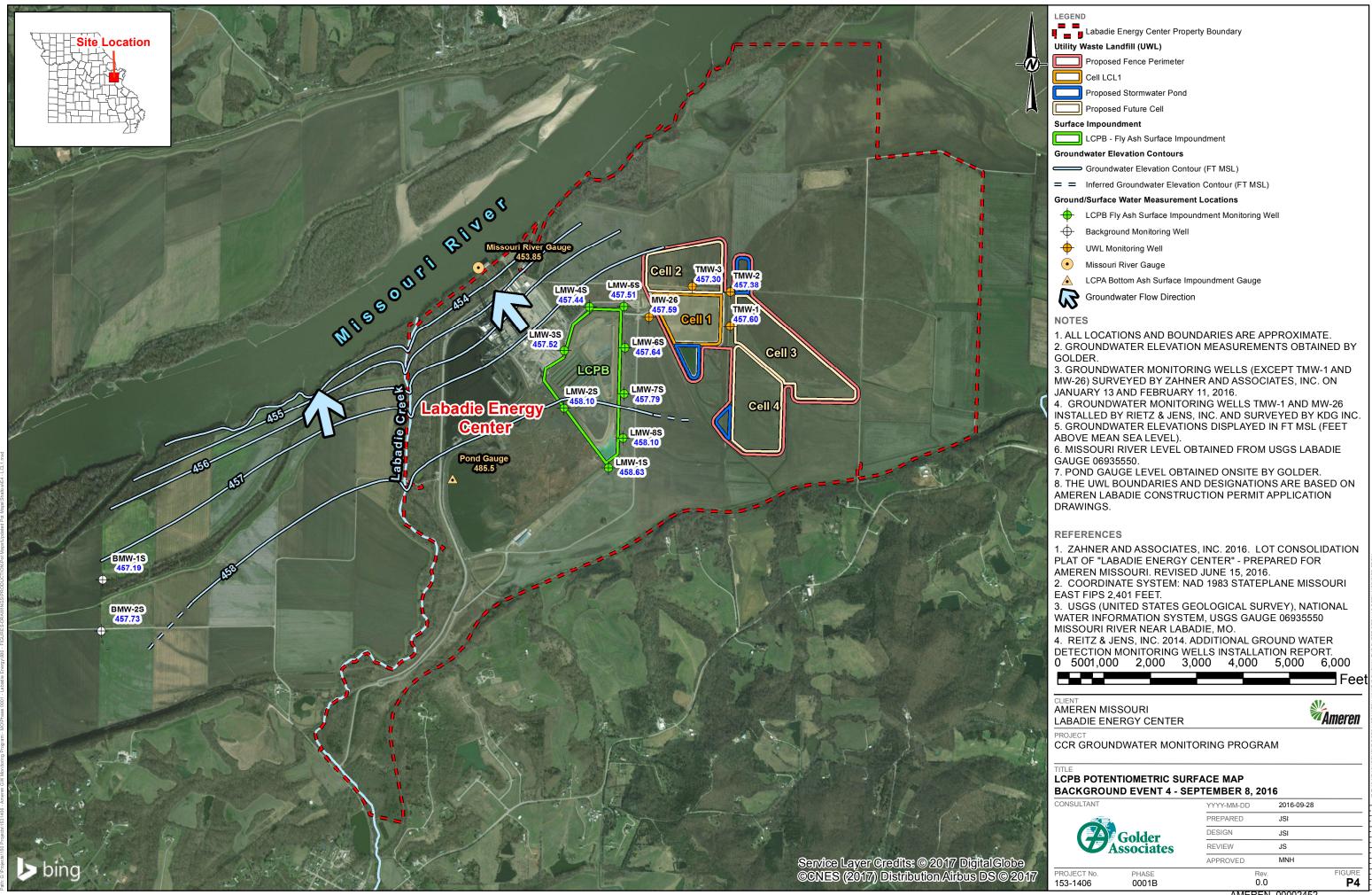
APPENDIX C POTENTIOMETRIC SURFACE MAPS FROM BACKGROUND CCR SAMPLING EVENTS

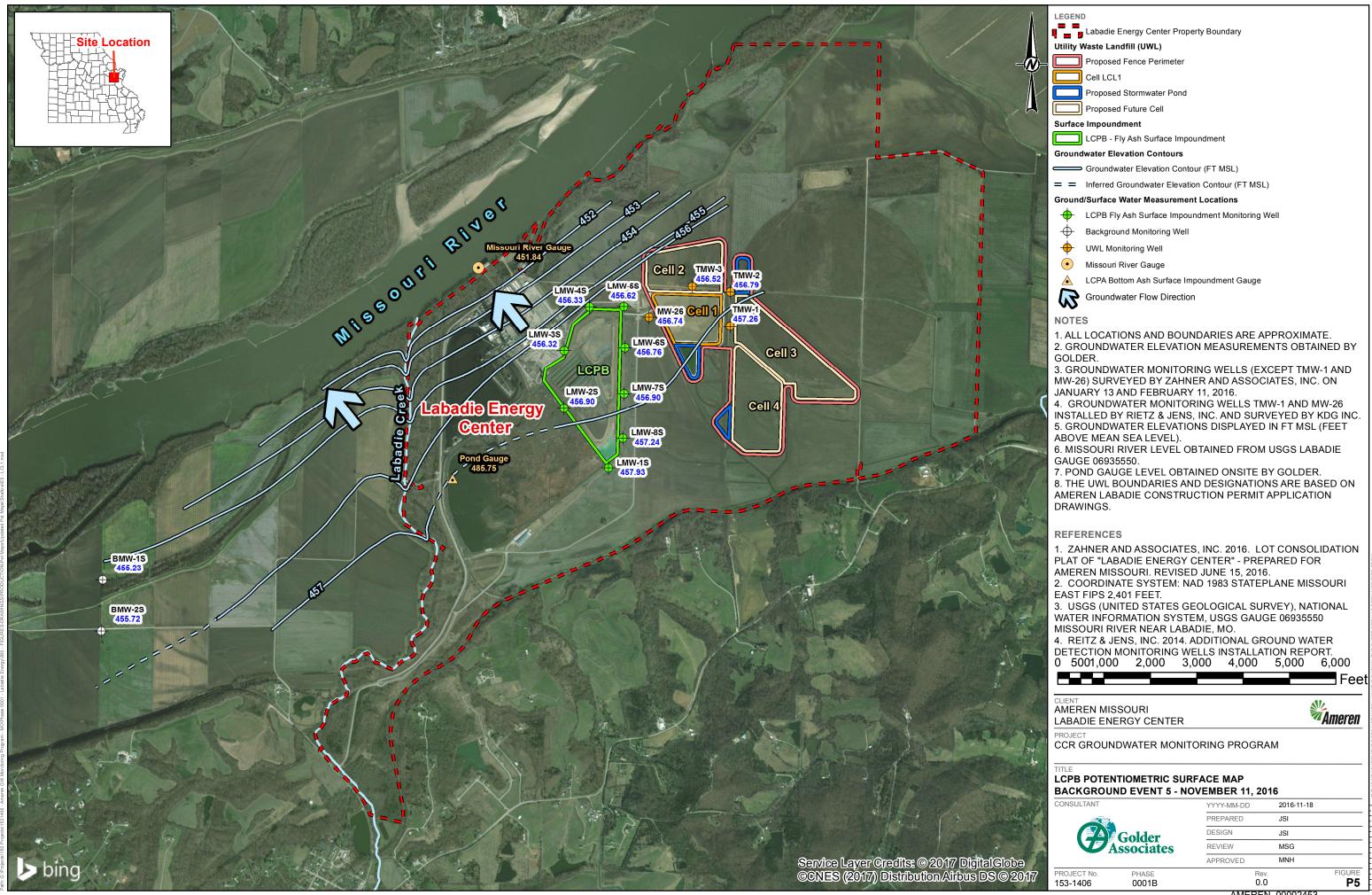


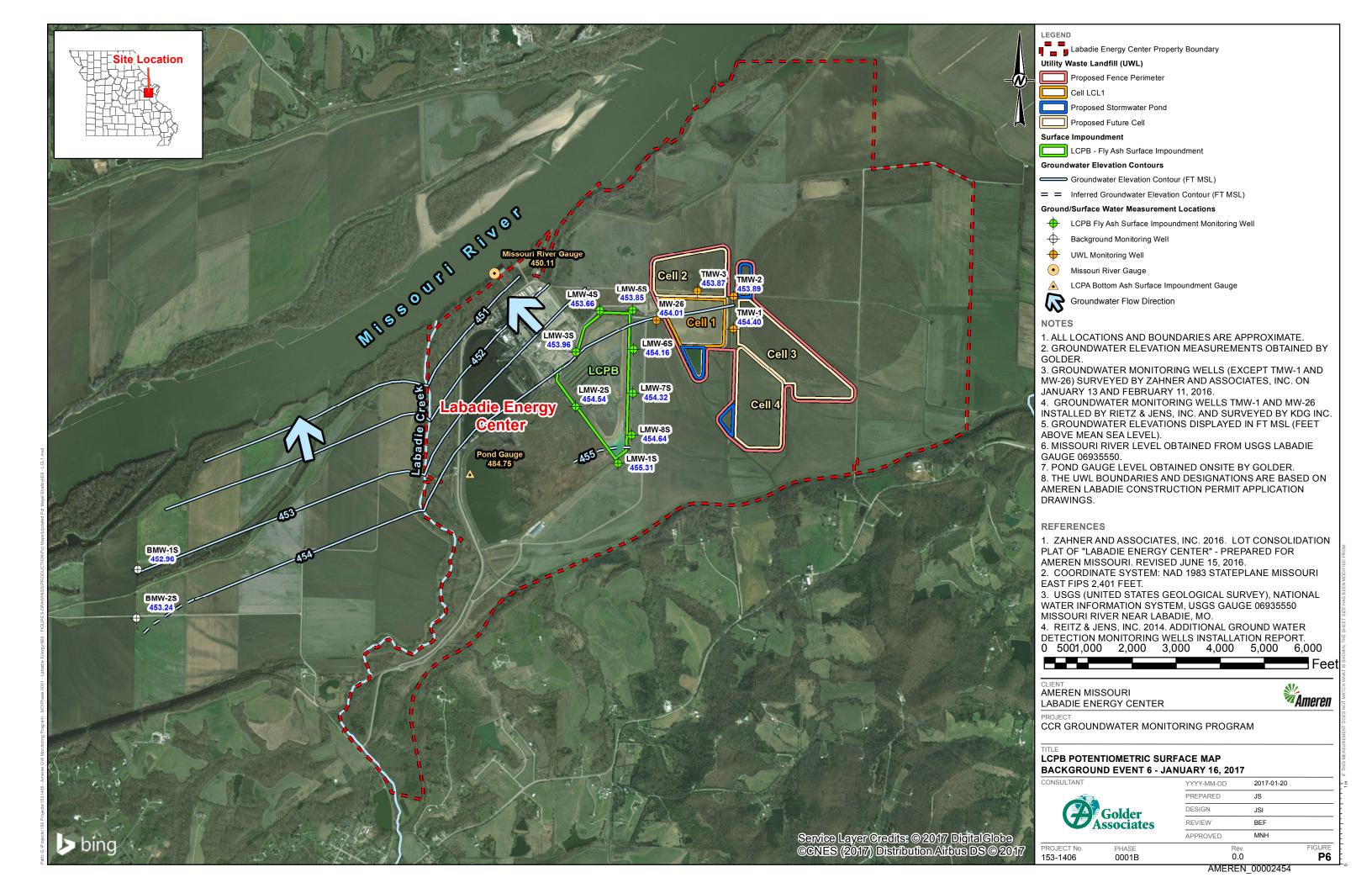


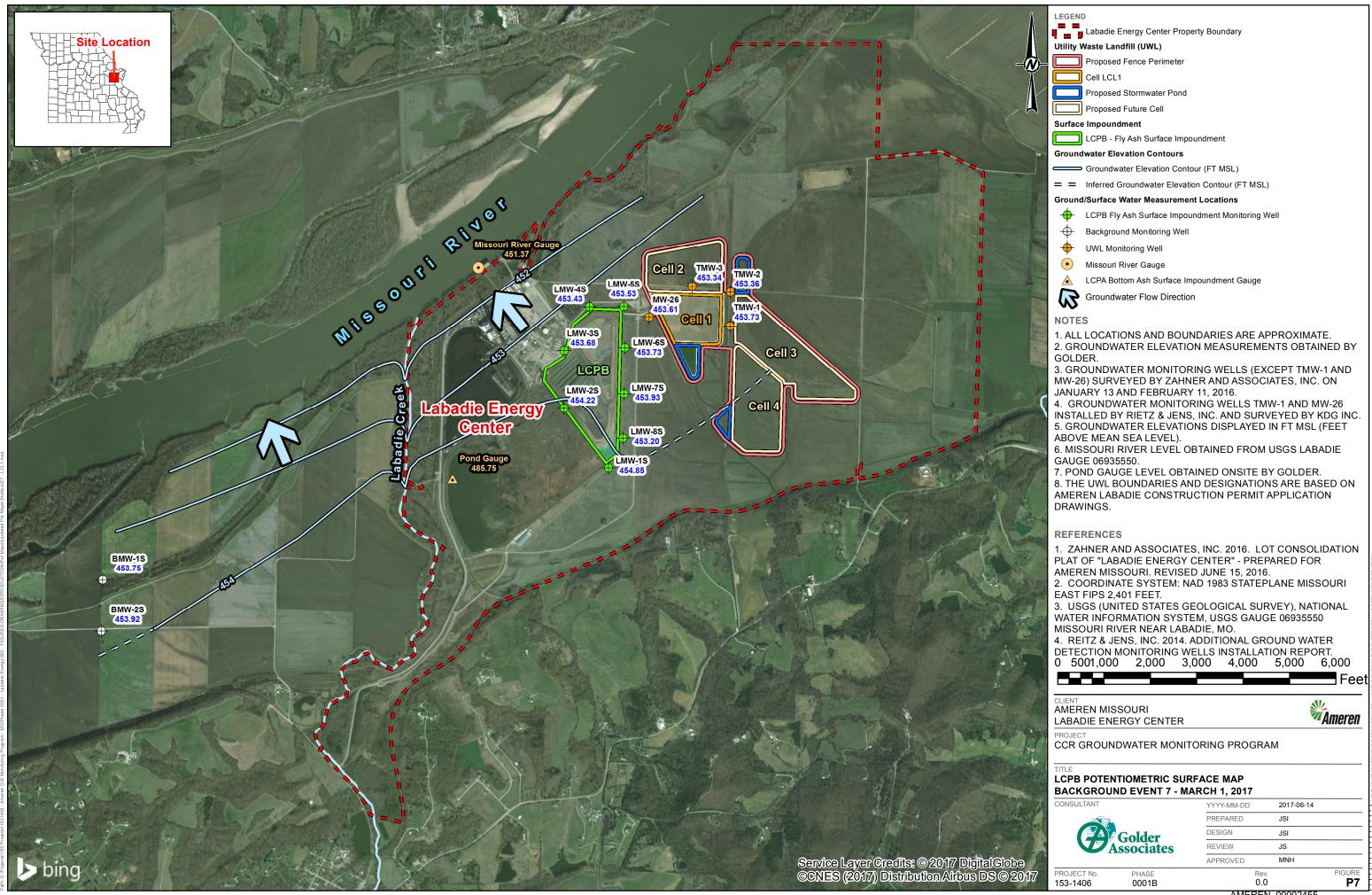
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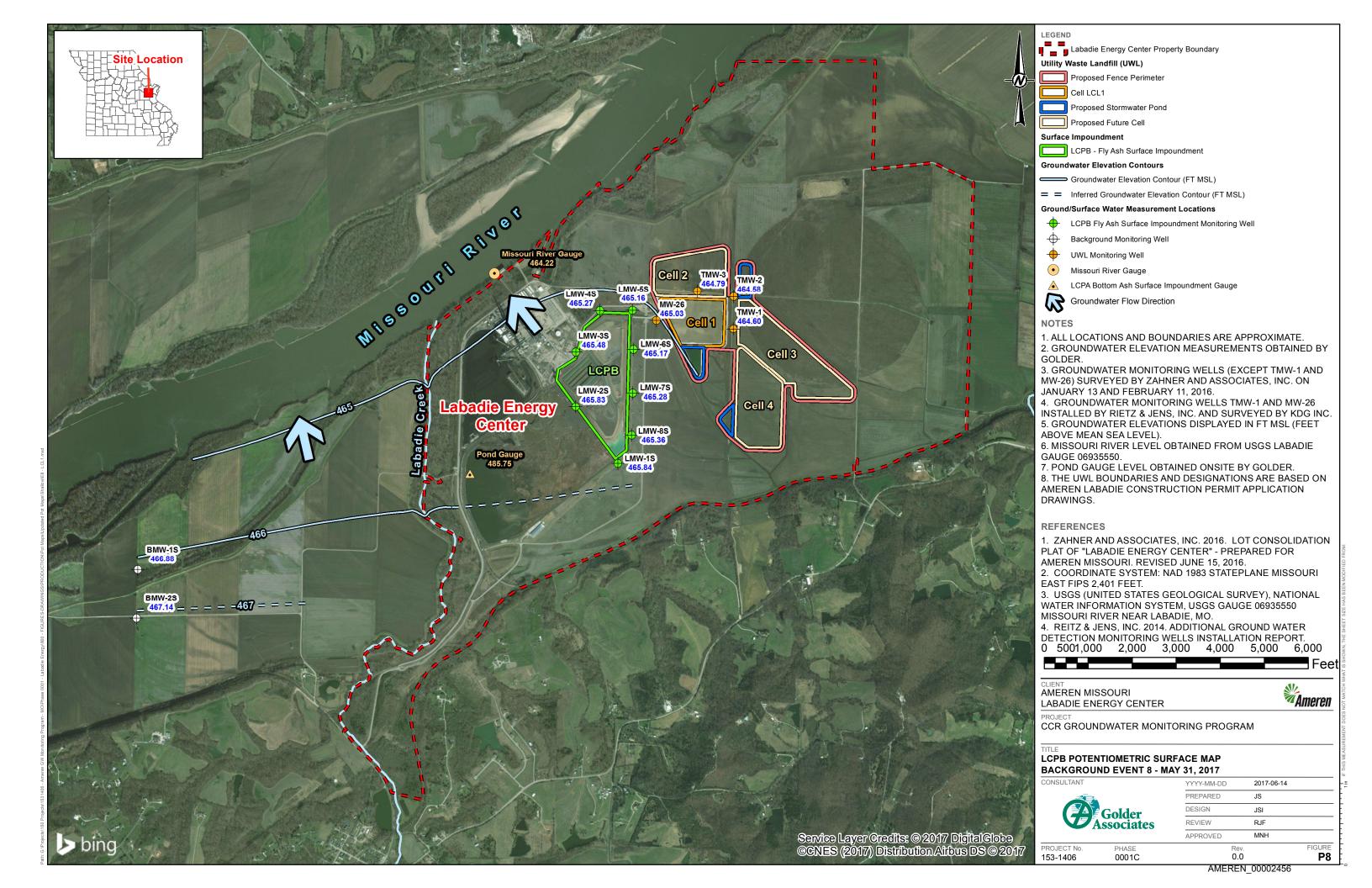








AMEREN 00002455

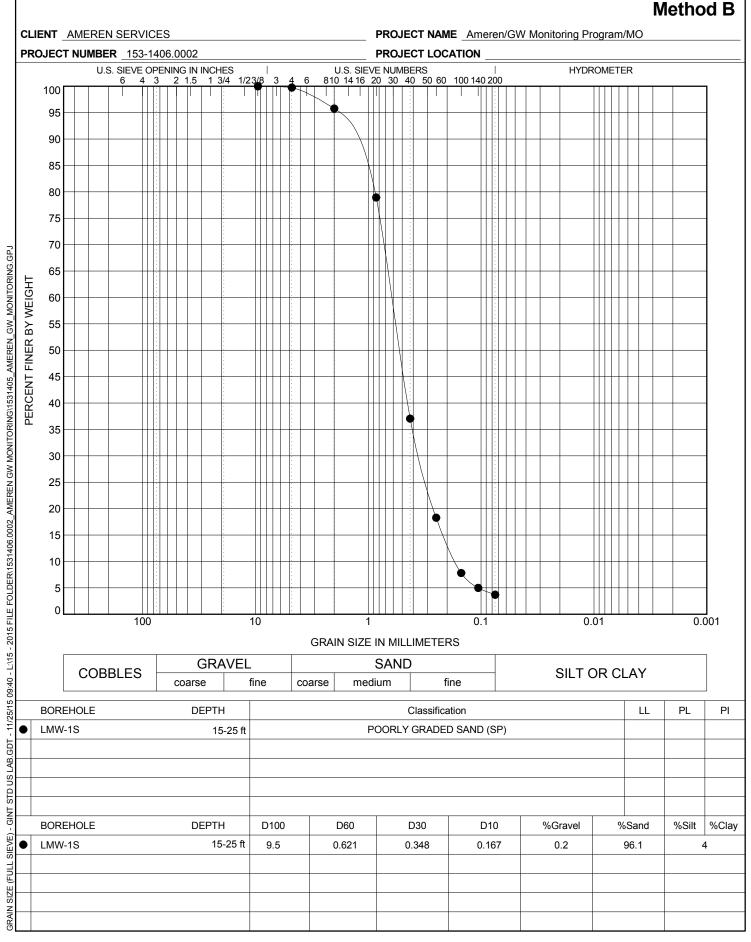


APPENDIX D GRAIN SIZE DISTRIBUTION



500 Century Plaza Drive, Suite 190 Houston, Texas 77073 **Golder** Telephone: (281) 821-6868 Fax: (281) 821-6870

GRAIN SIZE DISTRIBUTION ASTM D6913



APPENDIX E CCR MONITORING WELL CONSTRUCTION DIAGRAMS



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG LMW-1S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0001B SITE NAME: LABADIE ENERGY CENTER LOCATION: LMW-1S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 468.1 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 990727.7 EASTING: 726039.1 DRILLER: J. DRABEK STATIC WATER LEVEL: 9.50 FT BTOC COMPLETION DATE: 11/20/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK . - TOP OF CASING ELEVATION: 470.06 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: _____ 2.0 FT - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 468.1 FT MSL DIAMETER OF RISER PIPE (in.): _____ DIAMETER OF BOREHOLE (in.): ___ - CONCRETE SEAL DEPTH (ft. bgs): 2.5 — TYPE AND AMOUNT OF ANNULAR SEAL: _____ NONE TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 3 BAG - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 11.0 FINE: 10.0 - CENTRALIZER (yes (no) - TYPE: NONE TOP OF SCREEN DEPTH (ft. bgs): 13.6 TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: COARSE: 2.5 BAGS FINE: 1/3 BAG - BOTTOM OF SCREEN DEPTH (ft. bgs): 23.4 - BOTTOM OF WELL DEPTH (ft. bgs): 23.8 BOTTOM OF FILTER PACK (ft. bgs): 23.8
 TYPE AND AMOUNT OF BACKFILL: 1.2 FT - NATURAL CAVE IN TOTAL DEPTH OF BOREHOLE: 25.0 FT ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 30 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 16, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: J. INGRAM

DATE CHECKED: 4/19/2016



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG LMW-2S

PROJECT NAME: AMEREN CCR GW MONITORING PROJECT NUMBER: 153-1406.0001B SITE NAME: LABADIE ENERGY CENTER LOCATION: LMW-2S CLIENT: AMEREN MISSOURI SURFACE ELEVATION: 494.9 FT MSL GEOLOGIST: J. SUOZZI NORTHING: 992017.5 EASTING: 725074.2 DRILLER: J. DRABEK STATIC WATER LEVEL: 35.68 FT BTOC COMPLETION DATE: 11/23/2015 DRILLING COMPANY: CASCADE DRILLING METHODS: SONIC CAP LOCK - TOP OF CASING ELEVATION: 496.64 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM STICK UP: 1.7 FT - PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 494.9 FT MSL DIAMETER OF RISER PIPE (in.): _____ DIAMETER OF BOREHOLE (in.): ___ - CONCRETE SEAL DEPTH (ft. bgs): 2.5 - TYPE AND AMOUNT OF ANNULAR SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 4 BAG TYPE AND AMOUNT OF ANNULAR SEAL: HIGH SOLIDS BENTONITE 4 BAGS - TOP OF BENTONITE SEAL DEPTH (ft. bgs): 40.0 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ BENTONITE CHIPS - 1 BAG TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 46.5 FINE: 46.0 CENTRALIZER (yes) no) - TYPE: STAINLESS STEEL (TOP + BOTTOM) TOP OF SCREEN DEPTH (ft. bgs): 49.1 TYPE OF SCREEN: 2" X 4.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: COARSE: 2 BAGS FINE: 1/2 BAG BOTTOM OF SCREEN DEPTH (ft. bgs): 53.9 BOTTOM OF WELL DEPTH (ft. bgs): 54.3 - BOTTOM OF FILTER PACK (ft. bgs): ____ TOTAL DEPTH OF BOREHOLE: 55.0 FT TYPE AND AMOUNT OF BACKFILL: 0.7 FT - NATURAL CAVE IN ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL. 200 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000) MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON JANUARY 16, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY: __J. INGRAM DATE CHECKED: 4/19/2016

PREPARED BY MEREN JOSO POST ZI



	ABOVE GROUND
RING PROJECT NUMBER: 153-1406.0001B	ME: AMEREN CCR GW MONITO
LOCATION:LMW-3S	LABADIE ENERGY CENTER
SURFACE ELEVATION: 490.5 FT MSL	MEREN MISSOURI
NG: 993254.3 EASTING: 725081.6	J. INGRAM NORTHI
WATER LEVEL: 32.6 FT BTOC COMPLETION DATE: 2/2/2016	J. DRABEK STATIC
DRILLING METHODS: SONIC	MPANY: CASCADE
TOP OF CASING ELEVATION: 492.56 FT MSL PROTECTIVE CASING (yes) no): 4" X 5' ALUMINUM PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 490.5 FT MSL DIAMETER OF RISER PIPE (in.): 2.0 DIAMETER OF BOREHOLE (in.): 6.0 CONCRETE SEAL DEPTH (ft. bgs): 2.5 TYPE AND AMOUNT OF ANNULAR SEAL: 8 "BENTONITE CHIPS - 2 BAGS TYPE AND AMOUNT OF ANNULAR SEAL: HIGH SOLIDS BENTONITE	LOCK 2.1 FT A A A A A A A A A A A A A A A A A A A
TOP OF BENTONITE SEAL DEPTH (ft. bgs):	OF H2O USED DURING DRILLING. HORI TUM: NAVD88. WELL SURVEYED BY ZAH
SURFACE ELEVATION: 490.5 FT MSL NG: 993254.3	MEREN MISSOURI J. INGRAM J. DRABEK STATIC MPANY: CASCADE LOCK 2.1 FT OTES: FT BGS = FEET BELOW GROUND OF H20 USED DURING DRILLING. HORITUM: NAVD88. WELL SURVEYED BY ZAFTUM: TUM: NAVD88. WELL SURVEYED BY ZAFTUM: NAVD88. WELL

PREPARED BY MERENLOSOUS



Associates	ABOVE GI	ROUND MONITO	RING WELL CONST	RUCTION LOG <u>LMW-45</u>			
PROJECT NAME: AMER	REN CCR GW	MONITORING	PROJECT NUMBER:	: 153-1406.0001B			
SITE NAME: LABADIE E	ENERGY CEN	NTER	LOCATION:LMW-4S				
CLIENT: AMEREN MIS	SSOURI		SURFACE ELEVATION	ON: 470.7 FT MSL			
GEOLOGIST: J. INGRAN	Л	NORTHING: 99419	4.9	EASTING: 725624.1			
DRILLER: J. DRABEK		STATIC WATER LI	EVEL: 14.89 FT BTOC	COMPLETION DATE: 11/18/2015			
DRILLING COMPANY:	CASCADE		DRILLING METHODS	S: SONIC			
LOCK STICK UP: 2.2 FT			PROTECTIVE CASING (yes) PEA GRAVEL OR SAND DIAMETER OF RISER PIPE (in.) CONCRETE SEAL DEPTH (ft. b	472.88 FT MSL no): 4" X 5' ALUMINUM ON: 470.7 FT MSL): 2.0): 6.0 ogs): 2.5			
TOTAL DEPTH OF BOREHOLE: 33.0 FT			TYPE AND AMOUNT OF BENTO TOP OF SAND PACK DEPTH (F CENTRALIZER (yes (no)) - TY TOP OF SCREEN DEPTH (Ft. bg TYPE OF SCREEN: SCREEN SLOT SIZE (in.): AMOUNT OF SAND: BOTTOM OF SCREEN DEPTH (Ft. bg TYPE OF SCREEN DEPTH (Ft. bg TYPE OF SCREEN DEPTH (Ft. bg TYPE OF SCREEN DEPTH (Ft. bg TYPE OF SCREEN DEPTH (Ft. bg TYPE OF SAND PACK: BOTTOM OF WELL DEPTH (Ft. bg TYPE AND OF FILTER PACK (Ft. bg TYPE AND OF FILTER PACK (Ft. bg TYPE AND OF FILTER PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND AMOUNT OF SAND PACK (Ft. bg TYPE AND TYPE AND TYPE AMOUNT OF SAND PACK (Ft. bg TYPE AND TYPE AND TYPE AMOUNT OF SAND PACK (Ft. bg TYPE AND TYPE AMOUNT OF SAND PACK (Ft. bg TYPE AND TYPE AMOUNT OF SAND PACK (Ft. bg TYPE AND TYPE AMOUNT OF SAND PACK (Ft. bg TYPE AND TYPE AMOUNT OF SAND PACK (Ft. bg TYPE AND TYPE AMOUNT OF SAND PACK (Ft. bg TYPE AND TYPE AMOUNT OF SAND PACK (Ft. bg TYPE AND TYPE AMOUNT OF SAND PACK (Ft. bg TYPE AND TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PACK (FT. bg TYPE AMOUNT OF SAND PAC	gs):			
ADDITIONAL NOTES: FT BG 150 GALLONS OF H2O USE VERTICAL DATUM: NAVD88	D DURING DRIL 3. WELL SURVEY	W GROUND SURFACE. LING. HORIZONTAL DA' /ED BY ZAHNER AND A	FT MSL = FEET ABOVE MEA	N SEA LEVEL. NATES NAD83 (2000) MISSOURI EAST ZONE. LY 16, 2016.			

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Associates ABOVE G	ROUND MONITORI	NG WELL CONSTI	RUCTION LOG <u>LMW-5S</u>			
PROJECT NAME: AMEREN CCR GV	/ MONITORING	PROJECT NUMBER: 153-1406.0001B				
SITE NAME: LABADIE ENERGY CE	NTER	LOCATION:LMW-5S				
CLIENT: AMEREN MISSOURI		SURFACE ELEVATION	N: 466.9 FT MSL			
GEOLOGIST: J. INGRAM	NORTHING: 994201.6	· · · · · · · · · · · · · · · · · · ·				
DRILLER: J. DRABEK	STATIC WATER LEVI	EL: 10.38 FT BTOC	COMPLETION DATE: 11/18/2015			
DRILLING COMPANY: CASCADE		DRILLING METHODS	S: SONIC			
STICK UP: 1.9 FT	PF PE/ GRC DIAN DIAN CON	P OF CASING ELEVATION: ROTECTIVE CASING (yes) A GRAVEL OR SAND DUND SURFACE ELEVATIO METER OF RISER PIPE (in.) METER OF BOREHOLE (in.) MICRETE SEAL DEPTH (ft. bg	468.75 FT MSL no): 4" X 5' ALUMINUM N: 466.9 FT MSL : 2.0 : 6.0 gs): 2.5			
	TYP TOP TOP TYP SCR SIZE	E AND AMOUNT OF BENTO OF SAND PACK DEPTH (ft ITRALIZER (yes no) - TY OF SCREEN DEPTH (ft. bg E OF SCREEN: EEEN SLOT SIZE (in.):	s): 11.9 2" X 9.8' SCHEDULE 40 PVC 0.010 IN COARSE: #1 FINE: #0 COARSE: 4 BAGS FINE: 1/3 BAG			
TOTAL DEPTH OF BOREHOLE: 25.0 FT ADDITIONAL NOTES: FT BGS = FEET BELO 75 GALLONS OF H2O USED DURING DRILL VERTICAL DATUM: NAVD88. WELL SURVE FT BTOC = FEET BELOW TOP OF CASING	BOT TYP OW GROUND SURFACE. FT ING. HORIZONTAL DATUM: YED BY ZAHNER AND ASSO	MSL = FEET ABOVE MEAN STATE PLANE COORDINA OCIATES, INC ON JANUARY	ogs): 22.1 FILL: 2.9 FT - NATURAL CAVE IN N SEA LEVEL. TES NAD83 (2000) MISSOURI EAST ZONE.			



Associates	ABOVE GROU	JND MONITOR	ING WELL CONSTR	RUCTION LOG <u>LMW-6S</u>			
PROJECT NAME: AM	IEREN CCR GW MC	NITORING	PROJECT NUMBER: 153-1406.0001B				
SITE NAME: LABADI	E ENERGY CENTE	R	LOCATION:LMW-6S				
CLIENT: AMEREN I	MISSOURI		SURFACE ELEVATION: 467.2 FT MSL				
GEOLOGIST: J. SUO	ZZI NO	RTHING: 993320.	2	EASTING: 726391.4			
DRILLER: J. DRAB	EK ST.	ATIC WATER LEV	'EL: 10.49 FT BTOR	COMPLETION DATE: 11/20/2015			
DRILLING COMPANY	: CASCADE		DRILLING METHODS	: SONIC			
STICK UP: 2.4 FT	CAF	DIA DIA	POF CASING ELEVATION: _ PROTECTIVE CASING (yes) r A GRAVEL OR SAND OUND SURFACE ELEVATION METER OF RISER PIPE (in.): METER OF BOREHOLE (in.): NCRETE SEAL DEPTH (ft. bg	469.56 FT MSL no): 4" X 5' ALUMINUM N: _467.2 FT MSL 2.0 6.0 s):			
			PE AND AMOUNT OF BENTO P OF SAND PACK DEPTH (ft. NTRALIZER (yes (no)) - TYI P OF SCREEN DEPTH (ft. bgs	2" X 9.8' SCHEDULE 40 PVC			
			REEN SLOT SIZE (in.):				
				COARSE: #1 FINE: #0 OARSE: 3 BAGS FINE: 1/3 BAG			
			TTOM OF SCREEN DEPTH (f				
TOTAL DEPTH 25.0 FT			TTOM OF WELL DEPTH (ft. b	gs):			
OF BOREHOLE: 25.0 F		TYF	PE AND AMOUNT OF BACKF	ILL: 2.2 FT - NATURAL CAVE IN			
30 GALLONS OF H2O US VERTICAL DATUM: NAV	SED DURING DRILLING. D88. WELL SURVEYED I	HORIZONTAL DATUM BY ZAHNER AND ASS	T MSL = FEET ABOVE MEAN 1: STATE PLANE COORDINA OCIATES, INC ON JANUARY AGS WEIGH 50 LBS EACH.	TES NAD83 (2000) MISSOURI EAST ZONE.			

PREPARED BY MEREN JOSO 1990 PAREN JOSO 1990 PREPARED BY MEREN BY MEREN



Associates	ROUND MONITOR	ING WELL CONSTR	RUCTION LOG <u>LMW-75</u>			
PROJECT NAME: AMEREN CCR G	W MONITORING	PROJECT NUMBER: 153-1406.0001B				
SITE NAME: LABADIE ENERGY CI	ENTER	LOCATION:LMW-7S				
CLIENT: AMEREN MISSOURI		SURFACE ELEVATION	N: 466.7 FT MSL			
GEOLOGIST: J. SUOZZI	NORTHING: 992330.	1	EASTING: 726371.1			
DRILLER: J. DRABEK	STATIC WATER LEV	EL: 8.57 FT BTOC	COMPLETION DATE: 11/20/2015			
DRILLING COMPANY: CASCADE		DRILLING METHODS	SONIC			
STICK UP: 1.7 FT	PE PE GRI	P OF CASING ELEVATION: _ PROTECTIVE CASING (ves) r A GRAVEL OR SAND OUND SURFACE ELEVATION METER OF RISER PIPE (in.)	no): 4" X 5' ALUMINUM N: _466.7 FT MSL 2.0			
	DIA	METER OF BOREHOLE (in.):	6.0			
1. d. d. d. d. d. d. d. d. d. d. d. d. d.	CO	NCRETE SEAL DEPTH (ft. bg	s): <u>2.5</u>			
	ŢOI		TH (ft. bgs):			
	TYF	PE AND AMOUNT OF BENTO	NITE SEAL: $\frac{3}{8}$ " BENTONITE CHIPS - 1.5 BAGS			
	CEI TOI	NTRALIZER (yes (no) - TYI P OF SCREEN DEPTH (ft. bg:	s):			
			2" X 9.8' SCHEDULE 40 PVC			
		REEN SLOT SIZE (in.):	0.010 IN COARSE: #1 FINE: #0			
			OARSE: 3 BAGS FINE: 1/3 BAG			
		TTOM OF SCREEN DEPTH (1				
	ВО	TTOM OF WELL DEPTH (ft. b	gs):			
TOTAL DEPTH OF BOREHOLE: 25.0 FT	BO TYP	TTOM OF FILTER PACK (ft. b PE AND AMOUNT OF BACKF	gs):23.5 ILL:1.5 - NATURAL CAVE IN			
ADDITIONAL NOTES: FT BGS = FEET BEI 30 GALLONS OF H2O USED DURING DRI VERTICAL DATUM: NAVD88. WELL SURV FT BTOC = FEET BELOW TOP OF CASING	LLING. HORIZONTAL DATUM EYED BY ZAHNER AND ASS	I: STATE PLANE COORDINA OCIATES, INC ON JANUARY	TES NAD83 (2000) MISSOURI EAST ZONE.			

PREPARED BY MEREN JOOG PARTIES



Associates	ABOVE GI	ROUND MONITORII	NG WELL CONSTR	RUCTION LOG <u>LMW-85</u>			
PROJECT NAME: AME	REN CCR GW	MONITORING	PROJECT NUMBER:	153-1406.0001B			
SITE NAME: LABADIE	ENERGY CEN	ITER	LOCATION:LMW-8S				
CLIENT: AMEREN MI	SSOURI		SURFACE ELEVATION: 465.2 FT MSL				
GEOLOGIST: J. INGRAI	М	NORTHING: 991371.2		EASTING: 726351.3			
DRILLER: J. DRABE	<	STATIC WATER LEVE	L: 7.10 FT BTOC	COMPLETION DATE: 11/20/2015			
DRILLING COMPANY:	CASCADE		DRILLING METHODS	: SONIC			
LOCK STICK UP: 2.0 FT		PF	OF CASING ELEVATION: _				
			GRAVEL OR SAND UND SURFACE ELEVATIOI	N: _465.2 FT MSL			
	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	DIAM	IETER OF RISER PIPE (in.): IETER OF BOREHOLE (in.): CRETE SEAL DEPTH (ft. bg	6.0			
		TYPE	E AND AMOUNT OF ANNUL	AR SEAL: NONE			
				PTH (ft. bgs): DNITE SEAL: 3/8 "BENTONITE CHIPS - 1.5 BAGS			
		ТОР	OF SAND PACK DEPTH (ft.	. bgs):COARSE: 10.0 FINE: 9.0			
			TRALIZER (yes no) - TYI				
		TOP	OF SCREEN DEPTH (ft. bgs	s):			
		TYPE	OF SCREEN:	2" X 9.8' SCHEDULE 40 PVC			
		SCR	EEN SLOT SIZE (in.):	0.010 IN			
		SIZE	OF SAND PACK:	COARSE: #1 FINE: #0			
		AMO	UNT OF SAND: C	OARSE: 3 BAGS FINE: 1/3 BAG			
		ВОТ	FOM OF SCREEN DEPTH (f	ft. bgs):			
		ВОТ	ΓΟΜ OF WELL DEPTH (ft. b	gs):			
TOTAL DEPTH 23.2 FT	-		TOM OF FILTER PACK (ft. b	NONE			
OF BOREHOLE: 23.2 FT	_ 🖾 🗀	TYPE	E AND AMOUNT OF BACKF	ILL: INUNE			
VERTICAL DATUM: NAVD8	D DURING DRILL 8. WELL SURVE	ING. HORIZONTAL DATUM: /ED BY ZAHNER AND ASSO	STATE PLANE COORDINA CIATES, INC ON JANUARY	TES NAD83 (2000) MISSOURI EAST ZONE.			
FT BTOC = FEET BELOW T	UP OF CASING.	SAND AND BENTONITE BA	55 WEIGH 50 LBS EACH.				

PREPARED BY MEREN DOSUZOZZI



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG BMW-

ASSUCIALES				
PROJECT NAME: AMEREN CCR GW	MONITORING	PROJECT NUMBER:	153-1406.0001B	
SITE NAME: LABADIE ENERGY CEN	ITER	LOCATION: BMW-1S		
CLIENT: AMEREN MISSOURI		SURFACE ELEVATION: 471.2 FT MSL		
GEOLOGIST: J. INGRAM	NORTHING: 988310.0		EASTING: 715131.6	
DRILLER: J. DRABEK	STATIC WATER LEVEL: 13.60 FT BTOC		COMPLETION DATE: 2/01/2016	
DRILLING COMPANY: CASCADE		DRILLING METHODS	S: SONIC	
LOCK		OF CASING ELEVATION:		

STICK UP: __ — PEA GRAVEL OR SAND GROUND SURFACE ELEVATION: 471.2 FT MSL DIAMETER OF RISER PIPE (in.): ____ DIAMETER OF BOREHOLE (in.): ___ - CONCRETE SEAL DEPTH (ft. bgs): 2.5 NONE TYPE AND AMOUNT OF ANNULAR SEAL: TOP OF BENTONITE SEAL DEPTH (ft. bgs): 2.5 - TYPE AND AMOUNT OF BENTONITE SEAL: $\frac{3}{8}$ " BENTONITE CHIPS - 3 BAGS - TOP OF SAND PACK DEPTH (ft. bgs): COARSE: 17.5 FINE: 16.5 - CENTRALIZER (yes (no)) - TYPE: _____ TOP OF SCREEN DEPTH (ft. bgs): 20.5 TYPE OF SCREEN: 2" X 9.8' SCHEDULE 40 PVC SCREEN SLOT SIZE (in.): 0.010 IN SIZE OF SAND PACK: COARSE: #1 FINE: #0 AMOUNT OF SAND: COARSE: 3 BAGS FINE: 1/2 BAG BOTTOM OF SCREEN DEPTH (ft. bgs): ___ BOTTOM OF WELL DEPTH (ft. bgs): ______30.7 BOTTOM OF FILTER PACK (ft. bgs):

 TYPE AND AMOUNT OF BACKFILL:

 NONE TOTAL DEPTH OF BOREHOLE: 30.7 FT

ADDITIONAL NOTES: FT BGS = FEET BELOW GROUND SURFACE. FT MSL = FEET ABOVE MEAN SEA LEVEL.

100 GALLONS OF H2O USED DURING DRILLING. HORIZONTAL DATUM: STATE PLANE COORDINATES NAD83 US SURVEY FEET (2000)

MISSOURI EAST ZONE. VERTICAL DATUM: NAVD88. WELL SURVEYED BY ZAHNER AND ASSOCIATES, INC ON FEBRUARY 11, 2016. FT BTOC = FEET BELOW TOP OF CASING. SAND AND BENTONITE BAGS WEIGH 50 LBS EACH.

CHECKED BY:	J. INGRAM	
DATE CHECKED:	4/19/2016	



ABOVE GROUND MONITORING WELL CONSTRUCTION LOG ____ BMW-2S

Associates					
PROJECT NAME: AMEREN CCR G	W MONITORING	PROJECT NUMBER: 153-1406.0001B			
SITE NAME: LABADIE ENERGY CE	ENTER	LOCATION:BMW-2S			
CLIENT: AMEREN MISSOURI		SURFACE ELEVATION	ON: 472.5 FT MSL	-	
GEOLOGIST: J. INGRAM	NORTHING: 987210.	1	EASTING: 71510	04.3	
DRILLER: J. DRABEK	STATIC WATER LEV	EL: 14.30 FT BTOC	COMPLETION D	ATE: 2/02/2016	
DRILLING COMPANY: CASCADE		DRILLING METHODS	S: SONIC		
STICK UP: 2.1 FT	PE PE GRO	P OF CASING ELEVATION: ROTECTIVE CASING (yes) A GRAVEL OR SAND DUND SURFACE ELEVATIO METER OF RISER PIPE (in.) METER OF BOREHOLE (in.)	no): 4" X 5' ALUMINU ON: 472.5 FT MSL):	2.0	
	TYF	PE AND AMOUNT OF ANNU	LAR SEAL:	NONE	
10000 00000 00000 00000 00000 00000 00000	▼ TOF	P OF BENTONITE SEAL DEF	PTH (ft. bas):	2.5	
		PE AND AMOUNT OF BENTO			
		P OF SAND PACK DEPTH (ff	= :		
		NTRALIZER (yes no - TY		NONE	
	101	P OF SCREEN DEPTH (ft. bg	Js):	17.9	
	TYF	PE OF SCREEN:	2" X 9.8 SCHEDUL	E 40 PVC	
	SCF	REEN SLOT SIZE (in.):	0.010	IN	
	SIZI	E OF SAND PACK:	COARSE: #1	FINE: #0	
	AMO	OUNT OF SAND:	COARSE: 3 BAGS	FINE: 1/2 BAG	
	ВОТ	TTOM OF SCREEN DEPTH ((ft. bgs):	27.7	
		TTOM OF WELL DEPTH (ft. t		28.1	
TOTAL DEPTH 30.0 FT		TTOM OF FILTER PACK (ft. I		28.1	
OF BOREHOLE: 30.0 FT	■ TYF	PE AND AMOUNT OF BACK	FILL: <u>1.9 F1 - N</u>	ATURAL CAVE IN	
ADDITIONAL NOTES: FT BGS = FEET BEL	OW GROUND SURFACE. FT	Γ MSL = FEET ABOVE MEAN	N SEA LEVEL.		
100 GALLONS OF H2O USED DURING DR				RVEY FEET (2000)	
MISSOURI EAST ZONE. VERTICAL DATUM			IATES, INC ON FEBR	UARY 11, 2016.	
FT BTOC = FEET BELOW TOP OF CASING	غ. SAND AND BENTONITE BA	AGS WEIGH 50 LBS EACH.			

CHECKED BY: J. INGRAM

DATE CHECKED: 4/19/2016

APPENDIX F WELL DEVELOPMENT FORMS



Locat	tion	LMW	-15	1						
Monitor		45		Date	12/11/15		Time	120	5	
Well	Piezom	eter Dat	а		•					
Depth of	Well (from	top of PVC o	r ground)			15.75		feet		
Depth of	Water (fro	m top of PVC	or ground))		9.56	VIII-] feet		
Radius o					2		1	inches		
								feet		- h 4
Casing V	olume/				6.4.3=	20		cubic feet gallons	+	30 gel foundarilla
Devel	opmer	ıt / Purgi	na Dis	chara	e Data		4, 1			= 50 and Hol
Purging I		u.g.	5 13	a. g	Waten	à PUA	np			30 gal foundarilla = 50 gal Hzl
Start Pur	ging			Date	12/11/15		Time	120		
Stop Pur	ging			Date	12/11/15		Time	1534)	
Monitorin	ıg									
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comment
12/11/15	1215	18	15.60	7,74	0.852	71000	1.96	-77.4	9.75	muddy
	1230	30	15.91	7.60	0.850	71000	2.68	-73.4	9.62	middy
	1245	50	15.94	7.55	0.837	71000	2.55	-68.0	9.65	unuddy
	1315	75	15.86	7.53	0.838	71000	1.55	-68.9	9.60	muddy!
	7345	80	16.06	7.55	0.830	71000	3.65	-67.1	9.68	hemore some block
	1413	100	16.13	7.50	0.847	96.1	7.89	-54.8	9.53	cloudy, low flow
	1430	102	16-29	7.58	0.849	80.5	4.31	-63.0	9.42	cloudy, Low flow
	1445	107	16.22	7-55	6.849	32.8	3.32	-59.4	9.52	glardy, low flow
	1500	111	1619	7.58	0.850	18.1	3.05	-62.9	9.48	clear, Low flow
_	1515	118	16.17	7.56	0.851	12.5	4.06	-69.6	9.50	chear, low Flow
	1530	1.52	1620	7.58	0.851	9.38	316	-62.4	9.53	Cherry Low Tow
						E 2 E82				
							1 1-1			
							- '>			
							- 'X			
							- '>			



Project	Ref: A	Ameren GV	V Monite	oring			Project	No.: 153-	1406.	
Locat		LMh	1-25	Date	12/3/15		7 Time	1200		
		eter Dat	a	Date	1.6/2/17] Ilme	1200		
		(circle one) top of PVC o	- 1		56.0			feet		
Depth of		m top of PVC	or ground)		35.6	8		feet inches		
Casing V					5.3 .3:	16		feet cubic feet gallons		+200 gal Hzo from desiling
Devel	opmer	nt / Purgi	ng Dis	charg	e Data					= 216 gal total
Purging N	fethod				Waterra	Pump				
Start Purg	ging			Date	12/3/15		Time	1200		
Stop Purg	ing			Date	12/5/15		Time	0930	>	
Monitorin	9				٩					
Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
12 2 15	1240	MM	14 17	9 66	0 (24	71000	196	-011 0	3690	

Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
12315	1240	40	15.27	9.55	0.574	71000	1.96	-174.2	36.90	muddie
	1300	70	18.02	9.72	0.577	438	1.75	1.606-	37.04	cloudy
	1320	120	17.56	9.85	0.563	104	1.53	-232.4	37.24	cloudy
	1340	150	18.16	9.65	0.560	83.2	1.16	-221.2	37.06	cloudy
	1460	185	17.98	9.78	0.562	64.5	1.57	-214.5	37.10	cloudy
	1415	215	18.18	9.74	0.563	43.0	1.02	-210.1	37.01	clardy, remove surge bloc
	1425	220	16.92	9.50	0.550	74.5	5.08	-134.3	3/2.95	Cloudy, I how flow
	1500	225	16.52	9.44	0.547	129	3.19	-160.6	35.68	cloudy Lowflow
- tal	1525	227	16.04	9.45	0.53%	113	3.20	-158.1	35.60	cloudy, your flow
14/11	0750		-	pan			_	_		Resume purge
	0811	135	~	-	-	18.0	-	-	36.53	Clear
	0847	249	16.66	8.55	0764	16.5	4.79	-81-8	36.33	elear
	0900	257	17.09	9.52	0,766	24-9	4.78	-73.9	36.25	clear
	0970		17-43	7.65	0.774	26.7	4.56	-94.0	36.42	Clear
	0920	265	17.35	9.71	0-764	26.1	4.52	103-4	36.76	clear
	0930	270	17.51	9.70	0.777	7.87	4.42	-107.8	36.75	deed
	We see the		100					192-P-18		
			100 113	AU.						
-						3× == 1				
								,ä.		
		-								
		2 7552								
					KILLIN IN					

Menore Surge block

Project Ref: Ameren GW Monitoring	Projec	t No.: 153-1406. 604
Location LMW-3sa		
Monitored By: Date	LIZ 16 Time	1243
Well Piezometer Data		
(circle one) Depth of Well (from top of PVC or ground)	71.98	feet
Depth of Water (from top of PVC or ground)	32.55	feet
Radius of Casing	3	inches feet
Casing Volume	10,25 . 3 = 30.75	gallons +250 gal 420 from da: 11 in = 281 yal Mao total
Development / Purging Discharg	e Data	= 201 9 1 1 2
Purging Method	Waterra	
Start Purging Date	2 12 16 Time	1256
Stop Purging Date	2/12/16 Time	1710
Monitoring		

Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
2/12/16	1310	40	15.14	7.83	0.7.54	71000	1-24	61.2	50.69	mully
	1320	55	16.02	8.61	0.764	71000	0.98	18.3	58.37	V. closdy
	1325	65	16.58	803	8.764	71000	0.96	-19.1	56.26	V. Cloudy
igital Assig	1335	85	16.83	8.05	0.773	71000	0.70	-37.3	86.55	U. Cloudy
	1345	95	17-06	8.02	0.769	7/060	0.71	-51.2	56.00	v cloudy
	1400	120	17.01	7.89	8FF.0	71000	0.70	-61.9	56.58	y cloudy
	1415	130	16.40	7.97	O. 816	7/000	0.46	-35.4	37.29	y. mulby
	1430	175	17.10	7.88	0.845	71000	0-88	-72.0	33.85	J. cloudy
	1445	210	17.00	7.75	6.854	71000	6.86	-39.5	33.21	V. Clark
	1500	230	16.77	7.75	0.852	205	3.37	-69.2	33.14	cloudy
	1507	245	-	-		-	S ST	-	1	Dunp purge wreter
9	1528	250	-	-	-			-	33-65	Resume purge, remove surje
	1535	286	16.44	7.70		333	1.04	-70.1	33.42	V. Cloydy
	1550	310	16.06	7.74	0. 944	170	0.86	-71.7	33.32	Cloudy
	1600	320	15.51	7.72	0.840	473	127	-71.2	33.04	V. Cloudy
	1615	340	16.24	7.68	6.837	236	15.0	-69.4	33.00	y, cloudly
	1630	365	14.73	7.75	D.851	160	6.51	-80.8	32.59	cloudy
	1640	375	15.92	7.72	0.845	78.1	6.99	-87.7	32.40	cloudy
	1650		16.23	7.69	0.844	74.9	0.85		32.89	cloudy
	1700	400	16.15	7.71	0.843	154.0	0.08		32.88	clordy
	1710	410	16.22	7.66	0.842	116.0	1.05	-71.3	32.89	cloudy parse purge
			9883 1							



Project Ref: Ameren GW Monitoring	Project	No.: 153-1406.	cost
Location LMW-35			
Monitored By: Date	7/19/16 Time	6729	
Well Piezometer Data (circle one)			(71.98-33.45)0.163 =
Depth of Well (from top of PVC or ground)	71.98	feet	(H148 - 27 12)
Depth of Water (from top of PVC or ground)	3348	feet	
Radius of Casing	_ 2	inches feet (1.4690.30) - (0.163.) =
Casing Volume	• 3=	cubic feet gallons	

Development / Purging Discharge Data

Purging Method		Waterra		
Start Purging	Date 2	19/16	Time	0740
Stop Purging	Date 2	119/16	Time	1600

Monitoring

Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
119/16	1125	120	14.48	6.46	0.946	29.8	1.18	-66.5	34.20	Clear
	H35	145	14.45	6.62	0.942	28.0	1.31	-68.1	34.21	Clear
	1145	165	14.52	6.61	0.939	23.5	1.28	-69.7	34.03	clear
	1155	185	14.57	6.63	6.931	25.9	1.30	-84.1	34.04	Clear
. 244	1205	190	14.96	6.72	0.938	71.3	1-17	-86.0	33.65	D.I. water reads 2.39 N
	1220	195	15.07	6.78	0.939	51.4	1-26	-93.8	33.65	clear
	1235	203	15.16	6.85	6.938	37.4	1.42	-94.6	33.67	clear
	1250	207	1510	6.84	0.938	33-b	1.43	-95.1	33.66	Clear
	1305	210	15.06	6.87	0.938	32.8	1.43	-87-4	33.66	Clear
	1320	216	5.09	6.89	0,939	31.2	1-26	-90.4	33.66	elear
	1335	222	15.13	6.94	9.943	28.2	1.52	-79.1	33.65	deat
	1350	225	15.48	7.01	0.946	27.4	1.60		33.65	class
	1405	129	15.44	7.10	0.946	26.5	1.56	-95.2	33.65	chand
	1420	233		6.95	0.946	26.2	1.54	-81.1	33.65	clear
	1435	240	15.50	7.02	6.947	22.5	1-48	-81.8	33.65	clear
	1440	5 200	-	-	_	-		-		Ovas pure Water
	1455	150	17.42	7.06	0.932	229	1.57		33.64	chant
	1510	255	15.4%	6.93	0.947	16.8	1.59	-839	33.65	they
	1520	260	15.21	6.71	0.941	11.2	1.61	-72.8	33.65	clear
	1530	264	15.11	6.77	0.936	8.43	1.75	-73.1	33.66	Clear
	1540	240	14.91	6.81	0.934	7.88	2.16	-74.8	33.65	elser
	1545	272	14.79		0.937	7.73	1.76	-66.2	33.65	class
	1550				0.934	7.71	1.71	-52.3	33.67	elen
	1600	285	14.76	6.79	0.934	7.31	1-74	-51.9	33.66	Clear
	1610								de la constantina	
					2				W	
100				V						

post Devit +D: 72,00



Project Ref: Ameren GW Monito	ring	Project	No.: 153-14	06. 000/	
Location LMV-48					
Monitored By: 75	Date 11/30/15	Time	12/1		
Well Piezometer Data					
(circle one) Depth of Well (from top of PVO or ground)	34.83	?	feet		
Depth of Water (from op of PVC or ground)			feet		
Radius of Casing	2		inches		
Casing Volume	1.29.3	= 22 9=1	cubic feet	+150 301	Hoo From willing
Development / Purging Disc		0		= 172	391
Purging Method	Wat	rere			
Start Purging	Date 1/35/15	Time	1226		
Stop Purging	Date 11/30/1	Time	1444		
Monitoring					
Date Time Discharge (*)	pH Spec.Cond.	Turbidity Dissolved Oxygen	Potential	WL (ft Appearance	ce of Water and Comments

Date	Time	Volume Discharge (gals)	Temp	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
11 30 15	1246	25	15.15	7.37	0.856	71000	1,39	-47.1	14.99	Muddin
	1306	60	16.19	7.77	6.902	71000	0.66	-99.3	15.42	moddy
	1326	95	16.02	7.75	0.905	71000	0.71	1-[0]-	15.24	Cloude
	1346	115	16.01	7-73	0.915	71000	0.70	-100,9	15.18	c. ovdy
	1353	125	~	-		-	1			REMOVE SURGE BOCK
2	1413	155	15,91	7.74	0.917	8.97	1.73	-92.6	14.93	Clear
	14/23	165	15.99	7.40	-0.920	7.08	1.86	-90.9	14.92	clear
	1433	170	15-93	7.73	0.914	6.24	2.42	-90.0	14.90	Clear
	1443	175	15.90	7.73	0.411	4.64	2.413	-90.4	14.88	clear
			3 10			4 5 15				
4					30					
						-				
				5713 31						
									1111/2	
	-									
						The second		100		



Project	Ref: A	meren GV	V Monito	oring			Project	No.: 153-	1406.	
Locati	ion	LMh	1-55							
Monitore	ed By:	75		Date	12 1115	911	Time	082	8	
Nell F	Piezom	eter Data	a							
		(circle one)						,		
		top of PVC)or			23.96			feet		
100		m top of PVS	or ground)		10.38			feet		
adius of	Casing				2			inches		
Casina Va	eli ime							_feet		+ 75 gal Hzo used in dil
asing Vo	biume				5.7 .3	- 17.04	1	cubic feet gallons		t 75 gal Hzo used in ant
- 6							2 3			2 15 g. (total
Devel	opmen	t / Purgi	ng Dis	charge	e Data					VALUE OF THE PARTY
urging N	Method				Waterra					
Start Purg	ging			Date	12/1/15		Time	0851	2	
Stop Purg	jing			Date	12/1/15		Time	1243	3	
Monitoring	g							The same of	J. E.	
	V	Volume	Town				Dissolved	Redox		
Date	Time	Discharge (gals)	Temp (°)	рH	Spec.Cond. (_S/cm)	Turbidity (NTU)	Oxygen (mg/L)	Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
2/1/15		3	15.80	6.83	0.469	71000	2.52	42.4	10.90	Middy
	0121	20	15 95	7.30	6.497	71000	2.20	32.8	10.71	Muldy
+	1001	40	15.93	7.33	0.507	71006	2.58	6.0	10.61	Stately mulder
	1021	80	16.10	7,70	0.50%	7315	247	5.9	10.75	
	1025	85	16.06	7.33	0.506	180	2.52	4.6	10.80	Cloudy Sugar block
	1100	95	14.70	735	0.491	39.0	4.04	8.0	10.48	clede
	1120	97	15-15	7.38	0.504	42.7	4.71	7.4	10.42	clear
1 /8	1140	99	15-44	7.40	0.502	28.2		6.8	10.12	clear
1	1236	103	14.43	7.38	0.493	23.0	4.28	5.1	9.80	took break for drill
	1240	104	15.78	7.40	0.512	17.0	3.52	8.9	9.78	
									*	
	91							Marin M		
				200						
		34 4								
		4)							
										
-										

Project	Ref: A	meren GV	V Monite	oring			Project	No.: 153-	1406.	
Locat	ion	LMU	v - 65		- 630 2 30 - 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		7 12 3			
Monitore	ed By:	J5		Date	12/1/1	15	Time	1315		
Well F	Piezom	eter Data	a							
Donth of	Mall (fram)	(circle one)	r around)		25,09] feet		A PARTY OF
		n top of PVC			10.49	Facility and the second]feet		
Radius of		mop of 1 vo	pi ground,		2			linches		
Tradias of	Cusing				-			feet		
Casing V	olume							cubic feet	+	30 gal theo used for drilli
					6.H .3	= 20		galions	東行門	
Devel	opmen	t / Purgi	ng Dis	charg	e Data					: 50 gal
Purging N	Method	4			Waterra	Pump				
Start Purg	ging			Date	12/1/15		Time	1320		
Stop Purg	1			Date	12/2/15		Time	083	0	
Monitorin										
	9		X 95 5						T	
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
12/1/15	1331	5	13.95	7.57	0.742	71000	1.92	-78.1	10.69	Moddy
1	1340	20	15.51	7.73	0.739	71000	087	-93.0	10.65	msddy
	1350	40	1597	7.62	0.732	71000	1.51	-60.7	10.63	moddy
	1400	50	16.37	7.55	6.734	71600	1-16	-	10.62	muddy, Remove Surge block
	1440	60	15.70	7.72	0.725	3/000	5,00	- 75.8	10.35	Cloudy surge block
	1450	62	15.43	7.71	0-731	477	5.42	-75.5	10.33	Cloudy
4	1536	64	14.23	773	0.705	145	6,02	-74.9	10-28	cloudy
12/2/5	0755	7		-	-	- 1	-	1	-	Resurbe purige
1	0820	66	14.10	7.33	8-932	20.8	3.76	-75.0	9.91	clear
4	0\$30	67	14.76	7.60	6-945	16.6	3.29	-76.3	9.81	Clear
									2 20 20 20	
			Tall							
						7. 7.				

Project Ref: Ameren GW Monito	ring	Project No.: 153-14	06. 0 66 (
Location LMw-45			
Monitored By: \\ \mathcal{J}\lambda	Date 12/2/15	Time 0901	
Well Piezometer Data (circle one)			
Depth of Well (from top of PVC or ground)	25.27	feet	
Depth of Water (from top of PVC or ground)	8.57	feet	
Radius of Casing	2	inches	
Casing Volume	6.2 · 3 = 19	cubic feet gallons	+ 30 gal You durling = 49 gal total
Development / Purging Disc	harge Data		. 7 3
Purging Method	Waterra Pump	•	
Start Purging	Date [12/2/15	Time 0914	
Stop Purging	Date 12/2/15	Time 1230	

Monitoring

Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
12/2/15	0913	10	14.41	7.25	0.912	71000	1.61	6.2	8.90	an v dely
	0943	35	14.24	7.34	0.896	71000	1.73	-44.9	8.83	muddy
	1003	50	_			-	11111			Remove Surge Glock
	1020	SI	13.88	7.56	0.773	454	8.07	-50.3	8.55	Cloudy, Low & low
	1035	54	13.72	7.45	0.878	343	3.87	-46.7	8.58	Clouded, Low flow
	1050	57	13.84	7.52	0.879	197	5.14	-52-8	8.44	Clauly, Low Flow
	1105	58	13.54	7.47	0-875	159	3.72	-48.6	8.57	Closly, Low flow
	1130	60	13.43	7.45	0.881	76.6	5.55	-46.1	8,51	Sing My claude, low flow
	1150	62	14.99	7.47	11.904	46.9	5.04	-47.4	8.56	Strate cloudy low 101
1	1216	63	14.62	7.49	0.896	35.9	4.90	-47.9	8.55	chear, ford flow
	1220	63		7.47	0.899	25.2	5.28	-49.7	8.52	clear, for Flor
	1230	64	14.18	7.47	0.892	18.1	5-33	-49.2	8.52	clear, ten flow
-										
				_						
			-						-	
			100							
				-		- V 1		THE WAY		
							7977			
	7 20 10		F 20.5							
						-				



1405 67 13.69 7.62 1.080 54.5 3.58 -84.4 7.10 slightly cloudy, la 1410 70 13.66 7.63 1.093 24.0 2.85 -83.0 7.11 clear, low t 1430 72 13.52 7.62 1.098 16.3 2.97 -85.9 7.13 clear, law flo 1440 75 13.23 7.62 1.076 13.7 3.01 -87.4 7.10 clear, low flo 1450 77 13.13 7.61 1.074 19.1 3.43 -80.2 7.11 clear, law flo	
Depth of Well (from top of PVC or ground) Depth of Well (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of PVC or ground	
Depth of Well (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Water (from top of PVC or ground) Depth of Start Purging Depth of Water (from top of PVC or ground) Depth of Start Purging Date Depth of Water (from top of PVC or ground) Depth of Start Purging Date Depth of Water (from top of PVC or ground) Depth of Start Purging Date Depth o	
Peet Peet	
Casing C	
Spec.Cond. Time Casharge	
Development / Purging Discharge Data Turging Method Start Purging Date Time Discharge (°C) Date Time Discharge (°C) Discharge Discharge (°C) Discharge Discharge (°C) Discharge Discharge (°C) Discharge Discharg	
Development / Purging Discharge Data Unatro	
Date Time Discharge (gals) PH Spec.Cond. (m.S/cm) Turbidity (NTU) Dissolved (mg/L) Potential (+/- mV) Potential (+/-	
Date Time Discharge (gals) PH Spec.Cond. (MS/cm) Spec.Cond. (MS/cm) Dissolved Oxygen (mg/L) Potential (+/-mV)	floor d
Date Time Discharge (gals) PH Spec.Cond. (M.S/cm) Spec.Cond. (M.S/cm) Dissolved Oxygen (mg/L) Potential (H/-mV	
Date Time Volume Temp pH Spec.Cond. Turbidity Oxygen (ms/cm) NTU Dissolved Oxygen (mg/L) Potential (+/-mV) BTOC) Appearance of Water are (mg/L) 1305 30 14.55 7.57 1.067 71.000 1.51 77.8 7.38 mudly 1325 40 14.81 7.64 1.081 71.000 94 -87.2 7.29 mudly 1345 60	1 tot-
Date Time Discharge (gals) Temp Discharge (gals) PH Spec.Cond. Turbidity Oxygen (mg/L) PH Spec.Cond. (mS/cm) Turbidity Oxygen (mg/L) Potential (+/- mV) Potentia	
Date Time Discharge (gals) PH Spec.Cond. (MS/cm) NTU) Oxygen (mg/L) Potential (+/- mV) Po	
1325 40 14.86 7.64 1.081 71000 1.94 -87.2 7.29 moldy 1345 60	d Comment
1345 0	
1350 62 1445 4.60 1.093 207 3.90 -77.7 7.41 cloudy, lowfl 1400 65 13.85 7.61 1.078 20 7 3.50 -81.4 7.08 Clusty, low- 1405 67 13.69 7.62 1.080 54.5 3.58 -84.4 7.10 slightly cloudy, low- 1405 70 13.66 7.63 1.093 24.0 2.85 -83.0 7.11 cloudy, low- 1430 72 13.52 7.62 1.098 16.3 2.97 -85.9 7.13 clear, low-f 1440 75 13.23 7.62 1.076 13.7 3.01 -87.4 7.10 clear, low-f 1450 77 13.13 7.61 1.074 19.1 3.43 -80.2 7.11 clear, low-flow-	//-
1400 65 13.85 7.61 1.078 20 7 3.50 - 81.4 7.08 Clashy, fow 1405 67 13.69 7.62 1.080 54.5 3.58 - 84.4 7.10 slightly cloudy, for 1400 70 13.66 7.63 1.093 24.0 2.85 - 83.0 7.11 clear, low for 1430 72 13.52 7.62 1.098 16.3 2.97 - 85.9 7.13 clear, low for 1440 75 13.23 7.62 1.076 13.7 3.01 - 87.4 7.10 clear, low flow 1450 77 13.13 7.61 1.074 19.1 3.43 - 80.2 7.11 clear, low flow	-
1430 70 13.66 7.63 1.093 24.0 2.85 -83.0 7.11 clear, low to 1430 72 13.52 7.62 1.098 16.3 2.97 -85.9 7.13 clear, low flow 1440 75 13.23 7.62 1.076 13.7 3.01 -87.4 7.10 clear, low flow 1450 77 13.13 7.61 1.074 19.1 3.43 -80.2 7.11 clear, low flow flow 1450 77 13.13 7.61 1.074 19.1 3.43 -80.2 7.11 clear, low flow 19.1	Flow
1430 72 13.52 7.62 1.098 16.3 2.97 -85.9 7.13 C/cav, law for 1440 75 13.23 7.62 1.076 13.7 3.01 -874 7.10 C/cav, low fly 1450 77 13.13 7.61 1.074 19.1 3.43 -80.2 7.11 C/cav, law flo	w flow
1440 75 13.23 7.62 1.076 13.7 3.01 -874 7.10 clear, low fl 4 1450 77 13.13 7.61 1.074 19.1 3.43 -80.2 7.11 clear, law flo	taw
4 1450 77 13.13 7.61 1.074 19.1 3.43 -80.2 7.11 Clear, lawflo	
V 1500 80 13.05 7.60 1.080 17.4 3.37 - 83.4 7.10 Clear, low fl	ow



Project	Ref: A	meren GV	V Monite	oring	. 6		Project	No.: 153-	1406. ©	001
Locat	ion	BMW	-15							1
Monitore	ed By:	75	b	Date	2/11/16		Time	1200		j
Well F	Piezom	eter Data	a							
Depth of	Well (from	(circle one) top of PVC or	r ground)		33.63			feet		
Depth of	Water (fro	m top of PVC	or ground)		13.52			feet	4	
Radius of	Casing				2			inches		
								feet		
Casing V	olume							cubic feet	+100	Gal Wan from donting
					7.3 . 3	= 22		gallons		2
Devel	opmen	nt / Purgi	na Dis	charg	e Data					gal Mad from dorthing 122 gal Had
Purging N			.9	J	Wat	. CCm				1
				D-4-	2/11/16	E	1 -	13 ==		
Start Purg							Time	1202		
Stop Purg	ging			Date	2/11/16		Time	1437		
Monitorin	9									
Date	Time	Volume Discharge (gals)	Temp (°)	pН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
211/16	1220	30	12.40	6.94	1.267	259	1.70	-57.0	13.60	V. Cloudy
Print.	1226	-	_				- Allerino			Survey well
	1240	40	12.81	6.91	1.274	138	1.94	-46.1	13-65	cloudy
	250	90	12.85	6.92	1.277	108	1-25	-47.2	13.71	Cloudy
	1300	110	12,71	6.90	1.289	71000	4.33	-43.5	13.68	V. Clarky
But of	320	145	11.48	689	1.078	467	6.72	16-1	13.60	V. Cloudy scenare Surge blog
	1346	150	9.41	6.81	1.214	71000	5.40	14.7	13.53	v. cloudy fow flow
	1405	154	9.68	6.76	1.229	71000	3.74	+7.6	13.54	V. Cloudy
	1415	165	11.54	6.91	1.283	24.0	2.97	-3.0	13.55	cloudy
	1425	170	11.52	6.95	1.250	10.5	1.74	-14.6	13.60	Cleur
	1435	174	11.40	6.95	1-254	5.34	1-69	-17.3	13.63	Clew
					Name of the last					
						1000				
				1		o general				
						ma. I				

post Devit TD: 33.06



		ociales			VELOTIV	112141/1				201
Locat		meren GV		oring			Project	No.: 153-	1406. 🗷	1
Locat	ion	BMW	ds							
Monitore	ed By:	55		Date	2/12/1	6	Time	073	D	
Well F	Piezom	eter Data	a							
Depth of	Well (from	top of PVC o	r ground)		30.17			feet		
		m top of PVC			14.34	(159s) (L)] feet		
		ii top oi i v c	or ground,					1		
Radius of	Casing				2			inches		
								feet		11 - for 111
Casing V	olume				-			cubic feet	+10	2 gal H10 from 11.7. Zbg-1 H10 botal
1.					6.4 -3=	= 25.7		gallons	- 1	7 hard Mar Lotal
Devel	opmen	t / Purgi	ng Dis	charg	e Data					203-11/2 600 1
Purging N	Method				Water	16a				
				Dete			1 -	03//	6	
Start Pur				Date	2/12/16		Time	074	Y	
Stop Purg	ging			Date	91121/2		Time	1132		
Monitorin										
WOTHLOTH	9	_		T		post, juy to to				
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft BTOC)	Appearance of Water and Comments
2/12/16	828	30	12.98	7.09	0.763	71000	2.30	144.9	14.40	nully
	0840	40	13.04	7.37	0.755	71000	7.22	128.4	14.44	muldy
	0850	50	3.00	736	0.741	71000	2.24	104.7	14.43	maly
	0906	60	13.31	7.32	0.741	71600	1.33	104.2	14.60	slightly moddy
	0916	70	13.77	7.29	6.737	7/000	2.03	104.7	14.61	51, Thaty modely
- 54	0976	88	12.89	7.26	0.739	71600	2.27	106.7	14.61	U. cloudy remove surge block
	0930	90	13.56	7.28	0.730	71000	1,92	163.8	14.61	v. cloudy
	1950	100	17.10	7.28	6-731	71006	1.79	102.9	14-36	V. Clardy
	1005	145	12.56	7.30	6.731	7.1.3	1.74	111.2	1462	clear
	1012	150	11-10	7.32	0.733	84.1	1.78	108.1	14.63	cloudy, low flow
	1022	153	9.40	7.31	6 733	79.1	1.76	180-1	14.40	cloudy law flow
	1032	156	16.91	7 33	0.737	150	2.04	103.4	14.49	U. Clarky for flow
	1042	157	11.85	731	6.734	86.1	2.45	101.4	14.50	Victory, for flow
	1652	159	12.32	7.31	6.729	69.9	2.31	97.1	14.45	clady, lar Hou
	1115	163	12.31	7.30	0,733	38.5	7.38	98.9	14.50	clear, for the
23	1130	170	12.32	Contract of the Contract of th	0-727	21.6	2,30	96.0	14.54	clear fur flow
	1146	173	1239		A 7332	111.4	731		110 55	Claric b. Man

9212

12.55

post Devit TD:36.15

150

APPENDIX G CCR MDNR WELL CERTIFICATION FORMS

MISSOURI DEPARTMEN		REF NO		DAT	ATE RECEIVED					
NATURAL RESOURCES		CR NO	512868	CHE	CK NO.		01/27/20	016		
DIVISION OF	LIDVEV				170077					
GEOLOGY AND LAND S	URVEY	STATE WELL NO		1		REVENU	E NO.			
(573) 368-2165 MONITORING WELL		A206237 02/04/2016					012716			
CERTIFICATION RECORD		ENTERED NRBA PH1 PH2	SSM PH3		APPROVED B	Y		ROUTE		
CENTIFICATION RECORD		02/01/2016 02/01/2016 02/01/2016								
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NTRACTOR OR	DRILLING CC	NTRACTOR							
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	RI C/O BILL KUTOS	SKY					VARIANCE GRANTED BY DNR			
OWNER ADDRESS 3750 S. LINDBERGH BLVD.			STA'	STATE ZIP 63127			NUMBER			
SITE NAME LABADIE ENERGY CENTER			WEL	L NUMBER /1S			COUNTY FRANKLIN			
SITE ADDRESS 226 LABADIE POWER PLANT RD			CITY				STATIC WATER LEVEL 9.5 FT			
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D SURFACE COMPL PLACED				ION GROUT		N OF WEL			
X ABOVE GROUND LENGTH 5.0 FT.	DIAMETER 12.0						LAT. 38 ° 33' 14.39" LONG. 90 ° 49' 45.49"			
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH <u>2.5</u> FT.		OTHER				 _LEST	LARGEST		
								1/4 SE 1/4		
LOCKING CAP			_ SURFACE COMPL	ETTIC	N					
WEEP HOLE	T	\exists T $$	STEEL X AL	LUMINUM	PLASTIC			TWN. <u>44</u> NORTH		
		- 11				RANGE	2 RING FOR:	Direction <u>E</u>		
						RADIONL	JCLIDES	PETROLEUM PRODUCTS ONLY		
			 RISER			EXPLOSI SVOCS	ves X	METALS VOC PESTICIDES/HERBICIDESS		
ELEVATIONFT.	Г '		RISER PIPE DIAME	TER	2.0IN.		_			
			RISER PIPE LENGT	н _	<u>15.6</u> FT.	PROPOS	ED USE O	F WELL		
ANNULAR SEAL			HOLE DIAMETER			I 📙	GRATION WELL			
LENGTH0.0FT.		++	WEIGHT OR SDR#		SCH40	PIEZON	CTION WELL	OPEN HOLE		
SLURRY CHIPS			MATERIAL			DIRECT				
PELLETS GRANULAR CEMENT/SLURRY			MATERIAL STEEL	X THEF	MOPLASTIC (PVC)	DEF	PTH	FORMATION		
IF CEMENT/BENTONITE MIX:			OTHER			FROM	то	DESCRIPTION		
BAGS OF CEMENT USED:						0.0	1.0	FILL SND		
%OF BENTONITE USED:						1.0	5.0	SLT		
WATER USED/BAG: GAL.						5.0		STY CLY		
			BENTONITE SEAL			10.0		SND		
			LENGTH: 7.5	.ETS	GRANULAR	13.0 15.0	15.0 25.0	STY SND SND		
			SLURRY		I	10.0	20.0	OND		
			SATURATED ZONE		HYDRATED					
SECONDARY FILTER PACK										
LENGTH:1.0FT.			SCREEN							
	<u> </u>	SCREEN DIAMETER: 2.0IN.								
			SCREEN LENGTH:							
DEPTH TO TOP OF PRIMARY			DIAMETER OF DRI							
FILTER PACK:11.2FT.			<u></u>		· · ·					

LENGTH OF PRIMARY FILTER

PACK: _____12.8FT.

SCREEN MATERIAL

OTHER

X THERMOPLASTIC (PVC)

TOTAL DEPTH:

24.0 FEET

MISSOURI DEPARTMENT OF			REF NO		DATE RECE	DATE RECEIVED				
	JRAL RESOURCES			0512869	OUEOU NO			01/27/20	16	
	SION OF		CR NO		CHECK NO.	170077				
	LOGY AND LAND S	URVEY	STATE WELL NO)		R	REVENUE			
	368-2165		A206238	02/04/2016			012716			
MONITORING W			ENTERED NRBA	APPRO	APPROVED BY			ROUTE		
CERTIFICATION	RECORD		PH1 PH2	PH3						
INFORMATION OF DE	NIED DV DDIMADY OOM	ITD 4 OTOD OD		/2016 02/01/2016						
NOTE: THIS FORM IS NOT TO BE USED F	PLIED BY PRIMARY CONFORNESTED WELLS	NIRACIOR OR	DRILLING CO	DNIRACIOR						
OWNER NAME AMEREN MISSOURI C/O BI	LL KUTOSKY	RI C/O BILL KUTO	SKY					VARIANCE GRANT DNR	ED BY	
OWNER ADDRESS 3750 S. LINDBERGH BLVD.			STATE MO				NUMBER	_		
SITE NAME LABADIE ENERGY CENTER			WELL NUMI	IBER			COUNTY FRANKLIN			
SITE ADDRESS 226 LABADIE POWER PLAN			CITY LABADIE				STATIC WATER LE 35.68			
SURFACE COMPLETION TYPE	LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND DI SURFACE COMPL		LE SURFACE CO	MPLETION GF	ROUT L	OCATIO	N OF WELI	-	
X ABOVE GROUND	LENGTH 5.0 FT.	PLACED DIAMETER 12.0	IN.	X CONCRET	TE	L	AT.	38°3	3' 27.11"	
	DIAMETER 4.0 IN.	LENGTH 2.5 FT.				90° 4				
							SMAL	LEST	LARGEST	
LOCKING CAP				SURFACE COMPL	FTTION			1/4	1/4	<u>SE</u> 1/4
WEEP HOLE		Ļ —				PLASTIC S	SEC	18 7	WN44 NOR	ты
WEET HOLE		Ir					RANGE		Direction <u>E</u>	
		- 11				N	ONITOR	ING FOR:		
							RADIONU EXPLOSI\		PETROLEUM PRODUCTS ONLY METALS VOC	
		_		RISER			SVOCS		PESTICIDES/HERBICIDESS	
ELEVATION	FT.			RISER PIPE DIAME	•					
ANNIII AD SEAI				RISER PIPE LENGT		1 1		ED USE OF	WELL X OBSERVATION	
ANNULAR SEAL LENGTH37	5FT			HOLE DIAMETER WEIGHT OR SDR#		1 1		TION WELL	OPEN HOLE	
— —	_						PIEZOM		_	
SLURRY CHI PELLETS GRA	PS ANULAR	_		MATERIAL			DIRECT	PUSH		
CEMENT/SLURRY				STEEL	X THERMOPLAST	TIC (PVC)	DEP	TH	FORMATION	
IF CEMENT/BENTON	III E MIX:			OTHER			FROM	ТО	DESCRIPTION	
BAGS OF CEMENT U	JSED:			L			0.0	5.0	HYDROVAC	
%OF BENTONITE US							5.0		SLT	
WATER USED/BAG:	GAL.			BENTONITE SEAL			27.5 32.1		STY SND SDY SLT	
				LENGTH:6.0			38.0		STY SND	
				CHIPS PELI	LETS GRA	ANULAR	40.0	54.0	SND	
				SLURRY						
SECONDARY 5" TE	D DACK			SATURATED ZONE	HYE	DRATED				
SECONDARY FILTE LENGTH:(-								
				SCREEN						
				SCREEN DIAMETE						
DEDTI: TO TOO :	_ -	SCREEN LENGTH DIAMETER OF DR								
DEPTH TO TOP OF F FILTER PACK:		DEPTH TO TOP _								
	-	1 188 ***	01910 A 700	I						

TOTAL DEPTH: _54.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x <u>JEFFREY INGRAM</u> 006124 11/23/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _______7.8FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMEN		REF NO		DATE RECEIVED					
NATURAL RESOURCES		CR NO	00304714	CHECK NO.		03/14/201	6		
DIVISION OF	LIDVEV	0.1110		0.120111101	170083				
GEOLOGY AND LAND S (573) 368-2165	URVEY	STATE WELL		1	REVENUE NO.				
MONITORING WELL		A206414 ENTERED NR	03/15/2016	APPROVED B	Y		031416 ROUTE		
CERTIFICATION RECORD		PH1 PH2		APPROVED B	Ť		OUTE		
OZKINIOK KZOOKS			/15/2016 03/15/2016						
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NTRACTOR OR	DRILLING	CONTRACTOR						
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KU	TOSKY				VARIANCE GRANTED BY DNR		
OWNER ADDRESS 3750 S LINDEBERGH BLVD			STATE ZIP 63127			NUMBER			
SITE NAME LABADIE ENERGY CNETER			WELL NUMBER LMW3S			COUNTY ST LOUIS CITY			
SITE ADDRESS 226 LABADIE POWER PLANT ROAD				CITY ST LOUIS			STATIC WATER LEVEL 32.6 FT		
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF	DIAMETER AND D		HOLE SURFACE CO	MPLETION GROUT	LOCATIO	N OF WELL			
SURFACE COMPLETION	SURFACE COMPL PLACED DIAMETER 12.0								
X ABOVE GROUND LENGTH 5.0 FT. FLUSH MOUNT DIAMETER 4.0 IN.	IN.	X CONCRET OTHER			38 ° 33 90 ° 49				
<u> </u>	LENGTH <u>2.5</u> FT.					LLEST	LARGEST		
LOCKING CAP			SURFACE COMPL	ETTION		1/4	1/4 NE 1/4		
WEEP HOLE	<u></u>			LUMINUM PLASTIC	SEC	18 T\	VN44 NORTH		
WEET HOLE	Ir				RANGE		Direction <u>E</u>		
						RING FOR:			
					EXPLOS	1/	PETROLEUM PRODUCTS ONLY METALS VOC		
	_		RISER		svocs		PESTICIDES/HERBICIDESS		
ELEVATIONFT.			RISER PIPE DIAME	TER2.0IN.	PROPOS	ED USE OF	WELL		
ANNULAR SEAL			HOLE DIAMETER			GRATION WELL	X OBSERVATION		
LENGTH <u>46.5</u> FT.			WEIGHT OR SDR#	SCH40		CTION WELL	OPEN HOLE		
SLURRY CHIPS					DIRECT				
PELLETS GRANULAR CEMENT/SLURRY	- 11		MATERIAL STEEL	X THERMOPLASTIC (PVC)	DEI	OTI I	FORMATION		
IF CEMENT/BENTONITE MIX:			OTHER	A meranor exerce (i vo)	FROM	ТО	DESCRIPTION		
BAGS OF CEMENT USED:					0.0	0.5	SND SLT		
%OF BENTONITE USED:					0.5		SND		
WATER USED/BAG: GAL.					19.5	21.0 S	SND SLT		
			BENTONITE SEAL		21.0		IND CLY SLT		
			LENGTH:	ETS GRANULAR	23.7 47.1		SLY SND SND SLT CLY		
			SLURRY	<u></u>	54.5		STY CLY		
			SATURATED ZONE	HYDRATED	57.9		CLY SND		
SECONDARY FILTER PACK					60.0	70.0 S	SND		
LENGTH:1.0FT.			SCREEN						
			SCREEN DIAMETE						
			SCREEN LENGTH						
DEPTH TO TOP OF PRIMARY FILTER PACK: 57.7FT			DIAMETER OF DR DEPTH TO TOP						
FILLER PAGE: 5/ /FI	1 (0.000)	TO CONTROL OF THE PARTY OF THE							

TOTAL DEPTH: _70.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x <u>JEFFREY INGRAM</u> 006124 02/02/2016 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: <u>12.3</u>FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMEN		REF NO	DATE RECEIVED						
NATURAL RESOURCES		CR NO	00512871	CHECK NO.		01/27/20	16		
DIVISION OF	LIDVEV	OKTO		On Edit No.	170077				
GEOLOGY AND LAND S	URVEY	STATE WELL I		I	REVENUE NO.				
(573) 368-2165 MONITORING WELL		A206240	02/04/2016				012716		
CERTIFICATION RECORD		PH1 PH2	PH3	APPROVED B	Υ		ROUTE		
CERTIFICATION RECORD			01/2016 02/01/2016						
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NTRACTOR OR	DRILLING	CONTRACTOR	<u> </u>					
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUT	OSKY				VARIANCE GRANTED BY DNR		
OWNER ADDRESS 3750 S. LINDBERGH BLVD.	CITY ST LOUIS			STATE MO	ZIP 631:	27	NUMBER		
SITE NAME LABADIE ENERGY CENTER			WELL NUMBER LMW4S			COUNTY FRANKLIN			
SITE ADDRESS 226 LABADIE POWER PLANT RD				CITY LABADIE			STATIC WATER LEVEL 14.89 FT		
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF	DIAMETER AND D		OLE SURFACE COM	MPLETION GROUT	LOCATIO	N OF WELL			
SURFACE COMPLETION	SURFACE COMPL PLACED		$J \cap J$						
X ABOVE GROUND LENGTH 5.0 FT. FLUSH MOUNT DIAMETER 4.0 IN.	DIAMETER 12.0 LENGTH 2.5 FT.	IN.	X CONCRET OTHER	E	LAT. 38 ° 33' 48.65" LONG. 90 ° 49' 50.82"				
TEOGRAMOGIVI BIAMETER <u>4.0</u> IV.	LENOTH <u>2.5</u> 11.		OMER			LLEST	LARGEST		
							1/4 NE 1/4		
LOCKING CAP	<u></u>		SURFACE COMPL	UMINUM PLASTIC	050	40 -			
WEEP HOLE	١r		STEEL X AL	PLASTIC	RANGE		WN. <u>44</u> NORTH Direction E		
	- 11					RING FOR:			
					RADIONI	37	PETROLEUM PRODUCTS ONLY METALS VOC		
	_		RISER		svocs		PESTICIDES/HERBICIDESS		
ELEVATIONFT.			RISER PIPE DIAME		BBOBOO	ED LIGE OF	WELL		
ANNULAR SEAL			RISER PIPE LENGT HOLE DIAMETER			ED USE OF GRATION WELL	X OBSERVATION		
LENGTH0.0FT.			WEIGHT OR SDR#	SCH40	EXTRA	CTION WELL	OPEN HOLE		
SLURRY CHIPS					PIEZON DIRECT				
PELLETS GRANULAR CEMENT/SLURRY	-		MATERIAL STEEL	X THERMOPLASTIC (PVC)	-		FORMATION		
IF CEMENT/BENTONITE MIX:			OTHER	X THERWOPLASTIC (FVC)	FROM	ТО	FORMATION DESCRIPTION		
BAGS OF CEMENT USED:					0.0		STY CLY		
%OF BENTONITE USED:					1.0		SLT CLY		
WATER USED/BAG: GAL.					2.7		GRVL		
			BENTONITE SEAL		3.0		CLY SLT		
			LENGTH: 15.5	ETS GRANULAR	7.7 20.0		SND SND		
			SLURRY	<u></u>					
		-	SATURATED ZONE	HYDRATED					
SECONDARY FILTER PACK LENGTH:1.0FT.	_								
LENGIII			SCREEN						
			SCREEN DIAMETE						
			SCREEN LENGTH: DIAMETER OF DRI						
DEPTH TO TOP OF PRIMARY			DEPTH TO TOP						

TOTAL DEPTH: _33.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x <u>JEFFREY INGRAM</u> 006124 11/18/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____13.7FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMENT OF			REF NO		DATE RECEIVED					
	JRAL RESOURCES		CR NO	0512872	CHE	CK NO.		01/27/20	16	
4 A a=a	SION OF	LIDVEV	SATIS			OK NO.		170077	7	
1507	LOGY AND LAND S	URVEY	STATE WELL NO)			REVENUE	E NO.		
` ,	368-2165			02/04/2016					012716	
MONITORING W CERTIFICATION			ENTERED NRBASSM PH1 PH2 PH3			APPROVED B	Y		ROUTE	
CERTIFICATION	IKECOKD			PH3 /2016 02/01/2016						
INFORMATION SUPI	PLIED BY PRIMARY CON	NTRACTOR OR	DRILLING CO	ONTRACTOR						
OWNER NAME AMEREN MISSOURI C/O BI	ILL KUTOSKY	CONTACT NAME AMEREN MISSOUR	RI C/O BILL KUTO	SKY				VARIANCE GRANTED BY DNR		
OWNER ADDRESS 3750 S. LINDBERGH BLVD.			STA ³	TE	ZIP 6312	27	NUMBER			
SITE NAME LABADIE ENERGY CENTER			WEL	L NUMBER /5S	l		COUNTY FRANKLIN			
SITE ADDRESS 226 LABADIE POWER PLAN			CITY	, ADIE			STATIC WATER LEVEL 10.38 FT			
SURFACE COMPLETION TYPE X ABOVE GROUND FLUSH MOUNT	LENGTH AND DIAMETER OF SURFACE COMPLETION LENGTH 5.0 FT. DIAMETER 4.0 IN.	DIAMETER AND DI SURFACE COMPLI PLACED DIAMETER 12.0 LENGTH 2.5 FT.	ETION WAS	LE SURFACE CO X CONCRET		TION GROUT	LAT	N OF WELL 38 ° 3 90 ° 4	<u>3</u> ' <u>48.74</u> "	
FLOSH MOONT	DIAMETER 4.0 IN.		OTHER				90 4 LEST	LARGEST		
									1/4 NW 1/4	
LOCKING CAP				SURFACE COMPL						
WEEP HOLE		STEEL X ALUMINUM PLASTIC						WN44 NORTH		
		- 11					RANGE	RING FOR:	Direction <u>E</u>	
							RADIONU	CLIDES	PETROLEUM PRODUCTS ONLY	
				RISER			SVOCS	VES X	METALS VOC PESTICIDES/HERBICIDESS	
ELEVATION	FT.		1'1	RISER PIPE DIAME	TER	2.0IN.				
				RISER PIPE LENGT	тн _	<u>13.8</u> FT.		ED USE OF		
ANNULAR SEAL				HOLE DIAMETER				GRATION WELL	X OBSERVATION OPEN HOLE	
LENGTH	<u>).0</u> F1.		++	WEIGHT OR SDR#		SCH40	PIEZOM		OPEN HOLE	
SLURRY CH PELLETS GR		_		MATERIAL			DIRECT	PUSH		
CEMENT/SLURRY	RANULAR			STEEL	X THEF	RMOPLASTIC (PVC)	DEF	TH	FORMATION	
IF CEMENT/BENTO	NITE MIX:			OTHER			FROM	ТО	DESCRIPTION	
BAGS OF CEMENT	USED:						0.0	2.7	STY CLY	
%OF BENTONITE U	SED:						2.7	6.0	SLT	
WATER USED/BAG:	GAL.						6.0		SDY SLT	
				BENTONITE SEAL			11.5		SLT SND SND	
				LENGTH: 5.5	LETS	GRANULAR	13.5	25.0	SIND	
				SLURRY						
				SATURATED ZONE		HYDRATED				
SECONDARY FILTE		_								
LENGTH:	<u>u.5</u> F1.			SCREEN						
				SCREEN DIAMETE						
			SCREEN LENGTH: 9.8FT.							
DEPTH TO TOP OF	DIAMETER OF DRILL HOLE: <u>6.0</u> IN. DEPTH TO TOP <u>15.2</u> FT.									
FILTER PACK:				<u>v.c</u> 1 1.						

TOTAL DEPTH: 25.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x <u>JEFFREY INGRAM</u> 006124 11/18/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: <u>12.5</u>FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMEN	_	REF NO		DATE RECEIVED				
NATURAL RESOURCES	;)512873	OLIFOK NO		01/27/20	16	
DIVISION OF		CR NO		CHECK NO.		170077	•	
🛮 🕰 🛞 🛮 GEOLOGY AND LAND S	SURVEY	STATE WELL NO			REVENUE NO.			
(573) 368-2165		A206242 0		012716				
MONITORING WELL		ENTERED NRBA		APPROVED BY			ROUTE	
CERTIFICATION RECORD		PH1 PH2 02/01/2016 02/01	PH3					
INFORMATION CUIDDUIFD BY DDIMARY COL	UTD A CTOD OD							
INFORMATION SUPPLIED BY PRIMARY COINOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	VIRACIOR OR	DRILLING CC	INTRACTOR					
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOUI	RI C/O BILL KUTOS	SKY				VARIANCE GRANTED BY DNR	
OWNER ADDRESS 3750 S. LINDBERGH BLVD.			STATE MO	ZIP 6312	27	NUMBER		
SITE NAME LABADIE ENERGY CENTER			WELL NUMBER LMW6S			COUNTY FRANKLIN		
SITE ADDRESS 226 LABADIE POWER PLANT RD			CITY LABADIE			STATIC WATER LEVEL 10.49 FT		
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND DI		E SURFACE COM	IPLETION GROUT	LOCATIO	N OF WELL	-	
X ABOVE GROUND LENGTH 5.0 FT.	PLACED DIAMETER 12.0	IN.	CONCRETE		LAT.	38° 3	3' 40.03"	
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH 2.5 FT.		OTHER		LONG.			
					SMAL	LEST	LARGEST	
LOCKING CAP			SURFACE COMPLE	ETTION		1/4	1/4NW 1/4	
WEEP HOLE	-			UMINUM PLASTIC	SEC	17 T	WN44 NORTH	
WEEL FIGEE	Ir	\neg			RANGE		Direction E	
	- 11				MONITOR	RING FOR:		
					RADIONU EXPLOSI		PETROLEUM PRODUCTS ONLY METALS VOC	
	_		RISER		svocs		PESTICIDES/HERBICIDESS	
ELEVATIONFT.			RISER PIPE DIAMET	'				
ANNULAR SEAL			RISER PIPE LENGTH HOLE DIAMETER			ED USE OF GRATION WELL	WELL X OBSERVATION	
LENGTH0.0FT.			WEIGHT OR SDR#			CTION WELL	OPEN HOLE	
					PIEZOM			
SLURRY CHIPS PELLETS GRANULAR	_		MATERIAL		DIRECT	PUSH		
L CEMENT/SLURRY IF CEMENT/BENTONITE MIX:			STEEL	THERMOPLASTIC (PVC)	DEF	PTH	FORMATION	
			OTHER		FROM	ТО	DESCRIPTION	
BAGS OF CEMENT USED:			L_		0.0	4.0	STY CLY	
%OF BENTONITE USED:					4.0		SLY SLT	
WATER USED/BAG: GAL.			BENTONITE SEAL		5.0 8.2		STY SND SLY SLT	
			LENGTH:5.5		10.0		SND	
			CHIPS PELLE	GRANULAR GRANULAR	21.7	25.0	SND	
			SLURRY SATURATED ZONE	HYDRATED				
SECONDARY FILTER PACK			SATURATED ZONE	III HTUKATED				
LENGTH:1.0FT.	-							
			SCREEN	D. 0.0111				
	F		SCREEN DIAMETE SCREEN LENGTH:					
DEPTH TO TOP OF PRIMARY	_	DIAMETER OF DRII						
FILTER PACK:11.2FT.		DEPTH TO TOP	<u>15.2</u> FT.					

TOTAL DEPTH: 25.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x <u>JEFFREY INGRAM</u> 006124 11/20/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____13.8FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMENT OF			REF NO DATE RECEIVED			0.1/07/0040			
	URAL RESOURCES		CR NO	00512874	CHECK NO.		01/27/20	16	
4 A a=a	SION OF	UDVEV				170077			
	LOGY AND LAND S) 368-2165	URVEY	STATE WELL N			REVENU			
MONITORING W	,		A206243 ENTERED NRE	02/04/2016	APPROVED B	012716		012716 ROUTE	
CERTIFICATION			PH1 PH2	PH3	APPROVED B	NO INGO		ROUTE	
02.00.000	. KLOOKS			01/2016 02/01/2016					
INFORMATION SUP	PLIED BY PRIMARY COI	NTRACTOR OR	R DRILLING C	ONTRACTOR					
OWNER NAME AMEREN MISSOURI C/O B	ILL KUTOSKY	CONTACT NAME AMEREN MISSOU	IRI C/O BILL KUTO	DSKY				VARIANCE GRANTED BY DNR	
OWNER ADDRESS CITY ST LOUIS					STATE MO	ZIP 631:	27	NUMBER	
SITE NAME LABADIE ENERGY CENTER					WELL NUMBER LMW7S			COUNTY FRANKLIN	
SITE ADDRESS 226 LABADIE POWER PLA	NT RD				CITY LABADIE			STATIC WATER LEVEL 8.57 FT	
SURFACE COMPLETION TYPE	LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D SURFACE COMPL PLACED		DLE SURFACE COI	MPLETION GROUT	LOCATIO	N OF WELL	-	
X ABOVE GROUND	LENGTH <u>5.0</u> FT.	IN.	X CONCRET	LAT	<u>3</u> ' <u>30.25</u> "				
FLUSH MOUNT		OTHER			<u>90</u> ° <u>4</u>				
				_			LLEST	LARGEST 1/4 SW 1/4	
LOCKING CAP				_ SURFACE COMPL	ETTION		1/4	1/4 3W 1/4	
WEEP HOLE			STEEL X A	LUMINUM PLASTIC	SEC	<u>17</u> T	WN. <u>44</u> NORTH		
		- 11		_		RANGE	2 RING FOR:	Direction <u>E</u>	
				_		RADIONI	JCLIDES	PETROLEUM PRODUCTS ONLY	
						EXPLOSI SVOCS	IVES X	METALS VOC PESTICIDES/HERBICIDESS	
ELEVATION	FT.			1	TER2.0IN.				
				RISER PIPE LENGT			ED USE OF		
ANNULAR SEAL LENGTH	n net			HOLE DIAMETER WEIGHT OR SDR#			GRATION WELL CTION WELL	X OBSERVATION OPEN HOLE	
LENGIH	<u>u.u</u> F1.		++	WEIGHT OK 3DK#	<u>30H40</u>		METERS		
	HIPS RANULAR			MATERIAL		DIRECT	T PUSH		
CEMENT/SLURRY				STEEL	X THERMOPLASTIC (PVC)	DEI	PTH	FORMATION	
IF CEMENT/BENTO	NIIE MIX:			OTHER		FROM	TO	DESCRIPTION	
BAGS OF CEMENT	USED:			L		0.0	5.0	STY CLY	
%OF BENTONITE U WATER USED/BAG:						5.0	-	STY CLY	
WATER USED/BAG	GAL.	L L		BENTONITE SEAL		7.5 22.0		SND SND	
				LENGTH:7.5					
				CHIPS PELL	ETS GRANULAR				
				SATURATED ZONE	HYDRATED				
SECONDARY FILTE	ER PACK			_	_				
LENGTH:	<u>0.1</u> FT.	7 1 1		SCREEN					
			SCREEN SCREEN DIAMETER: 2.0IN.						
				SCREEN LENGTH					
DEPTH TO TOP OF		DIAMETER OF DR							
FILTER PACK: 12.0FT.				DEPTH TO TOP _	<u>15.2</u> FT.		1		

TOTAL DEPTH: _25.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x <u>JEFFREY INGRAM</u> 006124 11/20/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____13.0FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMENT OF						TE RECEIVED					
	JRAL RESOURCES			00512875	OUE	OKNO	01/27/2016 CK NO.				
	SION OF					170077					
	LOGY AND LAND S	URVEY					REVENU		<u>'</u>		
	368-2165		A206244	02/04/2016					012716		
MONITORING W			ENTERED NRBASSM APPR			APPROVED BY RO			ROUTE		
CERTIFICATION	RECORD		PH1 PH2	PH3							
				1/2016 02/01/2016							
NOTE: THIS FORM IS NOT TO BE USED	PLIED BY PRIMARY CON FOR NESTED WELLS	NTRACTOR OR	DRILLING C	ONTRACTOR							
OWNER NAME AMEREN MISSOURI C/O BI	ILL KUTOSKY	RI C/O BILL KUTO	OSKY				VARIANCE GRANTED BY DNR				
OWNER ADDRESS 3750 S. LINDBERGH BLVD.			STA MO	TE	ZIP 6312	27	NUMBER				
SITE NAME LABADIE ENERGY CENTER			WEL	L NUMBER V8S			COUNTY FRANKLIN				
SITE ADDRESS 226 LABADIE POWER PLAN	NT RD			CITY	/ ADIE			STATIC WATER LEVEL 7.1 FT			
SURFACE COMPLETION TYPE X ABOVE GROUND	LENGTH AND DIAMETER OF SURFACE COMPLETION LENGTH _5.0 FT.	DIAMETER AND DI SURFACE COMPLI PLACED DIAMETER 12.0 LENGTH 2.5 FT.	ETION WAS	X CONCRE		TION GROUT	LAT	<u>38</u> ° <u>3</u>	<u>13' 20.76</u> "		
FLUSH MOUNT	DIAMETER <u>4.0</u> IN.		OTHER				90°				
								LLEST	LARGEST 1/4 SW 1/4		
LOCKING CAP				_ SURFACE COMPI	LETTIC	ON	_	1/4	1/4 5W 1/4		
WEEP HOLE		<u> </u>		STEEL X	ALUMINUN	PLASTIC	SEC	<u>17</u> T	ΓWN. <u>44</u> NORTH		
		IF					RANGE	2	Direction <u>E</u>		
		- 11						RING FOR:	1		
				-			RADIONU EXPLOSI		PETROLEUM PRODUCTS ONLY METALS VOC		
		_		RISER			svocs	L	PESTICIDES/HERBICIDESS		
ELEVATION	FT.			RISER PIPE DIAME							
ANNULAR SEAL				RISER PIPE LENGTHOLE DIAMETER				GRATION WELL			
LENGTH) ()FT			WEIGHT OR SDR#				CTION WELL	OPEN HOLE		
				1		<u> </u>		METERS			
SLURRY CH PELLETS GR	IIPS RANULAR	_		MATERIAL			DIRECT	PUSH			
CEMENT/SLURRY				STEEL	X THE	RMOPLASTIC (PVC)	DEF	PTH	FORMATION		
IF CEMENT/BENTOI	NITE MIX:			OTHER			FROM	TO	DESCRIPTION		
BAGS OF CEMENT	USED:			L			0.0	4.6	STY CLY		
%OF BENTONITE U	SED:						4.6		SND		
WATER USED/BAG:	GAL.						10.0		STY SND		
				BENTONITE SEAL			13.0	23.0	SND		
				LENGTH: 6.5		GRANULAR		ı			
				SLURRY				ı			
				SATURATED ZONE		HYDRATED					
SECONDARY FILTE											
LENGTH:	<u>1.0</u> FT.	7 11		SCREEN							
				SCREEN DIAMET	ER:_	2.0IN.					
				SCREEN LENGTH				ı			
DEPTH TO TOP OF		DIAMETER OF DR									
FILTER PACK:	DEPTH TO TOP13.2FT.										
		1 (0000000)	A BOOOD TOOL	1							

TOTAL DEPTH: 23.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x <u>JEFFREY INGRAM</u> 006124 11/20/2015 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____13.2FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMEN	_				TE RECEIVED			
NATURAL RESOURCES	;		0304710			03/14/20	016	
DIVISION OF		CR NO		CHECK NO.		17008	13	
🛮 🧸 🛞 🛮 GEOLOGY AND LAND S	SURVEY	STATE WELL NO		REVENUE NO.				
(573) 368-2165		A206410 03/15/2016					031416	
MONITORING WELL		ENTERED NRBA	SSM	APPROVED B	Y	ROUTE		
CERTIFICATION RECORD		PH1 PH2 PH3 03/14/2016 03/15/2016 03/15/2016						
INFORMATION SUPPLIED BY PRIMARY COINDIE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	VIRACTOR OR	DRILLING CC	NIRACIOR					
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	CONTACT NAME AMEREN MISSOU	RI C/O BILL KUTOS	SKY			VARIANCE GRANTED BY DNR		
OWNER ADDRESS 3750 S LINDEBERGH BLVD			STATE MO	ZIP 6312	NUMBER			
SITE NAME LABADIE ENERGY CNETER			WELL NUMBER BMW1S	J.		COUNTY ST LOUIS CITY		
SITE ADDRESS BOLES RD			CITY ST LOUIS			STATIC WATER LEVEL 13.6 FT		
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION	DIAMETER AND D SURFACE COMPL PLACED		E SURFACE COM	MPLETION GROUT	LOCATIO	N OF WEL	L	
X ABOVE GROUND LENGTH <u>5.0</u> FT.	IN.	X CONCRETI	E	LAT.	38°;	32' _50.0"		
FLUSH MOUNT DIAMETER 4.0 IN.	LENGTH <u>2.5</u> FT.		OTHER		LONG	90°	52' _2.68"	
						LEST	LARGEST	
LOCKING CAP			SURFACE COMPLI	ETTION		1/4	1/4 1/4	
WEEP HOLE	Υ		STEEL X AL	UMINUM PLASTIC	SEC. LO	3002577	TWN NORTH	
	IF				RANGE		Direction <u>E</u>	
						RING FOR	7	
			_		RADIONU EXPLOSI		PETROLEUM PRODUCTS ONLY METALS VOC	
	_		RISER		svocs		PESTICIDES/HERBICIDESS	
ELEVATIONFT.			RISER PIPE DIAMET	· · · · · · · · · · · · · · · · · · ·				
ANNULAR SEAL			RISER PIPE LENGTI HOLE DIAMETER			ED USE O GRATION WELL		
LENGTH0.0FT.			WEIGHT OR SDR#			CTION WELL	OPEN HOLE	
п					PIEZON			
SLURRY CHIPS PELLETS GRANULAR	_		MATERIAL	_	DIRECT	PUSH		
CEMENT/SLURRY IF CEMENT/BENTONITE MIX:			STEEL	THERMOPLASTIC (PVC)	DEF	PTH	FORMATION	
			OTHER		FROM	ТО	DESCRIPTION	
BAGS OF CEMENT USED:					0.0	6.5	CLY SLT	
%OF BENTONITE USED:					6.5	9.3	STY CLY	
WATER USED/BAG: GAL.			BENTONITE SEAL		9.3 10.0	10.0 17.6	SND STY SND	
			LENGTH:14.0		17.6	18.6	STY CLY	
			CHIPS PELLE	GRANULAR GRANULAR	18.6	31.0	SND	
			SLURRY					
OF COMPANY FILTER DACK	Г		SATURATED ZONE	HYDRATED				
SECONDARY FILTER PACK LENGTH:1.0FT.	-							
			SCREEN					
	-		SCREEN DIAMETER: 2.0IN.					
DEDTH TO TOD OF DETHACK			SCREEN LENGTH:9.8FTDIAMETER OF DRILL HOLE: _6.0IN.					
DEPTH TO TOP OF PRIMARY FILTER PACK:17.8FT.		DEPTH TO TOP						

TOTAL DEPTH: _31.0 FEET FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED. SIGNATURE (PRIMARY COUNTRACTOR) PERMIT NUMBER DATE WELL DRILLING WAS COMPLETED x <u>JEFFREY INGRAM</u> 006124 02/01/2016 I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS PUMP INSTALLED SIGNATURE (WELL DRILLER) × JASON DRABEK PERMIT NUMBER SIGNATURE (APPRENTICE) APPRENTICE PERMIT NUMBER 004484

LENGTH OF PRIMARY FILTER

PACK: _____13.2FT.

SCREEN MATERIAL

OTHER

MISSOURI DEPARTMEN	-	REF NO		DATE RECEIVED					
NATURAL RESOURCES		CR NO	00304712	CHE	CK NO.		03/14/20	016	
DIVISION OF	LIDVEV				170083				
GEOLOGY AND LAND S	URVEY	STATE WELI	L NO		REVENUE NO.				
(573) 368-2165		A206412 03/15/2016					031416		
MONITORING WELL CERTIFICATION RECORD		ENTERED NRBASSM			APPROVED BY			ROUTE	
CERTIFICATION RECORD		PH1 PH2 PH3 03/14/2016 03/15/2016 03/15/2016							
INFORMATION SUPPLIED BY PRIMARY CONNOTE: THIS FORM IS NOT TO BE USED FOR NESTED WELLS	NTRACTOR OR	DRILLING	CONTRACTOR						
OWNER NAME AMEREN MISSOURI C/O BILL KUTOSKY	ME OURI C/O BILL KUTOSKY				VARIANCE O				
OWNER ADDRESS 3750 S LINDEBERGH BLVD	CITY ST LOUIS			STATE ZIP 63127		NUMBER			
SITE NAME LABADIE ENERGY CNETER			WEL	L NUMBER V2S	L		COUNTY ST LOUIS CITY		
SITE ADDRESS BOLES RD			CITY ST L	, OUIS			STATIC WATER LEVEL 14.3 FT		
SURFACE COMPLETION TYPE LENGTH AND DIAMETER OF SURFACE COMPLETION X ABOVE GROUND LENGTH 5.0 FT. DIAMETER 4.0 IN.	DIAMETER AND DE SURFACE COMPLI PLACED DIAMETER 12.0 LENGTH 2.5 FT.	ETION WAS	SURFACE COI X CONCRET OTHER		ION GROUT	LAT LONG SMA	38 °3 90 °	32' <u>39.4</u> " 5 <u>2' 2.97</u> " LARGEST	
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						EXPLOS	Ľ	PETROLEUM PRODUCTS ONLY METALS VOC	
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ELEVATIONFT.			RISER PIPE DIAME						
ANNULAR SEAL			RISER PIPE LENGT HOLE DIAMETER				SED USE O		
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SLURRY CHIPS						PIEZON DIREC*	METERS		
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%OF BENTONITE USED:						0.0 4.0	4.0 30.0	CLY SLT SND	
WATER USED/BAG: GAL.						4.0	00.0	OND	
			BENTONITE SEAL						
			LENGTH: 12.5	ETS	GRANULAR				
			SLURRY		OKANOLAK				
			SATURATED ZONE		HYDRATED				
SECONDARY FILTER PACK	_								
LENGTH: <u>0.5</u> FT.			SCREEN						
			SCREEN DIAMETE						
		SCREEN LENGTH: 9.8FT.							
DEPTH TO TOP OF PRIMARY			DIAMETER OF DRI						
FILTER PACK: <u>17.4</u> FT.			22 10 101 _						

SCREEN MATERIAL

SIGNATURE (APPRENTICE)

OTHER

FOR CASED WELLS, SUBMIT ADDITIONAL AS BUILT DIAGRAMS SHOWING WELL CONSTRUCTION DETAILS INCLUDING TYPE AND SIZE OF ALL CASING, HOLE DIAMETER AND GROUT USED.

PERMIT NUMBER

PERMIT NUMBER 004484

006124

I HEREBY CERTIFY THAT THE MONITORING WELL HEREIN DESCRIBED WAS CONSTRUCTED IN ACCORDANCE WITH MISSOURI DEPARTMENT OF NATURAL RESOURCES REQUIREMENTS FOR THE CONSTRUCTION OF MONITORING WELLS

LENGTH OF PRIMARY FILTER

PACK: <u>12.6</u>FT.

SIGNATURE (PRIMARY COUNTRACTOR)

x <u>JEFFREY INGRAM</u>

SIGNATURE (WELL DRILLER) × JASON DRABEK X THERMOPLASTIC (PVC)

TOTAL DEPTH:

02/02/2016

PUMP INSTALLED

DATE WELL DRILLING WAS COMPLETED

APPRENTICE PERMIT NUMBER

_30.0 FEET

APPENDIX H STATISTICAL ANALYSIS PLAN





STATISTICAL ANALYSIS PLAN

Prepared in accordance with the United States Environmental Protection Agencies Coal Combustion Rule, part 40 CFR 257.93 for Ameren Missouri's LCPB Surface Impoundment at the Labadie Energy Center, Franklin County, Missouri



Submitted To: Ameren Missouri

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Date: October 10, 2017

Project No.153-1406





EXECUTIVE SUMMARY

This Statistical Analysis Plan (SAP) was developed to meet the requirements of United States Environmental Protection Agency (USEPA) 40 CFR Part 257 "Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities; Final Rule" (the Rule or CCR Rule). The Rule requires owners or operators of an existing Coal Combustion Residuals (CCR) Surface Impoundment to install a groundwater monitoring system and develop a sampling and analysis program (§§ 257.90 - 257.94). Ameren Missouri has determined that the LCPB (Fly Ash) Surface Impoundment at the Labadie Energy Center in Franklin County, Missouri is subject to the requirements of the CCR Rule.

As a part of the groundwater sampling and analysis requirements of the Rule, statistical methods as described in Section §257.93(f) of the Rule need to be implemented to statistically evaluate groundwater quality. The selected statistical method must then be certified by a qualified professional engineer stating that the statistical method is appropriate for evaluating the groundwater monitoring data for the CCR Unit. Detailed descriptions of the acceptable statistical data methods are provided in the USEPA's *Statistical Analysis of Groundwater Data at RCRA Facilities, Unified Guidance* (USEPA, 2009) (Unified Guidance). The Unified Guidance is also recommended in the CCR Rule to be used for guidance in the selection of the appropriate statistical evaluation method.

This SAP details the statistical procedures to be used to establish background conditions, to implement detection monitoring, and to implement assessment monitoring (if needed) for Ameren Missouri at the above mentioned CCR Unit. Detailed information on collection, sampling techniques, preservation, etc. are provided in the Groundwater Monitoring Plan (GMP) for the CCR Unit specified above. This SAP is a companion documents to the GMP and assumes that data analyzed by the procedures described in this SAP are from samples that were collected in accordance with the GMP.

This SAP was prepared by Golder Associates, Inc. (Golder) on behalf of Ameren in order to document appropriate method of groundwater data evaluation in compliance with CCR Rules. The methods and groundwater data evaluation techniques used in this SAP are appropriate for evaluation of the groundwater monitoring data for the above mentioned CCR Unit and are in compliance with performance standards outlined in Section §257.93(g) of the CCR Rule.



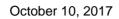


Table of Contents

EXECUTIVE SUMMARY	ES-1
1.0 BASELINE STATISTICS	1
1.1 STATISTICAL DATA PREPARATION AND INITIAL REVIEW	1
1.1.1 Physical and Statistical Independence of Groundwater Samples	1
1.1.2 Data Review – Testing For Outliers	2
1.1.2.1 Time Series Plots	2
1.1.2.2 Dixon's and Rosner's Tests	3
1.2 Upgradient Monitoring Wells	3
1.2.1 Calculate for Mean and Standard Deviation	3
1.2.1.1 Reporting of Low and Zero Values	4
1.2.2 Data Distribution	4
1.2.3 Temporal Trend	5
1.2.4 Comparing Background Datasets (Spatial Variation)	6
1.3 Compliance Monitoring Wells and Statistically Significant Increases	6
1.3.1 Interwell vs Intrawell Statistical Analysis	7
1.3.1.1 Interwell Statistical Analysis	7
1.3.1.2 Intrawell Statistical Analysis	7
1.3.2 Statistical Power	7
1.3.2.1 Site-Wide False Positive Rate	8
1.3.2.2 Verification Sampling	8
1.3.3 Statistical Evaluation Methods	9
1.3.4 Prediction Intervals	9
1.3.5 Double Quantification Rule	10
1.4 Responding to SSIs	10
1.5 Updating Background Values	10
2.0 ASSESSMENT MONITORING STATISTICAL EVALUATION	12
2.1 Establishing a Ground Water Protection Standard (GWPS)	12
2.1.1 Maximum Contaminant Level (MCL) Based GWPS	13
2.1.2 Non-MCL Based GWPS	15
2.1.2.1 Tolerance Interval Approach	15
2.1.2.2 Prediction Interval Approach	16
2.2 Returning to Background Detection Monitoring	16
2.3 Response to a SSL	17
2.4 Updating Background Values	17
RO REFERENCES	18

i





ii

List of Tables

Table 1

Physical Independence Confidence Interval Method Selection Table 2



1.0 BASELINE STATISTICS

This section discusses the procedures, methods, and processes that will be implemented as part of the Detection Monitoring statistical evaluation. Detection Monitoring will begin after eight rounds of sampling are completed at each monitoring well for each of the Appendix III and Appendix IV parameters. This background monitoring period provides baseline data for each monitoring well which can be used as the basis of the statistical evaluation. Detection monitoring will be completed on a semiannual basis unless adequate groundwater flow is not available for semiannual sampling and proper documentation as outlined in §257.94(d) is completed. Detection monitoring will analyze for Appendix III analytes as outlined in the Groundwater Monitoring Plan for this CCR Unit.

1

1.1 STATISTICAL DATA PREPARATION AND INITIAL REVIEW

Many of the statistical comparison tests used in detection, and assessment monitoring require various analyses to be completed prior to the data being used for the calculation of statistical limits. This section discusses the methods and procedures for completing this initial review of the data. The analyses required include testing for statistical independence, physical independence, and procedures to evaluate potential outliers.

1.1.1 Physical and Statistical Independence of Groundwater Samples

Detection, and Assessment Monitoring statistical evaluations assume that background and downgradient sampling results are statistically independent. The Unified Guidance states that "Physical independence of samples does not guarantee statistical independence, but it increases the likelihood of statistical independence." (Section 14.1, Unified Guidance). Physical independence is most likely achieved when consecutive groundwater samples are collected from independent volumes of water within a given aquifer zone. Using the Darcy Equation, minimum time intervals between sampling events can be calculated in order to confirm the minimum time interval for groundwater to travel through the borehole is less than the time between sampling events (**Table 1, Physical Independence**). This minimum time can be calculated as displayed in Section 14.3.2 of the Unified Guidance.



	Hydraulic	Average Hydraulic			
Well ID	Conductivity	Gradient	Effective Porosity	Well Bore Volume	Minimum Time
Symbol	K	1	n	D	T_{min}
Units	Feet/Day	Feet/Foot	%	Feet	Days
LMW-1S	97.32	0.00042	0.35	0.5	4.3
LMW-2S	30.78	0.00042	0.35	0.5	13.5
LMW-3S	37.44	0.00042	0.35	0.5	11.1
LMW-4S	75.75	0.00042	0.35	0.5	5.5
LMW-5S	56.15	0.00042	0.35	0.5	7.4
LMW-6S	56.15	0.00042	0.35	0.5	7.4
LMW-7S	40.95	0.00042	0.35	0.5	10.2
LMW-8S	56.15	0.00042	0.35	0.5	7.4
BMW-1S	127.68	0.00042	0.35	0.5	3.3
BMW-2S	112.31	0.00042	0.35	0.5	3.7

Table 1: Physical Independence

2

Notes:

- Average hydraulic gradient and effective porosity taken from table 2 in the Groundwater Monitoring Plan (GMP)
- 2. Hydraulic Conductivity taken from table 3 of the Groundwater Monitoring Plan (GMP)
- 3. Calculation completed using the Darcy Equation as outlined in section 14.3.2 of the Unified Guidance.

1.1.2 Data Review – Testing For Outliers

Careful review of the data is critical for verifying that there is an accurate representation of the groundwater conditions. Early identification of anomalous data (outliers) helps play a key role in a successful SAP. Possible causes for outliers include:

- Sampling error or field contamination;
- Analytical errors or laboratory contamination;
- Recording or transcription errors;
- Faulty sample preparation, preservation, or shelf-life exceedance; or
- Extreme, but accurately detected environmental conditions (e.g., spills, migration from the facility).

The following sections outline a few graphical and statistical tests that should be completed prior to the data being used to calculate statistical limits.

1.1.2.1 Time Series Plots

Time Series plots are a quick and simple method to check for possible outliers. Time series plots should be generated with the concentration of the analyte on the Y-axis and the sample date (time) on the X-axis. If any data points look to be potential outliers, the data should be flagged and further evaluated as described in Section 1.1.2.2 below.



1.1.2.2 Dixon's and Rosner's Tests

If graphical methods demonstrate that potential outliers exist, further investigation of these data points can be completed using Dixon's test for datasets with fewer than 25 samples and Rosner's test with datasets greater than 20 samples. Formal testing should only be performed if an observation seems particularly high compared to the rest of the dataset. If statistical testing is to be completed to whether an outlier exists, it should be cautioned that these outlier tests assume that the rest of the data (other than the outlier) are normally distributed. Additionally, because log-normally distributed data often contain one or more values that appear high relative to the rest, it is recommended that the outlier test be run on the transformed values instead of their original observations. This way, one can avoid classifying a high log-normal measurement as an outlier just because the test assumptions were violated. Most groundwater statistical packages can complete Dixon's and Rosner's tests and more information about Dixon's and Rosner's tests is provided in Sections 12.3 and 12.4 of the Unified Guidance. If the test designates an observation as a statistical outlier, the source of the abnormal measurement should be investigated. In general, if a data point is found to be a statistical outlier, it should not be used for statistical evaluation. However, outlier removal should be performed carefully, and typically only when a specific cause for the outlier can be identified.

3

In some cases where a specific cause for an outlier cannot be identified, professional judgment can be used to determine whether the outlier significantly affects the statistical results to the extent that removal is deemed necessary. If an outlier value with much higher concentration than other background observations is not removed from background prior to statistical testing, it will tend to increase both the background sample mean and standard deviation. In turn, this may substantially raise the magnitude of the prediction limit or control limit calculated from that data set. Thus, experience shows that it is a good practice to remove obvious outliers from the database even when independent evidence of the source of the outlier does not exist. The removal of outliers tends to normalize the data and therefore produce a more robust statistical limit. Outlier removal also tends to produces a more conservative statistical limit, since the data variability is decreased, thereby decreasing the standard deviation.

1.2 Upgradient Monitoring Wells

Following the identification and removal of outliers, the upgradient data are further reviewed to determine appropriate methods for statistical evaluation to maintain adequate statistical power while minimizing the chance of false positives. The following sections describe the procedures and methods that should be used, based on the background dataset, to compare the background datasets, to calculate the data distribution, to handle non-detect (ND) data, and to select appropriate statistical evaluation methods (interwell vs intrawell).

1.2.1 Calculate for Mean and Standard Deviation

Following outlier removal, initial summary statistics including mean and standard deviation should be calculated for the background monitoring well datasets. While these summary statistics are easily



completed in many groundwater statistical software packages, it is important to account for values that have low or zero values as described below.

4

1.2.1.1 Reporting of Low and Zero Values

1.2.1.1.1 Estimated Values (J Flag)

Estimated values are values that have a concentration between the method detection limit (MDL¹) and the practical quantitation limit (PQL²) for any given compound. These values are typically displayed with a J flag in laboratory report packages and are often referred to as "J-values". In most cases, The Unified Guidance recommends using the estimated value provided for statistical evaluation. Estimated values are typically used because the accuracy and power of most statistical evaluations lose power as the percentage of non-detects increases. While they are below the PQL, estimated values are considered detectable concentrations for statistical calculations, which has the effect of lowering the percentage of non-detects.

This "rule" should be applied with care, as there is an exception. Estimated values are not considered detectable concentrations if all values for a single constituent are less than the PQL. This is discussed in more detail in Section 1.3.5 of this document.

1.2.1.1.2 Non-Detects Values (ND)

Non-Detect Values (ND) are concentrations that were not detected at a concentration above the MDL. ND values are typically displayed with a "U" or "ND" flag in laboratory data report packages. The following approaches for managing ND values are based on recommendations in the Unified Guidance and are applicable for use with the statistical evaluation procedures that will be further discussed and used in this SAP (prediction intervals, confidence intervals, and tolerance intervals):

- If <15% ND, substitute ½ the PQL;
- If between 15% to 50% ND, use the Kaplan-Meier or robust regression on ordered statistics to estimate the mean and standard deviation;
- If >50% but less than 100% ND, use a non-parametric test; or
- If 100% of values are less than the PQL, use the Double Quantification Rule.

1.2.2 Data Distribution

Statistical evaluations of groundwater data require an understanding of the data distribution for each analyte in each monitoring well. Data typically fall into one of the following distributions:

² PQL = minimum concentration of an analyte (substance) that can be measured with a high degree of confidence that the analyte is present at or above that concentration (typically 5-10x higher than the MDL).



¹ MDL = lowest level of an analyte (substance) that the laboratory can reliably detect with calibrated instrumentation; generally based on results of an annual "MDL study" performed in accordance with 40 CFR Part 136, Appendix B; MDLs are generally set using laboratory grade deionized water spiked with a known concentration and thus do not account for effects of matrix interference inherent in typical groundwaters.



- Normal distribution Sometimes referred to as Gaussian distribution, a normal distribution is a common continuous distribution where data form a symmetrical bellshaped curve around a mean. Normally distributed data are tested using parametric methods.
- Transformed-normal distribution Similar to a normal distribution, however, data are asymmetrical until transformation is applied to all data which then causes it to form a bell-curve. Transformed-normal data distributions are also tested use parametric methods.
- Non-Normal Distribution When the data are not or cannot be transformed into a symmetrical distribution. Non-normal data distributions are tested using Nonparametric methods.

Testing for data distributions can be completed in several different ways including the skewness coefficient, probability plots with Filliben's test, or the Shapiro-Wilk/Shapiro-Francia Test. All of these methods may be employed, however, the Shapiro-Wilk and Shapiro-Francia tests are generally considered the best method according to the Unified Guidance. The Shapiro-Wilk test is best for sample sizes under 50 while the Shapiro-Francia test is best with larger datasets of 50 or more observations. Most groundwater statistical software packages can complete both Shapiro-Wilk and Shapiro-Francia tests and a detailed discussion of the testing procedures is provided in Section 10.5.1 of the Unified Guidance.

Based on the outcome of the data distribution testing, data will use either Parametric or Non-parametric tests. It is important to note that non-parametric testing usually requires larger datasets in order to minimize the Site Wide False Positive Rate (SWFPR) therefore when the raw data are not normally distributed, a transformed-normal distribution is preferred when possible.

1.2.3 Temporal Trend

Most statistical tests assume that the sample data are statistically independent and identically distributed. Therefore, samples collected over a period of time should not exhibit a time dependence. A time dependence could include the presence of trends or cyclical patterns when observations are graphed on a time series plot. Trend analysis methodologies test to see whether the dataset displays an increasing, decreasing, or seasonal trend. A statistically significant increasing or decreasing trend could indicate a release from the CCR unit (or alternative source) and further investigation of the cause of the trend may be necessary.

If a trend is suspected, a Theil-Sen trend line should be used to estimate slope and the Mann-Kendall Trend Test should be used to evaluate the slope significance (Chapter 14, Unified Guidance). If a statistically significant trend is reported, based on a Sen's slope/Mann-Kendall trend test, the source of the trend should be investigated. If the trend can be shown to be a result of an upgradient or off-site source, the data can be de-trended and used to calculated statistical limits. De-trending can be accomplished by computing a linear regression on the data (see Section 17.3.1 of the Unified Guidance) and then using the regression residuals instead of the original measurements in subsequent statistical analysis.



1.2.4 Comparing Background Datasets (Spatial Variation)

After physical independence, outlier, trend, and summary statistical testing is completed, the datasets from the background monitoring wells should be compared to one another for each individual constituent. The comparison of these background datasets is useful for determining whether spatial variability exists in the background dataset, and can also be used to decide whether an interwell or intrawell approach is more appropriate for statistical evaluation.

6

Box and whisker plots can be used to perform side by side comparison for each well and can be completed for each individual analyte to determine if the variance is equal across the background datasets. If the box plots appear to be staggered and do not appear to be from the same population (same variance) then a Lavene's test using an α of 0.01 should be used as a check to determine if the background datasets have spatial variation. Testing methods and procedures are provided in Section 11.2 of the Unified Guidance.

The preferred method for comparing background datasets is a Mann-Whitney (or Wilcoxon Rank Sum) Test, which evaluates the ranked medians of both the historical and new dataset populations. An α of 0.05 should be used for this evaluation. After calculation, if the Mann-Whitney statistic does not exceed the critical point, the test assumes that the two data populations have equal medians, and therefore are likely from the same statistical distribution. The testing methods and procedures for this analysis are provided in Section 16.2 of the Unified Guidance.

If spatial variability is identified within the background dataset, an additional investigation may be needed in order to confirm that the variability is not caused by impacts from the CCR unit. If there is spatial variability and it is not caused by impacts from the CCR unit, then an intrawell approach to statistical evaluation may be appropriate.

1.3 Compliance Monitoring Wells and Statistically Significant Increases

After completing the previously described analyses of the background data, a statistical evaluation of the compliance monitoring data should be completed to determine if there are any Statistically Significant Increases³ (SSIs) that could trigger assessment monitoring. Section §257.93(F) of the CCR Rule specifies the list of methods that can be used for statistical evaluation. These specific methods to be used for statistical evaluation of data from the RMSGS are detailed below. Further, the Unified Guidance is recommended in the CCR Rule to be used for guidance in the selection of the appropriate statistical evaluation method. This section provides a guide to choosing the correct statistical evaluation to analyze the compliance wells for SSIs, the basic principles of each method, and response activities for identified SSIs.

³ SSI = a verified statistical exceedance; under compliance monitoring programs, the first time an exceedance is reported it is an initial statistical exceedance and is only considered an SSI if a confirmatory result verifies the initial exceedance.



1.3.1 Interwell vs Intrawell Statistical Analysis

1.3.1.1 Interwell Statistical Analysis

An interwell statistical evaluation compares the groundwater results from the compliance (downgradient) monitoring wells to a pool of background (typically upgradient) monitoring well results. If results from the downgradient wells are statistically higher (or significant) than the background dataset then an exceedance is triggered. This upgradient verses downgradient method typically assumes that:

7

- Naturally, un-impacted groundwater characteristics in the compliance monitoring wells is comparable and equal on average to the background monitoring wells.
- Upgradient and downgradient monitoring well samples are drawn from the same aquifer and are screened in essentially the same hydrostratigraphic position.
- The aquifer unit is homogeneous and isotropic.
- Groundwater flow is in a definable pathway from upgradient to downgradient wells beneath the CCR Unit.

An interwell approach is preferable for statistical evaluation because it compares data to a background dataset that is not influenced by the CCR Unit. Interwell methods should be used with two exceptions: (1) there are significant differences in the datasets of the background wells (as indicated by methods described in Section 1.2.4) or (2) it can be demonstrated that groundwater geochemistry at all wells (background and compliance) is not impacted by the CCR Unit.

1.3.1.2 Intrawell Statistical Analysis

An intrawell statistical evaluation compares the groundwater results from a compliance monitoring well to historical data collected from that same compliance monitoring well. This method can be used for CCR monitoring when groundwater data from the background monitoring wells is statistically different than that of the compliance monitoring wells or when it can be shown that there is no impact from the CCR Unit in either upgradient or downgradient/compliance wells.

1.3.2 Statistical Power

As discussed above, one of the primary goals of the selection of a proper statistical evaluation method is to limit the potential for results to falsely trigger a SSI while also maintaining sufficient statistical power to detect a true SSI. Falsely triggering a SSI when no release from the CCR unit has occurred is referred to as a false positive. The False Positive Rate (FPR), typically denoted by the Greek letter α , is also known as the "significance level". The FPR is the probability that a future compliance observation will be declared to be from a different statistical distribution than the background data. If the FPR is set too high, it can lead to the conclusion that there is evidence of impact when none exists. Conversely, if the FPR is set too low, it can lead to a false conclusion that no contamination exists, when it actually does exist (also known as a "false negative"). Ultimately, the ability to accurately identify SSIs depends on the selection of an appropriate FPR, which is referred to as the statistical power. FPRs are set for each parameter (or for each





parameter in each well for intrawell analysis). However, statistical analysis programs and the resulting decision making do not depend on each individual measurement/comparison error rates, but are dependent on the collective error rate from all of the individual comparisons. When the individual FPRs are integrated over the entire statistical monitoring program, it is referred to as the site-wide false positive rate (SWFPR), which is a better measure of the ability of the entire statistical program to detect false positive observations.

1.3.2.1 Site-Wide False Positive Rate

For CCR monitoring, detection monitoring events are based on multiple comparisons, which include the seven (7) Appendix III parameters, at each compliance monitoring well. The SWFPR can be calculated based on several input parameters, including the assumed FPR, the number of downgradient monitoring wells (n), the number of parameters, and the number of statistical comparisons events in a given year for the CCR Unit. The Unified Guidance recommends that a statistical evaluation program be designed with an annual, cumulative SWFPR of approximately 10%.

The Unified Guidance recommends measuring statistical power using power curves which display the probability that an individual comparison will detect a concentration increase relative to background results. After determining the statistical method based on the background data, a power curve can be generated in order to determine the statistical power of the compliance monitoring program. The methods and procedures for calculating the SWFPR are described in Section 6.2.2 of the Unified Guidance.

1.3.2.2 Verification Sampling

Verification Sampling is an important aspect of the SAP as it improves statistical power while maintaining the SWFPR. Most statistical evaluations incorporate verification sampling mathematically into their determination of the SWFPR. Verification sampling is typically completed at a 1 of 2 pass strategy. As described above if an initial statistical exceedance is reported, then verification sampling will be performed to confirm the initial exceedance. Verification samples should be collected on a schedule that allows for physical independence of the samples. In a 1 of 2 pass strategy, if the concentration of the verification sample is less than the calculated compliance limit, then no SSI is triggered. If the initial and subsequent verification observation are above the calculated compliance limit, a SSI is triggered.

Due to the time constraints for reporting put forth in the CCR rule, it is suggested that verification sampling not be completed at the next regularly scheduled sampling event, but instead be collected prior to the next sampling event. Verification sampling within 90 days (assuming a 1 of 2 pass verification sampling strategy) will typically allow sufficient time to complete laboratory and statistical analysis in accordance with the timeframes set forth in the CCR Rules.



1.3.3 Statistical Evaluation Methods

As outlined above, the CCR rule list 5 possible methods for statistical evaluation. The different methods that can be employed for CCR monitoring as outlined in §257.93(F) are:

9

- §257.93(F)(1) "A parametric analysis of variance followed by multiple comparison procedures to identify statistically significant evidence of contamination. The method must include estimation and testing of the contrasts between each compliance well's mean and the background mean levels for each constituent."
- §257.93(F)(2) "An analysis of variance based on ranks followed by multiple comparison procedures to identify statistically significant evidence of contamination. The method must include estimation and testing of the contrasts between each compliance well's median and the background median levels for each constituent."
- §257.93(F)(3) "A tolerance or prediction interval procedure, in which an interval for each constituent is established from the distribution of the background data and the level of each constituent in each compliance well is compared to the upper tolerance or prediction limit."
- §257.93(F)(4) "A control chart approach that gives control limits for each constituent."
- **§257.93(F)(5)** "Another statistical test method that meets the performance standards of paragraph (g) of this section."

1.3.4 Prediction Intervals

Section §257.93(F)(3) outlines using prediction intervals or tolerance intervals for statistical evaluation. Based on recommendation from the Unified Guidance, prediction limits are the preferred method for calculating detection monitoring compliance limits and will be used to calculate compliance limits for the seven Appendix III constituents. In addition, the Unified Guidance suggests using prediction limits with verification sampling (Chapter 19 of the Unified Guidance), because prediction limits help to maintain low SWFPR while still providing high statistical power. Tolerance intervals, which are a backward looking procedure, should not be used for detection monitoring, but will likely be used in assessment monitoring, as further described in Section 2.0 below. If, at any point in the future, a different statistical method becomes more applicable to the site conditions, this document may be modified to include that method as recommended by the Unified Guidance.

Prediction interval methods can be used for parametric and non-parametric datasets as well as for intrawell or interwell statistical analysis. Prediction limits use background data from either background monitoring wells for interwell analysis or from historical data for intrawell analysis calculate a concentration that represents an upper limit of expected future concentrations for a particular population. In contrast to tolerance limits, prediction intervals are a forward looking, predictive analysis, which incorporate uncertainty in future measurements, and are thus the most appropriate method for detection monitoring programs. Typically, a one-sided upper prediction limit is used to evaluate detection monitoring observations. Observations must be lower than the prediction limit (or within the upper and lower prediction limits for pH) to be considered "in control". Parametric methods are generally preferred over non-parametric methods, because they result in lower SWFPRs and higher statistical power.





For detection monitoring, if parametric testing is required, the procedures outlined in Section 19.3.1 of the Unified Guidance should be used to calculate prediction limits for the statistical analysis. If non-parametric testing is required, the procedures outlined in Section 19.4.1 of the Unified Guidance should be used to calculate prediction limits. Most groundwater statistical software includes algorithms for calculating either parametric or non-parametric prediction limits.

1.3.5 Double Quantification Rule

In situations where the entire background dataset is reported as ND or Estimated (J-flag), the Double Quantification Rule (DQR) will be used to supplement the prediction limit analyses. Generally, the Appendix III constituents occur at detectable concentrations in natural groundwater; however, if ND results are encountered for a given constituent, the DQR can be implemented. A demonstration that this statistical evaluation is as least as effective as any other test and results as described in §257.93(f)(5) can be made. The DQR is recommended by the Unified Guidance as a supplement to prediction limits because it reduces the number of non-detects used for statistical analysis and provides a lower SWFPR while maintaining statistical power.

Under the DQR, a SSI is triggered if a compliance well observation is higher than the reporting limit (RL)/PQL in either (1) both a detection monitoring sample and its verification resample, or (2) two consecutive sampling events in a program were resampling is not utilized.

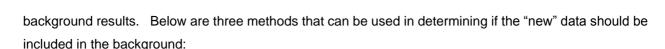
1.4 Responding to SSIs

If the statistical evaluation for an Appendix III analyte triggers a SSI, the data must be evaluated to determine if the cause of the SSI is due to a release from the CCR Unit or from an alternative source. Possible alternative sources may include laboratory causes, sampling causes, statistical evaluation causes, or natural variation. If the SSI can be attributed to one of these sources and the SSI was not caused by the CCR Unit, an alternate source demonstration (ASD) can be completed. An ASD must be certified by a qualified professional engineer and completed in writing within 90 days of completing the statistical evaluation for a particular sampling event. If the SSI cannot be attributed to an alternative source and is from the CCR Unit, then Assessment Monitoring is triggered.

1.5 Updating Background Values

The Unified Guidance suggests that updating statistical limits should only be completed after a minimum of 4 to 8 new measurements are available (i.e., every 2 to 4 years of semiannual monitoring, assuming no verification sampling). The periodic update of background, during which additional data are incorporated into the background, improves statistical power and accuracy by providing a more conservative estimate of the true background population. Prior to incorporating new data into the background dataset, a test should be performed to demonstrate that the "new data" are from the same statistical population as the existing





11

- Time Series Graphs As described in Section 1.1.2.1, time series graphs can be used as a qualitative test to assist with the determination whether a new group of data match the historical data or if there is a concentration trend that could be indicative of a release or evolving groundwater conditions.
- Box-Whisker plots can also be used to determine whether or not the datasets are similar.
- Mann-Whitney (or Wilcoxon Rank) Test Used to evaluate the ranked medians of both the historical and new dataset populations. An α of 0.05 should be used for this evaluation. After calculation, if the Mann-Whitney statistic does not exceed the critical point, the test assumes that the two data populations have equal medians, and therefore are likely similar.

Ultimately, the Mann-Whitney (Wilcoxon Rank Sum) Test is the statistical test that is used to determine whether new observations should be included in the background dataset. It is important to note that a difference in background datasets does not automatically prevent the new data from being used; however, if differences are noted, a review of the new data will be conducted to determine if the noted difference is a result of a change in the natural conditions of the groundwater or if it is the result of a potential release from the CCR Unit. If the new data are included in the background dataset, the prediction limits will be recalculated, as described in Section 1.3.4 above.





2.0 ASSESSMENT MONITORING STATISTICAL EVALUATION

This section discusses the procedures, methods, and processes that will be implemented as part of the assessment monitoring statistical evaluation, if required. Assessment monitoring will be initiated if a SSI is triggered during detection monitoring. As per the CCR Rule in Section §257.95(b), assessment monitoring must be initiated within 90 days of identifying an SSI (not the sample event which provided the data that resulted in the SSI). This 90-day period includes sampling the groundwater monitoring network for the Appendix IV constituents. Following the initial sampling event for all Appendix IV constituents, the monitoring network is then sampled again within 90 days of receiving the results from the initial Appendix IV sampling event. Following these initial assessment monitoring events, assessment monitoring is performed on a semiannual basis. During one of the two semiannual events, the full list of Appendix IV constituents must be tested. During the second assessment monitoring event of each year, only the Appendix IV constituents that are detected during the previous semiannual event are required to be Assessment monitoring is terminated if concentrations for all Appendix III and Appendix IV monitored. constituents in all compliance wells are statistically lower than background for two consecutive sampling events (§257.95(e)). The following sections discuss the procedures, methods, and processes that will be implemented as part of the assessment monitoring statistical evaluation. As discussed in Section 1.1 of this document, many of the statistical comparisons used in assessment monitoring require various analyses to be completed prior to the data being accepted into the statistical evaluation. Before using the results from assessment monitoring, the steps outlined in Sections 1.1 and 1.2 will be completed. Please refer to those sections for descriptions on the methods and techniques required to complete these analyses.

2.1 Establishing a Ground Water Protection Standard (GWPS)

Following the removal of outliers and the performance of general statistics described in Sections 1.1 and 1.2, GWPS will be developed for use in the assessment monitoring program. The GWPS is a key element to the assessment monitoring process. GWPS must be generated for each of the detected Appendix IV analytes. If interwell methods are utilized (preferred method), a site-wide GWPS will be generated for each analyte based on Appendix IV results reported for background/hydraulically upgradient wells. If intrawell methods are utilized, a well specific GWPS will be generated for each analyte.

For Appendix IV parameters that have a maximum contaminant level (MCL), as established by the United States Environmental Protection Agency, the GWPS is set equal to the MCL. For those constituents whose background concentration are greater than the MCL, the GWPS will be calculated from the background data. Finally, for those constituents that do not have an established MCL, the GWPS will be calculated. Several analytes (cobalt, lead, lithium, and molybdenum) do not have MCLs established and therefore the GWPS must be calculated based on their background concentrations.





2.1.1 Maximum Contaminant Level (MCL) Based GWPS

Many of the Appendix IV analytes have USEPA MCL levels. As specified in the CCR Rule in Section §257.95(b), the GWPS must either be the MCL, or a limit based on background data, whichever is greater. This section describes the methods to be used for statistical analysis when the MCL is to be used as the GWPS.

For Assessment Monitoring, the Unified Guidance recommends the confidence interval method to evaluate for potential exceedances, which are referred to as "statistically significant levels" (SSLs) (Chapter 21, Unified Guidance). Using confidence intervals, SSLs are identified by comparing the calculated confidence interval against the GWPS. A confidence interval statistically defines the upper and lower bounds of a specified population within a stipulated level of significance. Confidence intervals are required to be calculated based on a minimum of 4 independent observations, but a more representative confidence interval can be developed when all of the available data are utilized.

The specific type of confidence interval should be based the attributes of the data being analyzed, including: (1) the data distribution, (2) the detection frequency, and (3) potential trends in the data. Table 1 below is based on Table 4-4 from the Electric Power Research Institute's *Groundwater Monitoring Guidance for the Coal Combustion Residual Rule* (2015), which displays the criteria for selecting an appropriate confidence interval. The method and procedure for calculating the Upper Confidence Limit (UCL) and Lower Confidence Limit (LCL) is provided in the section reference from the Unified Guidance, which is listed in the last column of Table 1, below.



Table 2- Confidence Interval Method Selection

Data Distribution	Non-detect Frequency	Data Trend	Confidence Interval Method			
Normal	Low	Stable	Confidence Interval Around Normal Mean (Section 21.1.1)			
Transformed Normal (Log-Normal)	Low	Stable	Confidence Interval Around Lognormal Arithmetic Mean (Section 21.1.3)			
Non-normal	N/A	Stable	Nonparametric Confidence Interval Around Median (Section 21.2)			
Cannot Be Determined	High	Stable	Nonparametric Confidence Interval Around Median (Section 21.2)			
Residuals After Subtracting Trend are Normal (with equal variance)	Low	Trend	Confidence Band Around Linear Regression (Section 21.3.1)			
Residuals after Subtracting Trend are Non-Normal	Low	Trend	Confidence Band Around Theil-Sen Line (Section 21.3.2)			

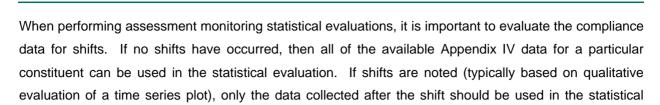
14

In an assessment monitoring program the LCL is of prime interest. If the LCL exceeds the GWPS, there is statistical evidence that a SSL has been triggered. An initial SSL should be confirmed by verification sampling. If only the UCL exceeds the GWPS while the LCL is below the GWPS, the test is considered inconclusive and the Unified Guidance recommends that this situation be interpreted as "in compliance". If both the UCL and the LCL are below the GPWS, the data are also "in compliance" with the GWPS.

It is important to note that a slightly different set of criteria are used to determine whether assessment monitoring can be terminated. Additional discussion of the criteria used for exiting assessment monitoring and returning to detection monitoring is provided below in Section 2.2.

During Assessment Monitoring, a per test FPR (α) of 0.05 will be used as an initial error level for calculating the two-tailed confidence intervals for the compliance wells (which actually means 2.5% FPR per tail). In some cases based on recommendations from the Unified Guidance, it is appropriate to adjust the FPR of the confidence interval based on the number of data points available as well as the distribution of the data being evaluated. If deemed necessary based on recommendations from the Unified Guidance, an approach is provided in Section 22 of the Unified Guidance for determining an appropriate per test FPR based on the data characteristics.





2.1.2 Non-MCL Based GWPS

evaluation.

Background or historical concentration limits should be assessed using the following techniques for all Appendix IV analytes. These concentration limits should then be compared with the MCL, if available, and the higher of these two values will be used as the GWPS.

The Unified Guidance provides two acceptable approaches for establishing a non-MCL based GWPS (unless all values are ND, in which case the Double Quantification Rule as described above in Section 1.3.5 should be used). The two methods include the tolerance interval approach or the prediction interval approach.

2.1.2.1 Tolerance Interval Approach

If the background dataset is normally or transformed normally distributed, the Unified Guidance recommends Tolerance Intervals over the Prediction Intervals for establishing a GWPS. The GWPS should be based on a 95 percent coverage/95 percent confidence tolerance interval. If the background data are non-normal (even after transformation), then a large number of background observations are required to calculate a non-parametric tolerance interval (typically a minimum of 60 background observations are required to meet these requirements). If there is an insufficient number of background observations to calculate a non-parametric tolerance interval, then a non-parametric Prediction Interval approach should be used, as described in Section 2.1.2.2 below.

The Upper Tolerance Limit (UTL) is calculated for each detected Appendix VI constituent. Tolerance Limits, as outlined in the Unified Guidance (Section 17.2), are a concentration limit that is designed to contain a pre-specified percentage of the dataset population. Two coefficients associated tolerance intervals are (1) the specified population proportion and (2) the statistical confidence. The coverage coefficient (γ), which is used to contain the population portion, and the tolerance coefficient (or confidence level (1- α)), which is used to set the confidence of the test. Typically, the UTL is calculated to have a coverage and confidence of 95%. When an MCL does not exist or the background concentrations are greater than the MCL, the calculated UTL for each constituent is used as the GWPS. The confidence interval for each compliance well is then compared with the GWPS.

In order to calculate a valid confidence interval, a minimum of four data points are necessary for each of the detected Appendix IV constituents in each compliance monitoring well (or four "new" assessment





monitoring observations in each well when intrawell statistical methods are employed). Using the Tolerance Interval Approach, a statistically significant level (SSL) is triggered when calculated lower confidence limit (LCL) for each compliance well is greater than the GWPS.

Tolerance limits can be completed using both parametric (Section 17.2.1 of Unified Guidance) or non-parametric methods (Section 17.2.2 of Unified Guidance). However, as described above, the non-parametric method requires at least 60 background (or historical) measurements in order to achieve 95% confidence with 95% coverage. Tolerance Intervals can be calculated using most groundwater statistical software packages.

2.1.2.2 <u>Prediction Interval Approach</u>

If Tolerance Intervals cannot be used to calculate the GWPS (based on recommendation from the Unified Guidance, such as non-parametric datasets, ect.), then a Prediction Interval method should be used. This method is very similar to Section 1.3.4 of this document, however, for assessment monitoring, the Unified Guidance suggests using a prediction interval about a future mean for normally/transfomred-normally distributed datasets or a prediction interval about a future median for datasets with a high percent of ND or non-normally distributed data.

When using prediction intervals to calculate for a GWPS, a one-sided prediction interval is calculated using background (or historical) datasets based on a specified number of future comparisons - four future comparisons is typical. The Upper Prediction Limit that is calculated as a product of this method then becomes the GWPS, and is compared against the confidence interval for the compliance data, as described in Section 2.1.2.1, above. As also described above, if the LCL is greater than the calculated prediction limit then an SSL is triggered.

2.2 Returning to Background Detection Monitoring

As specified in 257.95(e) of the CCR Rule, in order to return to detection monitoring, the concentration of all constituents listed in Appendix III and Appendix IV must be shown to be at or below calculated "background (or historical) values" for two consecutive semiannual sampling events. This determination of background values is based on the statistical evaluation procedure established for detection monitoring. Therefore, if prediction limits (with the double quantification rule for analytes with all non-detects) are used for detection monitoring, prediction limits should be calculated and used for all Appendix III and IV analytes to determine when the monitoring program can return to Detection Monitoring. It is important to remember that Appendix IV constituents are only required to be sampled annually with only those Appendix IV constituents that are detected during the previous semiannual event being required to be analyzed during the second semiannual event of a given year. If statistical results demonstrate that concentrations for all constituents are below background levels for a particular event, all Appendix IV constituents should be sampled during the next event in order to achieve this goal of returning to Detection Monitoring. If this



17



statistical evaluation demonstrates that any of the Appendix III or Appendix IV are at a concentration above background levels, but no SSLs have been triggered, then the CCR unit will remain in assessment monitoring (257.95(f)).

2.3 Response to a SSL

If the assessment monitoring statistical evaluation demonstrates that a SSL has been triggered, then the owner/operator of the CCR unit must complete the following four actions as described in 257.95(g):

- Prepare a notification identifying the constituents in Appendix IV that have exceeded a CCR Unit specific GWPS. This notification must be placed in the facilities operating record within 30 days of identifying the SSL
- Define the nature and extent of the release and any relevant site conditions that may affect
 the corrective action remedy that is ultimately selected. The characterization must be
 sufficient to support a complete and accurate assessment of the corrective measures
 necessary to effectively clean up releases from the CCR Unit and must include at least the
 following;
 - A. Installation of additional monitoring wells that are necessary to define the contaminant plume.
 - B. Collect data on the nature and estimated quantity of the material released,
 - C. Install and sample at least one additional monitoring well at the facility boundary in the direction of the contaminant plume migration,
- 3. Notify off-site property owners if the contamination plume has migrated offsite on to their property, and
- 4. If possible, provide an alternative source demonstration that determines that the SSL is not caused by a release at the facility within 90 days of completing the statistical evaluation. If no alternative source demonstration can be made and the plume is determined to have come from the CCR Unit then initiate corrective action.

Actions 1-3 must be completed regardless of whether or not an alternate source demonstration can be made.

2.4 Updating Background Values

The background for Assessment Monitoring Parameters should be updated using the same methods and techniques described in Section 1.5 for updating detection monitoring background data.





3.0 REFERENCES

EPRI. 2015. Groundwater Monitoring Guidance for the Coal Combustion Residual Rule. Electric Power Research Institute. November.

18

- USEPA. 2009. Statistical Analysis of Groundwater Monitoring Data at RCRA Facilities, Unified Guidance.

 Office of Resource Conservation and Recovery Program Implementation and Information Division.

 March
- USEPA. 2015. Federal Register. Volume 80. No. 74. Friday April 17, 2015. Part II. Environmental Protection Agency. 40 CFR Parts 257 and 261. Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule/ [EPA-HQ-RCRA-2009-0640; FRL-9919-44-OSWER]. RIN-2050-AE81. April.



APPENDIX I EXAMPLE FIELD FORMS

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		CICICO								
Project	Ref:				-		Project N	No.:		
Locati	ion									
Monitore	ed By:			Date			Time			
Well P	Piezom	eter Data	3							
Depth of \	Well (from	(circle one) top of PVC or	ground)					feet		
Depth of \	Water (fror	m top of PVC	or ground)					feet		
Radius of	Casing							inches		
								feet		
Casing Vo	olume							cubic feet		
								gallons		
Devel	opmen	t / Purgii	ng Dis	charge	e Data					
Purging M	1ethod									
Start Purg	ging			Date			Time			
Stop Purg	jing			Date			Time			
Monitoring	g									
Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft TOC)	Appearance of Water and Comm

Date	Time	Volume Discharge (gals)	Temp (°)	рН	Spec.Cond. (S/cm)	Turbidity (NTU)	Dissolved Oxygen (mg/L)	Redox Potential (+/- mV)	WL (ft TOC)	Appearance of Water and Comments

GROUNDWATER SAMPLE COLLECTION FORM



Project Ref:						Project No. :	
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FIELD MEASUR	REME	NTS					
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7							
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Hand Pump

Teflon

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CLIENT:			SURFACE ELEVATI	ON:
GEOLOGIST:		NORTHING:		EASTING:
DRILLER:		STATIC WATER LEVEL	-:	COMPLETION DATE:
DRILLING COMPANY:			ORILLING METHOD	S:
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		SIZE C	OF SAND PACK:	
		AMOU	INT OF SAND:	
		——— вотто	OM OF SCREEN DEPTH	I (ft. bgs):
TOTAL DEPTH				. bgs):
OF BOREHOLE (ft. bgs):		BOTTO	OM OF FILTER PACK (ft. AND AMOUNT OF BACK	. bgs):
CHECKED BY:				PREPARED BY:



RECORD OF WATER LEVEL READINGS

Project N	lame:			Location:			Project No.:				
Borehole No.	Date	Time	Measuring Device / Serial No.	Measurement Point (M.P)	Water Level Below M.P.	Correction To Survey Mark	Survey Mark Elevation	Water Level Elevation	Ву	Comments	

Sheet ___ of ___



Project Name:													
Calibration By:													
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Chain of Custody Record >>> Select a Laboratory <<< #N/A #N/A #N/A Regulatory Program: DW NPDES RCRA Other: #N/A COC No: **Client Contact** Project Manager: Site Contact: Date: Tel/Fax: Carrier: COCs Your Company Name here Lab Contact: of Address **Analysis Turnaround Time** Sampler: For Lab Use Only: WORKING DAYS City/State/Zip CALENDAR DAYS Walk-in Client: Phone (xxx) xxx-xxxx TAT if different from Below FAX Lab Sampling: (xxx) xxx-xxxx 2 weeks Project Name: 1 week Site: Job / SDG No.: 2 days P O # 1 day Sample Type Sample Sample # of (C=Comp, Sample Identification Date Time G=Grab) Matrix Cont. Sample Specific Notes: Preservation Used: 1= Ice, 2= HCI; 3= H2SO4; 4=HNO3; 5=NaOH; 6= Other Possible Hazard Identification: Sample Disposal (A fee may be assessed if samples are retained longer than 1 month) Are any samples from a listed EPA Hazardous Waste? Please List any EPA Waste Codes for the sample in the Comments Section if the lab is to dispose of the sample. Unknown Poison B Return to Client Archive for___ Non-Hazard Flammable Disposal by Lab Months Special Instructions/QC Requirements & Comments: **Custody Seals Intact:** Cooler Temp. (°C): Obs'd: Corr'd: Therm ID No.: Custody Seal No .: Yes No. Relinquished by: Date/Time: Received by: Company: Company: Date/Time: Relinguished by: Date/Time: Date/Time: Received by: Company: Company:

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Golder Associates

Field Boring Log

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	SAMPLE TYPES				ABBREVIATION	<u>s</u>			ORDER OF DESCRIPTION	<u>NC</u>		NON-COHES	IVE S	OILS	COHESIVE S	OILS		
C.S. * D.O. D.S. F.S. P.S.	CHUNK SAMPLE DRIVE OPEN (SPT) DENISON SAMPLE FOIL SAMPLE PITCHER SAMPLE SOIL CORE	ANG BL BR C CIN CO CL CLY	ANGULAR BLACK BROWN COARSE CAVE-IN COHESIVE CLAY CLAYEY DRY	GR HE HO LYD M MIC MOT MST NC	GRAY HETEROGENEOUS HOMOGENEOUS LAYERED MEDIUM MICACEOUS MOTITLED MOIST NON-COHESIVE	RX RND SAT SD SI SIY	RED RESIDUAL ROCK ROUNDED SATURATED SAND SILT SILTY SOME	ENERAL CONSTITUENTS	1) GROUP SYMBOL 2) SOIL GROUP NAME 3) PRIMARY COMPONENTS 4) SECONDARY COMPONENTS; 5) MINOR COMPONENTS; 6) COLOR 7) WEATHERING 8) STRUCTURE 9) SENSITIVITY	CL/SI: SD: S GL: S S		RELATIVE DEI VERY LOOSE LOOSE COMPACT DENSE VERY DENSE	VLS LS CP DN	0-4 $4-10$ $10-30$ $30-50$	VERY SOFT SOFT	VS S FM ST	<0.25	FINGER PRESSURE EXTRUDES 5 MOLDS EASILY MOLDS THUMB INDENTS THUMBNAIL INDENTS RESISTS THUMBNAIL
*	WASH SAMPLE E SIZE	EL F FL FRAG GL	ELONGATED FINE FLAT FRAGMENTS GRAVEL	NP OG ORG	NON-PLASTIC ORANGE ORGANIC POCKET PEN. PLASTIC LIMIT	TR WL WH WR Y	TRACE WATER LEVEL WEIGHT OF HAMMER WEIGHT OF RODS YELLOW	BEHAVIOR GI	10) CONTAMINATION 11) MINEROLOGY 12) ORIGIN; 13) BEHAVIOR (CO/NC) 14) MOISTURE/WATER CONTEN 15) DENSITY/CONSISTENCY	"AND"	" 5 – 12% K "-Y" 12 – 35% 35 – 50%	MOIST FEEL	FLOW S COC	S DL	W~PL CAN	NOT ROLL	-	

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